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ROCOZ DATA REDUCTION AND ANALYSIS

PROGRAMS AND PROCEDURES

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JANUARY 19, 1984



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INTRODUCTION

General

The Rocoz data reduction programs transform data from the Rocoz photometer to ozone number density and overburden as a function of altitude. Required auxiliary data are the altitude profile versus time and, for appropriate corrections to the ozone cross sections and scattering effects, air pressure and temperature profiles. Air temperature and density profiles may also be used to transform the ozone density versus geometric altitude to other units, such as to ozone partial pressure or mixing ratio versus pressure altitude.

A set of seven programs are used to accomplish this. The programs and the functions of each are as follows:

RADAR: Reads the 7-track BCD tape, converts from English to metric units, converts from seconds after launch to seconds after the hour, and writes real numbers on the 9-track tape.

LISTRAD: Displays data from the "PASS1" radar tape generated by the Eclipse Computer at WFF.

RAW OZONE: Displays selected records from the digitized telemetry tape to enable a preliminary assessment of the instrument performance and data quality.

EDIT OZONE: For each rotation of the filter wheel, this program extracts a value for each filter, corresponding values of the compensation channel and of the uncompensated signal, converts telemetry data on battery voltage and instrument temperature to engineering units, and provides some statistics on instrument performance.

MERGE: Obtains altitude information corresponding to each filter observation; computes corresponding solar zenith angles

SMOOTH: Derives smoothed photometer output at integer altitudes for each filter, with statistical measures of deviations.

PROFILE: Converts the smoothed photometer data (intensity or intensity ratios) to ozone number

and air densities for evaluation of Rayleigh scattering effects. The program then converts the ozone densities and geometric altitude to other useful units: ozone partial pressure, mixing ratio, pressure altitudes, and, at intervals corresponding to standard pressure levels, SBUV pressure levels, and Umkehr layers.

History

The first of the series of Rocoz photometers was flown by A. Krueger in the 1950's; data reduction and analysis was with the assistance of a desk calculator. In 1977-8, D. U. Wright of GSFC and E. H. Shaffer of Systems and Applied Sciences Corporation (SASC) implemented the data reduction on the IBM 360/91 computers in the Science and Applications Computing Center (SACC) at GSFC. These programs were documented in the "Rocoz Automatic Data Processing User's Guide" prepared by SASC under Contract NAS5-24278.

These programs were revised by K. Tewari of P & P Industries to accommodate changes in tape format, modified to reduce uncertainties, and adapted to special projects, particularly, the use of the Rocoz instrument on various balloon platforms.

This latest revision, by E. Reed and G. Batluck of GSFC and S. Cooke of Republic Management Systems is the result of a line-by-line examination of the programs. Major revisions include:

The frames in each wheel rotation cycle are identified and handled in terms of the time tag rather than an index number.

The noise from sources other than analog-to-digital conversion is evaluated.

Some auxiliary parameters (e.g., earth radius) are computed more precisely.

Numerous changes were made to improve efficiency and to add to clarity.

Smoothing is accomplished by a least squares fit to $\ln S = A + B \ln (hs-hb)$.

The Profile program has been completely rewritten.

The effective ozone absorption coefficient calculation can be readily modified to include the temperature dependence of the ozone absorption.

A number of tests were added to the Profile program to evaluate the self-consistency of the data set.

"Pedigree" records were added to the EDIT, RADAR, MERGE, SMOOTH, and PROFILE programs to enable inclusion of relevant auxiliary information in the archived data set. The Pedigree records of each previous step are copied to the output tape such that the Profile tape has a complete set of Pedigree records giving the entire history of the processing of the data.

This document describes the result of this latest revision and includes details of the tape and data formats.

Implementation

These programs are written in Fortran-IV (Fortran-66) as implemented on the IBM-3081 computer in the Science and Application Computing Center (SACC) at GSFC. Tapes are identified through the FTIO set of subroutines rather than through the Job Control Language. Other system and SACC-supplied subroutines are:

CMOVE for efficiently moving blocks of data within the programs

BCD5 for converting BCD characters to EBCDIC

SHFTL and SHFTR for extracting the integers which give time information.

(Continued)

Data Requirements

The following information is needed for the complete analysis of the data from a Rocoz flight, using the GSFC set of programs:

1. Rocoz Data Sheet, identifying the vehicle and payload, giving statistics on time of flight and flight performance, and Dobson observations.
2. Calibration data for the Rocoz photometer giving:
 - Filter set number, when calibrated
 - Calibration of filter, A0, A1, A2, and/or filter shape
 - Zero offsets for S0, S1, S2, and S3
 - Battery voltage calibration (word 6)
 - Temperature sensor calibration (marker pulse height)
3. Rocoz telemetry tape, 9-track
4. Radar tape, 9-track, altitude, latitude, longitude, and time
5. Data sonde information:
 - Flight identification and launch time
 - Temperature vs altitude
6. ECC data
 - Flight identification and time
 - Altitude, ozone partial pressure, ozone column, air pressure and air temperature versus time
 - Radar track of ECC sonde
7. Strip chart of telemetry data (desireable, but not absolutely necessary)

RAW PROGRAM

RAW - Outline of Chapter

Overview	II-2
Input Data	II-3

RAW PROGRAM

OVERVIEW

The sole purpose of the RAW Program is to read and dump sample sets of the digital data from computer facilities at Wallops Space Flight Center to validate contents of the tape before proceeding with the subsequent processing steps.

The sample sets may be chosen by record (Version 1 of Software-Input Card Data: Card 1, Variable 3) or by Seconds of Time (Version 2).

The actual processing of these data takes place when the 'EDIT' Program is run. Details concerning the digital input data and the approach to the analysis of same is provided in the 'EDIT' Program section of this document. A description of the RAW Telemetry Tape Format and related pertinent information may be found in the section entitled 'TAPE FORMATS'.

RAW PROGRAM

INPUT DATA

<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
<u>Card 1</u>			
1-6	6A1	Input Tape #	TAPEIN
9-10	I2	Input File #	NF
13	I2	Version #	IVER
16-19	I4	Flight #	NFLIT
<u>Card 2</u>			
1-3	I3	# of Samples	ISAMP
6-9	I4	Beginning Rec #	IBEGIN
12-15	I4	End Record #	ISTOP
17-20	I4	Increment	INCR

Example:

010 0001 0010 0050

Print 10 sample sections of the first 10 records every
50 records.

Card 3

1-6	F6.1	Start Seconds	TIMES
9-14	F6.1	End Seconds	TIME2

The first 2 cards are necessary and the 3rd card is optional, used only if output is chosen by seconds of time, rather than by Record # as in Version #1. Version #2 was never used after Flight # 290.

RADAR PROGRAM

RADAR - Outline of Chapter

Overview	II-6
Input Data	II-7

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RADAR PROGRAM

OVERVIEW

The Radar segment of software is intended to process the Radar tape as received from Wallops Space Flight Center only to the extent of reformatting the data such that it will be acceptable to the 'MERGE' Program which is run after 'EDIT'.

During the 'REFORMATTING', Radar data items not required in later processing were bypassed and a parity check was effected to properly locate the negative sign intended for selected data words. The resulting file is written unformatted onto a tape using the FTIO (Fortran I/O) package.

This 'REFORMATTING' effort was not necessary after Flight 316 when we began receiving Radar tapes which could be used in the 'MERGE' processing phase in their original form.

RADAR PROGRAM

INPUT DATA

<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
<u>Card 1</u>			
2-7	6A1	Input Tape	TAPEIN
14-15	I2	Input Unit	IUNIT
19-20	I2	File #	NF
24-25	I2	# Files	NFILE
30-36	F7.2	# Seconds after Hr	STIME
40-42	I3	Flight	IFLT
46-47	I2	Date-Year	IDATE(1)
49-50	I2	Month	IDATE(2)
52-53	I2	Day	IDATE(3)

<u>Card 2</u>			
2-7	6A1	Output Tape	TAPOUT
14-15	I2	Output Unit	IUNIT2
19-20	I2	Output File #	NF2

<u>Card 3</u>			
2-5	F4.0	Vehicle	R(3)
8-9	I2	Launch Month	LMO
11-12	I2	Launch Day	LDY
14-15	I2	Launch Year	LYR
18-25	F8.1	Launch Time (HHMMSS.S)	R(5)
28-34	F7.3	Latitude (Degrees)	R(6)
37-44	F8.3	Longitude (Degrees)	R(7)
47-62	4A4	Launch Site	SITE

Vehicle is either: 1. Rocket
2. Balloon

Launch Site is either: 01 Wallops Is., Va.
02 Poker Flats, Alaska
03 Natal, Brazil
04 Marambio, Antarctica
05 Palestine, Texas

The above card input was used for flights up thru # 315.
Starting with # 316, the following card input is used:

<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
2-4	I3	Flight #	IFLT
7-13	F7.0	Launch Date (MMDDYY)	DATE
16-21	6A1	Input Tape #	TAPEIN
24-25	I2	Input File #	NFILE

Beginning with Flight # 316, no radar output tapes are produced. Instead, the new version of radar tape is input directly into the Merge Program.

EDIT PROGRAM

Edit - Outline of Chapter

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EDIT PROGRAM

Overview

The primary function of the EDIT Program is to extract for each rotation (cycle) of the filter wheel, a value for each filter and the corresponding compensation word. In addition, the battery voltage monitor and instrument temperature sensor are read and averaged, the length of each rotation (cycle) is noted, and some statistics on noise are generated.

The filter wheel contains four filters, designated S0, S1, S2, and S3, with the S3 filter at the shortest wavelength, S0 at the longest. When each filter is fully in the optical path of the instrument, the output of the photodiode is sampled and held, and a constant value appears on the telemetry word for the remainder of the cycle. A marker pulse on a separate telemetry word (channel) indicates the beginning of each rotation, defined as the time corresponding to an observation through the S0 filter.

Telemetry Data

Data is transmitted at rate of 8K bits/second, or 88.9 frames per second where each frame consists of a synchronization word followed by 8 data words, each 10 bits long. A typical rotation requires about 650 ms, during which the data are sampled about 58 times. The telemetry words are defined as follows:

<u>Word</u>	<u>Function</u>
1	Signal from the S0 filter
2	Signal from the S1 filter
3	Signal from the compensation detector
4	Signal from the S2 filter
5	Signal from the S3 filter
6	Battery voltage monitor
7	Marker pulse, temperature monitor
8	Signal from detector, before compensation

During the initial data reduction process each frame is tagged with time information (day, hour, minutes, seconds, and milliseconds) and grouped into records, each of which contains 110 frames of data.

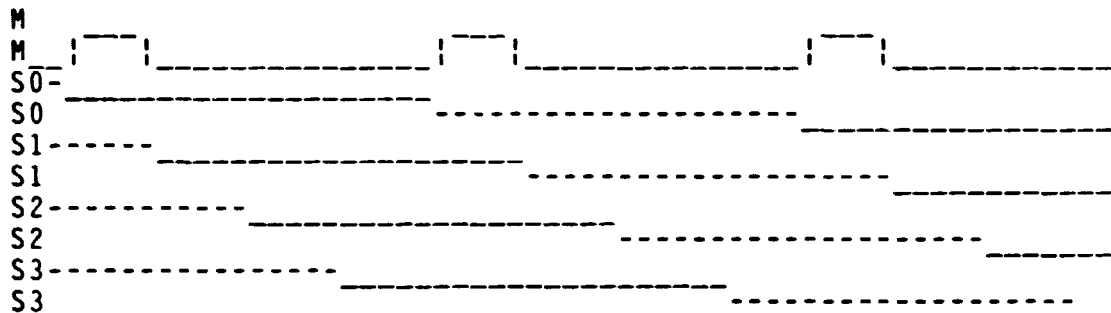
In this program, the input data is read in Subroutine BLOCK. The Header record and Data Description records describing the tape are converted and displayed. The data words are

EDIT PROGRAM

converted to IBM format by switching bytes. The three time words appended to each frame of data are broken apart and interpreted in terms of the date and time.

Identification of Cycles

The identification of the start of each cycle for each of the four filter words is done in Subroutine CYCLE. CYCLE transfers data from the input telemetry tape records to the array, KEEP, always maintaining 200 frames of data in KEEP, and calling Subroutine BLOCK whenever another telemetry record is required. Before moving a frame into KEEP, the data is tested to be sure that the times are increasing and that word 7 (marker pulse) channel is either near the expected base level or the expected marker level, thus identifying and discarding frames that show evidence of being noisy. The initial expected values (MPEAK and LPEAK) are provided on cards as obtained from inspection of a listing of the telemetry data, and are updated by a running average as the program processes the tape. The timing of the changes is diagrammed as follows:



The beginning of a set of values for word 1 (S0) is taken as the first frame after a base value and containing a marker value. The beginning of the word 2 set (S1) is the opposite transition, that is the first frame with a base value after a frame with a marker value. The end of the S0 set of values is the frame with the last base value before a marker value. The time interval between the start of the S1 set and the end of the S0 set is divided into thirds; the S2 set of words is assumed to start at the end of the first third; the S3 set of words is assumed to start at the end of the second third. The length of the S1 set is taken to be 94% of the length of the S0 set, S2 set is 88%, and S3 set is 82% of the S0 set. (The shorter times for some filters allow for uncertainties in the start times due to noisy data and for variations in the cycle time.) Thus, 40

EDIT PROGRAM

to 60 samples are available for each of the four filters, unless diminished by noise and telemetry drop-outs.

Selection of Filter Values

Since the S0 - S3 words are presented to telemetry by sample-and-hold circuitry, each channel should remain constant for a complete rotation. Inspection reveals that this is not the case: the first word is sometimes at the old, rather than the new level; the digitization error is typically \pm one bit; noise either in the instrument and the telemetry system can introduce greater variability; drop-outs in the received telemetry signal can reduce the number of available samples. Subroutine AVE selects a value representative for the array of words available for each filter.

The rules used by Subroutine AVE are:

- If only one sample is available, use it.
- If two samples are available and agree within 6 counts, take their average.
- If three or more samples are available, a subset is chosen in which all the words are ± 3 counts of a test value. If this subset represents more than half of the samples available, the average of the values in this subset is used. If the subset represents less than half of the values, a new test value is chosen (the next word) and a new subset tested.
- If the above rules do not result in an acceptable value, the word is set to -99., indicating that there is not an acceptable value for this filter during this rotation.

Subroutine AVE is used not only to obtain representative values for each filter but also for the marker pulse height and for the marker pulse base level.

For each of the four filters, Subroutine COMPWD finds the value of the compensation channel (word 3) corresponding to the time of the first sample for the filter. It chooses the frame near the start frame chosen in Subroutine CYCLE, for which word 8 (the uncompensated signal through the filter wheel) is at a maximum; word 3 of this frame is then chosen as representing the value of the compensation word at the moment that the filter wheel signal was sampled and held.

EDIT PROGRAM

Averaged Values

Running averages of the most recent ten values are maintained for the height of the marker pulse, the base level of the marker, and the length of the cycle and used for the detection and deletion of aberrant data. To do this, Subroutine Cycle calls Subroutine TENAVE as it nears the completion of processing for each cycle.

The average battery voltage is obtained from a simple average of all the values of word 6 in the most recent record of telemetry data (110 frames) transferred into the array KEEP by Subroutine CYCLE. The instrument temperature is obtained from the value of the marker pulse in the cycle under consideration. The average value of all the compensation words in the cycle is obtained in Subroutine CMPWD.

The average values for the temperature and the battery voltage are converted into engineering units in Subroutine CONVRT. Calibration data are obtained from the preflight testing and given to the program through DATA5 cards. The temperature data are read in at three temperatures and a standard temperature versus counts curve is adjusted to fit the calibrations at the three temperatures. This adjusted curve is then used to convert the counts to temperatures. Calibration values for the battery word are read in at two points, and a straight line relationship is assumed.

EDIT PROGRAM

Common Areas

Four labeled common areas are used: LABEL1 transfers initialization data from MAIN to Subroutine CYCLE; LABEL3 contains the telemetry data, transferring it from BLOCK to CYCLE; LABEL5 contains the output data generated in various subroutines; and CAL contains calibration data, making it available in MAIN for use in the Pedigree records and in Subroutine CONVRT for conversion of telemetry data to engineering units.

COMMON/LABEL1/IREC,DELTAT,MPEAK,LPEAK,LIMIT

<u>Variable</u>	<u>Type</u>	<u>Content</u>
IREC	I*4	Number of the last record to be processed (Statement is in Block, usually commented out.)
DELTAT	R*4	Initial value for length of cycle, ms.
MPEAK	I*4	Initial value for marker pulse peak.
LPEAK	I*4	Initial value for marker base level.
LIMIT	I*4	Delta for acceptable marker values.

COMMON/LABEL3/DATA(1210),INPUT (1220)

DATA(1210)	R*4	Input record in IBM format, no header.
INPUT(1220)	R*4	Input record from telemetry tape.

COMMON/LABEL5/OUTX(20)

OUTX(20)	R*4	Output array.
----------	-----	---------------

COMMON/CAL/B1,V1,B1,V2,T(3),VT(3)

B1	R*4	Battery voltage, first calibration pt.
V1	R*4	Counts corresponding to B1.
B2	R*4	Battery voltage, second calibration.
V2	R*4	Counts corresponding to B2.
T(3)	R*4	Temperatures (deg. C) for calibration.
VT(3)	R*4	Counts corresponding to T(3).

EDIT PROGRAM

Input Data

<u>Card</u>	<u>Column</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
1	1-6	6A1	Location of input tape	TAPEIN
	9-14	6A1	"INPUT"	IOIN
	17-18	I2	Input unit	IUNIT1
	21-22	I2	Input file	NF1
2	1-6	6A1	Location of output tape	TAPOUT
	9-14	6A1	"OUTPUT"	IOOUT
	17-18	I2	Output unit	IUNIT2
	21-22	I2	Output file	NF2
	24-26	I3	Length of output record, 80	LEN2
3	1-5	F6.3	Initial length of cycle, sec.	DELTAT
	8-10	I3	Number of first record to be processed.	IREC
	13-15	I3	Initial value of marker pulse, counts.	MPEAK
	18-20	I3	Initial value of marker base, counts.	LPEAK
	23-25	I3	Acceptable range of marker.	LIMIT
4	1-5	F5.1	Battery voltage.	B1
	6-13	F8.2	Corresponding counts.	V1
	14-18	F5.1	Battery voltage.	B2
	19-26	F8.2	Corresponding counts.	V2
5	1-5	F5.1	Low temperature, degrees C.	T(1)
	6-13	F8.2	Corresponding counts.	VT(1)
	14-18	F5.1	Mid temperature.	T(2)
	19-26	F8.2	Corresponding counts.	VT(2)
	27-31	F5.1	High temperature	T(3)
	32-29	F8.2	Corresponding counts.	VT(3)
6	1-5	F5.1	Flight number.	OUTX(2)
	8-11	F4.0	Payload number.	OUTX(3)
	14-15	I2	Month Telemetry Tape received.	IDATE(1)
	17-18	I2	Day "	IDATE(2)
	20-21	I2	Year "	IDATE(3)

MERGE PROGRAM

Merge - Outline of Chapter

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MERGE PROGRAM

Overview

To compute the ozone concentration it is necessary to have the signal from each filter as a function of altitude. In the Merge Program, the edited telemetry data and the radar data are merged on the basis of time (in seconds after the hour) as the common variable. The solar zenith angle is computed and included in each record of the Merge tape. For the lower part of the flight, a table of counts for each filter as a function of temperature is constructed and displayed. The basic structure of the SASC/P&P version of the program is retained, with the addition of the Pedigree records, provision for direct use of the "PASS1" radar tape produced by Code 961 on the Eclipse computer at WFF, determination of counts versus temperature, and other minor, mostly cosmetic, changes.

After mounting and reading the first records on the Edited Ozone Data Tape and the radar tape, the agreement in flight numbers is verified, and up to 3000 records of radar data are read, storing the time and location data in arrays. The solar zenith angle is computed every 60 seconds and stored in another array. Finally, ozone data are read, the altitude for each filter word interpolated from the radar arrays, the solar zenith angle interpolated for the time of this record, and the Merge records written on the output tape.

Radar Data

For flights through 1982 (through Rocoz flight 315) radar data was provided in the form of a "MESUP" tape, with smoothed data for location and velocities given in English units and written in character format on a 7-track tape. This is then converted to metric data in binary files on a 9-track tape by the Radar Program. The resulting "Reformatted Radar Tape" is then suitable as input to the Merge Program.

For flights beginning with Rocoz no. 316 (August 1983), radar data is supplied by CODE 961 at WFF, using the Eclipse computer. This "PASS1" tape gives the location as a function of time, in meters and in degrees of latitude and longitude. The Merge Program has been modified to permit it to read this tape directly.

MERGE PROGRAM

Both types of tapes from WFF provide time in terms of seconds since launch. These must be converted to seconds since the hour prior to merging with the telemetry data. For MESUP tapes this is done in the Radar Program; for the PASS1 tapes, this is done in the Merge Program. The Merge Program also creates a Pedigree record for the PASS1 tape.

Zenith Angle Computation

In Subroutine ZENITH the solar zenith angle with respect to the Rocoz payload is computed. The apparent right ascension and declination of the sun and sidereal time is provided through DATA5 cards; the location of the payload is obtained from the radar tape. If the radar data is from the MESUP tape, then the location in distance from the launch site must be converted to latitude and longitude. The earth radius required for this conversion is obtained from the latitude of the launch site by the formula (from Basic Physics of the Solar System, Blanco and McCuskey, Addison-Wesley Publ., 1961, p. 83):

$$R0 = 6378388. (1 - 3.367 \times 10^{-3} (\sin(\text{lat}))^2 + 7.1 \times 10^{-6} (\sin(2 \text{ lat}))^2)$$

where R0 is the radius of the earth at the launch site and lat is the latitude of the launch site. The location of the payload is then:

$$\begin{aligned} \text{latp} &= \text{lat0} + 57.29578 \text{ rns}/R0, \text{ and} \\ \text{lonp} &= \text{lon0} + 57.29578 \text{ rew}/(R0 \cos(\text{lat0})) \end{aligned}$$

where latp and lonp are the latitude and longitude of the payload, lat0 and lon0 are the latitude and longitude of the launch site, and rns and rew are the distance (meters) north and east of the launch site. With the appropriate trigonometry, the solar zenith angle as a function of elapsed time and payload location can then be computed. See the program listing for the steps in detail.

The Merge Process

After the radar is stored in arrays, and the solar zenith angle computed for each minute, the Edited ozone data is read in, a record at a time. Provision is included for skipping "bad" sections of data as defined by the input DATA5 cards, although in recent flights this has not been

MERGE PROGRAM

used. The altitude at the time of each word is interpolated from the radar data and the solar zenith angle at the time of the S0 filter is interpolated from the array of zenith angles and are placed in an output record for the Merge tape. The interpolation is done by Subroutine AITKEN, which uses a four-point scheme. Also on the Merge tape are the time for the S0 filter, the value for each filter during this cycle, the corresponding compensation word values, and information concerning the operation of the photometer, namely, the length of the cycle, the number of telemetry samples (frames) used in evaluating the cycle, the temperature of the photometer, and the battery voltage. Processing is terminated when the end of either the radar data or the Edited ozone data is reached. All values written on the tape are also listed for inspection prior to running the Smooth Program.

Counts vs Temperature

To assist in the determination of the zero offset values for filters S2 and S3 as a function of temperature, Subroutine TMPAVE is called for each Merge record as it is generated. For altitudes less than 45 km, S3 less than 100 counts, and temperatures between 39.74 and -10 degrees C., the counts for S3, S2, and S1 are accumulated in 0.5 degree buckets. At the conclusion of the Merge Program, Entry PRINTM of TMPAVE is called to calculate the averages and print a table of the results. In calculating the average count, the maximum and minimum values available in each bucket are discarded.

MERGE PROGRAM

Common Areas

Only one common area is used, named Z, to transfer the astronomical data, time, and payload location data from MAIN to Subroutine Zenith where they are used in the computation of the solar zenith angle. The resulting solar zenith angle is returned to MAIN via this same common area.

<u>Variable</u>	<u>Type</u>	<u>Content</u>
RH,RM,RS	R*4	Apparent Right Ascension in hours, minutes, and seconds
RACOR	R*4	Change of Apparent Right Ascension, seconds per day
DD,DM,DS	R*4	Apparent Declination in degrees, minutes, and seconds.
DECOR	R*4	Change of Apparent Declination, seconds per day.
SH,SM,SS	R*4	Apparent Sidereal Time in hours, minutes, and seconds.
GMT	R*4	Greenwich mean time in hours.
REW,RNS	R*4	Distances east and north from launch site in meters; if MODE=2, degrees
SOLARZ	R*4	Solar zenith angle, degrees

Input Data

The Merge Program uses either the Reformatted Radar Tape or the PASS1 Radar Tape and the Edited Ozone Data Tape as input; detailed descriptions of these tapes are given in the section on Tape Formats. DATA5 "cards" are used to identify the input and output tapes and files, to state the flight number, and other data needed to construct a Radar Pedigree record, to provide the astronomical data, and to delineate "bad" time periods on the Edited Ozone Data Tape. The Apparent Right Ascension and Declination of the Sun may be obtained from tables for 0h Ephemeris Time in Section C of the Astronomical Almanac and the Sidereal time from tables of Universal and Sidereal Times in Section B.

MERGE PROGRAM

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
1	2-7	6A1	Edited Ozone Data Tape ID	EDITED
	12-16	I5	" " file number	NF
	17-21	I5	" " unit number	IUNIT
2	2-7	6A1	Merge Data Tape ID	MERGED
	12-16	I5	" " file number	NF1
	17-21	I5	" " unit number	IUNIT1
3	2-7	6A1	Radar Data Tape ID	RADAR
	12-16	I5	" " file number	NF2
	17-21	I5	" " unit number	IUNIT2
	25-26	I2	Mode #2 reformatted radar #2 PASS1 radar	MODE
4	1-5	F5.1	Rocoz flight number	PED(2)
5	1	I1	Location	LOCA
			=1 Wallops Island	
			=2 Churchill	
			=3 Natal	
			=4 Primrose Lake	
			=5 Poker Flats	
			=6 Marambio	
	28-33	F6.1	Time correction for Edited Ozone, usually 0., seconds	RESTR
	36-38	I3	Begin Edited Ozone record no.	IBEG
	41-42	I2	Number of bad sections of O3 data maximum of 20	NBAD
	43-72	30A1	Rocoz no., date, and time	LAUNCH
6	11-20	F10.2	Apparent Right Ascension, hour	RH
	21-30	F10.2	" " " minutes	RM
	31-40	F10.2	" " " seconds	RS
	41-50	F10.2	" Correction sec/day	RACOR
7	11-20	F10.2	Apparent Declination, degrees	DD
	21-30	F10.2	" " " minutes	DM
	31-40	F10.2	" " " seconds	DS
	41-50	F10.2	" Correction sec/day	DECOR
8	11-20	F10.2	Sidereal Time hours	SH
	21-30	F10.2	" " " minutes	SM
	31-40	F10.2	" " " seconds	SS
	41-50	F10.2	Launch time, hour, GMT from which seconds are counted	HOUR
9-28	1-6	F6.1	Start of section to be skipped seconds after hour	BAD1
	9-14	F6.1	End of section to be skipped, sec	BAD2

SMOOTH PROGRAM

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SMOOTH PROGRAM

Overview

The Smooth Program obtains a value representing the flux through each of the filters at each integer km of altitude. These values are obtained from lines which are a least squares fit to the data in the vicinity of each altitude. If requested, Smooth will do a similar computation for the ratio of flux to that through the S0 filter. The results, with related information, are written on the Smooth Tape for input to the Profile Program and also presented in the form of tables and plots for examination and evaluation.

For input, the Smooth Program requires the Merge data tape, values for the zero offsets and their temperature dependence, the minimum acceptable value for the compensation word, and the desired altitude range.

The Smooth Program described here is based on the code supplied by P & P Industries; much of the descriptive material in the SASC "Rocoz Automatic Data Processing User's Guide" of January 1979 is still applicable. The principal changes are fitting to a logarithmic function instead of a polynomial and basing the error on the fit of the data rather than assuming a fixed count. Additions include a test of the compensation word and the use of the temperature coefficient of the zero offset.

MAIN reads the input from DATA5 and from tape, places all of the Merge data on a disk, calls SELECT to identify and process the data in the vicinity of each altitude level, calls LOGFIT to obtain values representative of each altitude level, calls OUTPUT to write the output in tabular form and on a Merge tape, and finally calls GRAPH to plot altitude and intensity.

All tape and disk input and output are through calls to the FTIO package available on the IBM-3081 computer at GSFC Science and Applications Computing Center. Graphs are prepared with the assistance of the WOLFLOT package likewise available on that computer.

SMOOTH PROGRAM

Selection and Preparation of Data

Initially, the data records are copied from the Merge tape to a disk data set. The data are assumed to be ordered as descending altitude. (For analysis of data from the ascent portion of a balloon flight, this program would require modification.) MAIN chooses integer altitudes, beginning at the top of the altitude range read from DATA5, and calls Subroutine SELECT.

SELECT searches the disk data set for Merge records in the vicinity of this center altitude. Equal numbers of records above and below that for the center altitude are chosen except as limited by the availability of data. Collection of records continues until 100 records are available and the altitude interval is at least two km, or until a maximum of 800 records are collected. The average values for cycle length and the compensation word are computed from the values given in the 99 Merge records centered at the selected altitude. If requested, records are created for which the fluxes for the S3, S2, and S1 filters have been divided by the S0 flux.

Not all of the data are used. Excluded are: records more than 0.5 km above the top of the requested range; filter words with a value of less than 2.0 counts (before zero correction); and filter words for which the corresponding compensation word is below the minimum acceptable value.

Subroutine SELECT corrects all the remaining filter words for zero offset. The zero offsets for the S0 and S1 filters are taken from the records of the laboratory preparation of the payloads, and are usually 0.0. Values for the S2 and S3 filters are obtained from inspection of the Merge listing of the S2 and S3 values at low altitudes. A plot of these data versus temperature usually reveals a non-zero temperature coefficient. Values at two temperatures are placed in DATA5; In SELECT, a temperature dependent offset is computed for each filter word.

Finally, In Subroutine LOGFIT, filter words which are more than two standard deviations from the initial fitted line are discarded, and the constants for the line recomputed. The number of records selected and the number of filter words used are included in the Smooth output record.

SMOOTH PROGRAM

Smoothing and Error Estimates

In Subroutine LOGFIT (based on a program given by P.R.Bevington in Data Reduction and Error Analysis for the Physical Sciences, McGraw-Hill, 1969, p. 104-105, 180-185), the arrays of flux (or ratio to S0) and altitude are fitted to a line of the form

$$\ln I = \ln A + B (h - h_b)$$

where I is the flux or flux ratio,

A is the value of I corresponding to h_b)

h is the altitude, and

h_b is the lowest altitude in this array.

Normally each value is given equal weight (MODE = 0), although the code includes provision for other weighting schemes. Values for A, B, and the standard deviation for the array are calculated, and all points which are more than 2 standard deviations from the calculated value of $\ln I$ are discarded. The remaining values in the array are used in a recomputation of A, B, corresponding standard deviations (SIGMAA and SIGMAB), and the correlation coefficient.

This treatment is not appropriate for all arrays of data, particularly those at large optical depths for which the signal is essentially constant with altitude. Such arrays are detected by testing DELTA and variance for near-zero values. They are evaluated by obtaining the average value of I over the altitude range and calculating the corresponding standard deviation. Here, also, values of I which are more than 2 standard deviations away from the average are discarded and the average recomputed. When this method is used, the values of A, B, SIGMAA, SIGMAB, and the correlation coefficient in the Smooth Data Record are set to zero.

Subroutine SHAPE is provided which may be called from Subroutine LOGFIT (see the comments immediately after ISN 0053) to list the residuals for all the points of an array.

To provide a measure of the extent of smoothing, the number of points used and the upper and lower altitude limits of each array is included in the Smooth Data Record.

In an earlier version of this program, provision was included for associating an error with each point and using this error in the evaluation of the error in the fitted line. This feature is no longer used, although the error arrays are still present.

SMOOTH PROGRAM

Graphical Displays

Subroutine GRAPH, called from MAIN, uses the WOLFLOT package to prepare plots of the smoothed value of the signal (or ratio to the S0 signal) as a function of altitude at each km, using values from the SAVE array. These are displayed as a printer plot and can also be written to tape for use with higher resolution plotters.

Common Areas

Two named common areas are used, one for the arrays of data associated with a particular altitude level, and the other for the output records.

COMMON/LABEL1/N,S(4,800),H(4,800),ER(4,800)

Found in MAIN and Subroutine SELECT.

N	I*4	Number of points in this fitting interval
S(4,800)	R*4	Number of counts (telemetry) for each of the four filters.
H(4,800)	R*4	Altitude for each of the points (km)
ER(4,800)	R*4	Error associated with each point.

COMMON/LABEL2/SAVE(20,50,4)

Found in MAIN and Subroutine OUTPUT.

SAVE(20,50,4) R*4 Array containing all output records.

Input Data

The Smooth Program uses the Merge Tape as the source of data from the Rocoz photometer as a function of altitude; the detailed description of this tape is given in the section on Tape Formats. DATA5 "cards" are used to identify input and output tapes and files, run options, altitude range, minimum compensation channel value, and zero offsets to be applied to each filter. The data in terms of telemetry counts is always evaluated; upon request, the data as the ratio to the S0 signal is also smoothed.

SMOOTH PROGRAM

The altitude range is obtained from inspection of the listing from the Merge program. The upper limit is the altitude at which the attitude is relatively stable, usually several km lower than the ejection altitude; the lower limit is the lowest integer altitude for which data are available. The minimum compensation word value is usually set equal to one-half the minimum compensation value observed, such that data more than about 60 degrees from the Rocoz optical axis can be discarded. Zero offsets for S0 and S1 are obtained from laboratory measurements; for S2 and S3, the data at the lower altitudes are plotted as a function of temperature, a straight line drawn, and values read at two temperatures.

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
1	1-6	6A1	Input Tape Identification	TAPEIN
	9-10	I2	Input Tape File number	NF
	13-14	I2	Input Tape Unit	IUNIT
2	1-6	6A1	Output Tape Identification	TAPOUT
	9-10	I2	Output Tape File number	NF2
	13-14	I2	Output Tape Unit	IUNIT2
3	1-2	I2	Type of weighting, usually 00	MODE
	45	I1	=0: no ratios; =1 divide by S0	LRAT
4	1-6	F6.1	Zero offset (counts) for S0	OFF(1)
	9-14	F6.1	Zero offset (counts) for S1	OFF(2)
	17-22	F6.1	Zero offset (counts) for S2	OFF(3)
	25-30	F6.1	Zero offset (counts) for S3	OFF(4)
5	1-6	F6.1	Temperature (deg. C) for above	TA
	9-14	F6.1	Temperature for next two values	TB
	17-22	F6.1	Zero offset for S2 at 2nd temp.	S2B
	25-30	F6.1	Zero offset for S3 at 2nd temp.	S3B
6	1-4	F4.0	Rocoz flight number	PED(2)

PROFILE PROGRAM

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PROFILE PROGRAM

Overview

The Profile Program obtains data for the RocoZ photometer from the Smooth tape, reads selected values for the Datasonde, the ECC sondes, and the Dobson spectrophotometer, and reads filter calibration values and related tables. The program uses these data in the computation of ozone profiles for each filter and also creates a composite profile based on data from all the filters. With the air temperature and pressure data available from the Datasonde and the ECC sonde, the ozone profile is then be expressed in units such as partial pressure and mixing ratios. Various aspects of the data set are examined for self-consistency. Finally, the basic data and the derived profiles are written on a Profile tape, intended as the archival product of the flight. The Profile Program does not create plots of the data but does include a number of printed tables. These functions are distributed among the 21 Subroutines as follows:

- (1) Assembly of the RocoZ data and correlative observations with the required calibration data.
(CARDS, TAPE, INARRY, SHAPE)
- (2) Computation of related data.
(MODEL, DATSND, SECANG)
- (3) Computation of ozone profiles and composite profile.
(OZDENS, SLANTA, ALFEFF, COMPST)
- (4) Evaluation of RocoZ data set.
(CHECKS, OVERLP, LINFIT)
- (5) Computation of related parameters and display of observations in tables.
(RELATD, PRTWRT)
- (6) Placement of the ozone profiles and related data on the Profile Tape.
(TAPWRT)
- (7) Display of various arrays as desired for test and diagnostic purposes.
(PRTPRF, PRTPED, CFTWRT, PRTSAV)

The general structure is shown in the Block Diagram of the Profile Program.

PROFILE PROGRAM

Brief Description of Each Subroutine

CARDS reads set-up information (e.g. altitude range for each filter) and correlative data from the Datasonde, the Dobson spectrophotometer, and the ECC sondes.

TAPe reads RocoZ data from the Smooth tape.

MODEL contains an ozone model, with derived overburdens. The present Krueger-Minzner mid-latitude model should be replaced with one dependent on latitude and season.

DATSND calculates densities and pressures corresponding to the datasonde temperature profile.

SECANG obtains the secant of the solar zenith angle for each altitude level; for angles over 60 degrees, the Chapman function is computed instead.

OZDENS computes ozone density and column content for each altitude level for each filter, based either on observed fluxes or their ratio to the S0 flux.

SLANTA computes the slant air mass (atmospheres) and the slant ozone overburden (atm-cm) at the three altitude levels under consideration in OZDENS.

ALFEFF computes effective ozone absorption and Rayleigh scattering coefficients, given filter transmission, temperature, slant overburdens, and ozone absorption coefficients.

INARRY obtains solar flux, diffuser transmissions, detector response, Rayleigh scattering coefficients, and ozone absorption coefficients from external data sets, determines range of wavelengths for which data are available, and sets up these arrays for use in computing the effective absorption coefficient.

SHAPE obtains the measured filter transmission.

COMPST obtains a weighted (inversely to associated error) of the available RocoZ ozone data at each altitude level. ECC data are not included.

CHECKS tests the internal consistency of the data related to this profile by (1) comparing ozone values at a given level from different filters, (2) computing

PROFILE PROGRAM

ozone overburden from the Composite Profile as a function of altitude and comparing it with the Model, (3) comparing the measured ozone densities with those from the Model, (4) comparing the (Rocoz+ECC) column content with that measured by the Dobson instrument, (5) comparing various estimates of the rate of change of $\ln I$, (6) comparing the variation of the intensity in the compensation channel with that expected due to changes in the solar zenith angle and scattering, and (7) computing the drag coefficient as a function of altitude (large variations may indicate a defective Starute or errors in the radar altitude data).

- OVERLP called by CHECKS to assemble and analyze the ozone densities at each altitude level.
- LINFIT called by OVERLP to compute a straight line fit to the data at each level.
- RELATD incorporates air temperatures and pressures, and computes ozone values within standard layers and at standard pressure levels.
- PRTPRF displays the contents of the COMMON/PROFLS/ which includes the Datasonde, the ECC, and the model profiles.
- CFTWRT displays the contents of the arrays generated by INARRY and FSHAPE, used in the computation of effective absorption coefficients.
- PRTPED displays the contents of the Pedigree array.
- PRTSAV displays the contents of the SAVE array for each filter, listing the ozone profile and values used in its derivation.
- PRTWRT formats arrays for hard copy printout with appropriate labels and column headings, including the arrays generated by RELATD.
- TAPWRT writes the data selected for archiving on a tape.

PROFILE PROGRAM

Observations and Supplied Values

In the analysis of observations from a Rocoz photometer, additional data are used: various constants, an air temperature profile from a Datasonde, air pressure and ozone profiles from an ECC sonde, total ozone from a Dobson spectrophotometer, and a model ozone profile. The flight plans require that a Datasonde and two ECC sondes be launched close to the time of the Rocoz launch, that all sondes be tracked by radar, and that the Dobson spectrophotometer be operated according to its usual schedule. The raw data from the Datasonde, the ECC sonde, and from the Dobson spectrophotometer are analyzed by the responsible groups, and the observations are provided in terms of the various atmospheric parameters. Data selected from those reports are entered into the Profile program where they are made ready for use with the Rocoz data.

This section of the document discusses the selection and use of the constants and observations. The precise formats for the input of data are found in "Profile Program - Input Data" and in the chapter on Tape Formats. Within the Profile Program, these observations are stored in COMMON/PROFLS/ in arrays which are described in detail in the section on Common Areas.

Constants

Used in the conversions of units, hypsometric computations, estimation of acceleration due to gravity, computation of dynamic viscosity, etc., are a number of constants. The values for Avogadro's number, the gas constant, the mean molecular weights of air and ozone, the volume of an ideal gas, Sutherland's constant, and beta are those given in the U.S. Standard Atmosphere, 1976. The acceleration of gravity at 45 degrees latitude is from the Smithsonian Meteorological Tables (R.J. List, ed., 1968, p. 488).

Avogadro's Number	$6.022169 \times 10^{26} \text{ kmol}^{-1}$
gas constant, R^*	$8314.32 \text{ N m/(kmol K)}$
acceleration of gravity at sea level at 45 deg latitude	$9.806160 \text{ m sec}^{-2}$
mean molecular weight of air	28.9644 kg/kmol
mean molecular weight ratio, ozone/air	1.65714
volume of ideal gas at STP	$22.4136 \text{ m}^3/\text{kmol}$
Sutherland's constant	110.4 K
beta	$1.458 \times 10^{-6} \text{ kg/(s m K}^{1/2})$
degrees to radians	$0.01745329 \text{ rad/deg}$

PROFILE PROGRAM

Dobson Observations

At the Wallops Flight Facility, total ozone is measured by use of a Dobson Spectrophotometer. Occasionally, at remote sites, other instruments may be used which observe total ozone at similar wavelengths, such as the SenTran filter photometer or the Brewer Ozone Spectrophotometer.

To be entered into the Profile Program (Subroutine CARDS) are total ozone values observed before and after the Rocoz flight; the program refers to these as AM and PM data. The date of observation and two values of total ozone are stored in words 2-4 of the type -501. pedigree record (PED(x,6)). Values of total ozone range from about 200 to 650 Dobson Units; a Dobson Unit is intended to be equal to a milliatm-cm of ozone but it is recognized that the effects of non-ozone absorbers and scatterers may, under some circumstances, be inseparable from that of ozone.

In Subroutine CHECKS the ozone column content as measured by the Dobson spectrophotometer is compared to the column content indicated by the combined Rocoz-ECC ozone profile.

Datasonde Observations

The air temperature profile above about 20 km can be obtained from a Datasonde, a small rocket payload consisting of a temperature sensor and a telemetry transmitter suspended from a decelerator, tracked by radar as it transmits temperature data during its descent from the vicinity of 60 km. If only one Rocoz flight is planned on a given day, one Datasonde is usually scheduled with a launch time within one hour of the Rocoz launch. If multiple Rocoz flights are scheduled, Datasonde launches are usually scheduled shortly prior to the first Rocoz launch and shortly after the last Rocoz. Data from the sondes are reduced at the Wallops Flight Facility, with scientific quality control under the cognizance of F. Schmidlin. The reduced data is in terms of air temperature as a function of altitude and also includes the 2-sigma error value associated with each point.

To be entered into the Profile Program (Subroutine CARDS) are information concerning the flight, the temperature profile, and independently observed air pressure and air temperature at a "base" altitude. Identification of the flight (an 8-character Flight Number, date and time of flight), are stored in words 5-8 of the type -502. pedigree record (PED(x,7)). A base altitude and air pressure derived from the independent observations made by the ECC sonde are

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entered and stored in words 9 and 10 of PED(x,7) for use in deriving air pressures and densities at the datasonde altitudes. The time in minutes (MDEL) between the Datasonde and Rocoz launches is entered for use in estimating the temperature error. The altitude, air temperature, and 2-sigma temperature error are entered at integer km altitudes, beginning at the highest altitude for which a temperature observation is available. The temperatures are stored in the remainder of the type -502. pedigree record and in as many type -503. records as are necessary. For use later within the Profile Program, the base altitude, air temperature, and air pressure are stored in DSB in COMMON/PROFLS/, and the altitude, temperature, and temperature error are in SONDE, also in COMMON/PROFLS/. The index for the location in SONDE of the lowest altitude level of the profile is noted and stored as MXSND. Altitudes are stored in km; temperatures in kelvin.

Because the real interest is in the temperature at the time of the Rocoz flight, an error due to atmospheric variability is added to the instrumental error. The formula used in Subroutine CARDS, from F.Schmidlin, (J.Geophys.Res., 86,9599-9603, Oct.20,1981) is

$$\text{delT(Rocoz)} = \text{SQRT} (0.5 * \text{Terr} * \text{Terr} + B * \text{MDEL})$$

where

delT(Rocoz) is the one-sigma error in temperature for the time of the Rocoz flight,

Terr is the two-sigma error of the Datasonde temperature,

B is 0.32 above 52.5 km; 0.19 below 52.5 km, and

MDEL is the difference in minutes between the two launch times, or a maximum of 100.

If the flight report does not include estimated errors in the temperature, the instrument errors given by Schmidlin (see above) may be used. DelT(Rocoz) is stored in SONDE (5,x) and used later in Profile in the estimation of the error associated with the expression of the ozone content in terms of partial pressure or mixing ratios.

In Subroutine DATSND, a profile of air pressure and density is derived from the datasonde temperature profile and the base values of pressure through use of the hypsometric equation:

$$P(\text{alt}) = P(\text{base}) * \exp \frac{(-G * M * (H - H_b) * 1000)}{(R * T)}$$

where

P(alt) is the pressure (mbar) at altitude, H

P(base) is the pressure (mbar) at a base altitude, H_b,

PROFILE PROGRAM

G is the acceleration of gravity at the latitude of observation and altitude H,
M is the mean molecular weight of dry air at sea level, = 28.9644 kg/kmol,
R is the gas constant, = 8314.32 N m/(kmol K)
T is the average temperature (kelvin) between H and Hb, = 0.5 (T(alt) + T(base)),
H is the altitude (km) for P(alt), and
Hb is the altitude (km) for P(base).

The acceleration of gravity at the latitude of observation is computed according to the Smithsonian Meteorological Tables (6th ed., 1968, p.488, R.J.List,ed.). That is, at sea level and 45.00 degrees latitude,

$$G(45) = 9.806160 \text{ m/s}^2.$$

At any other latitude,

$$G(\text{lat}) = G(45)(1 - 0.0026373 \cos(2*\text{lat}) + 0.0000059 \cos^2(2*\text{lat})).$$

To adjust for the altitude of observation,

$$G(\text{alt}) = G(\text{lat}) R_0^2 / (R_0 + H)^2,$$

where R0 is the radius of the earth at the latitude of observation and is given by

$$R_0 = 6378.388(1 - 0.0033670 \sin^2(\text{lat}) + 0.0000071 \sin^2(2*\text{lat})) \text{ km},$$

from the International Ellipsoid (Basic Physics of the Solar System, p.83, V.M.Blanco and S.W.McCuskey, Addison-Wesley, 1961).

Densities are then derived from the air temperature and pressures as follows:

$$D(\text{alt}) = (P(\text{alt}) * 100.) * M / (T(\text{alt}) * R), \quad \text{where}$$

D(alt) is the density at each altitude level (kg/m³),

P(alt) is the pressure at each altitude level (mbar),
(1 pascal = 100 mbar)

T(alt) is the temperature at each altitude level
(kelvin),

M and R are the mean molecular weight and the gas constant as defined above.

These data (altitude, temperature, pressure, density, and temperature error) are stored in the array, SONDE(5,70). In Subroutine SLANTA, SONDE is used in the computation of slant air mass above a given altitude and its rate of change with altitude. In Subroutine ALFEFF, SONDE is used in the computation of an average temperature, weighted by air density for the ten km above a given altitude, for use in obtaining the appropriate ozone absorption coefficient. In Subroutine OZDENS, temperature, temperature error, and pressure are stored in the SAVE arrays with the corresponding ozone data and are used in OZDENS, COMPST, and RELATD to convert ozone density to ozone partial pressure,

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the expression of ozone content in terms of mixing ratios and layer content, and in the estimation of errors of these derived ozone values.

ECC Sonde Observations

One or more ECC sondes are launched near the time of the Rocoz rocket launch, usually within an hour, before and after. This is a small payload suspended from a weather balloon, consisting of a standard rawinsonde with an ECC package attached. The data from the electrochemical cell (ECC) is inserted into the stream of rawinsonde data, with readings initiated by each successive closure in the microbaroswitch. The rawinsonde provides data on air pressure, air temperature, and humidity, with humidity data limited to the lower troposphere. Maximum altitude is limited by the burst altitude of the balloon, usually above 30 km. Altitudes are derived from the observations of temperature and pressure via the hypsometric equation; recent ECC flights have been radar tracked and these altitudes should be more accurate, especially at the higher levels. The ECC ozone values, expressed as partial pressure of ozone, have their greatest accuracy in the lower stratosphere, from the tropopause to no more than about 30 km. Some profiles show large excursions, usually due to the normal "layer-cake" structure of the ozone mixing ratios; occasionally there may be an excursion due, apparently, to the release of bubbles from the walls of the cell. A standard data reduction procedure for ECC's is in place at the Wallops Flight Facility, and reports are issued in a standard format, providing data at the microbaroswitch standard pressure levels as well as at each minute in flight.

In Subroutine CARDS of the Profile program, provision is made for entering data from two ECC sondes. The flight identification (8 characters) and launch date and time are stored in type -506. pedigree records. A "tie-on altitude" at an integer km level is chosen near the base of the Rocoz ozone profile and the corresponding ozone content (atm-cm) from ground level to this altitude, readily obtainable from the standard ECC data product, are likewise entered into Subroutine CARDS and stored in the -506. record. Next are entered data for 19 selected standard pressure levels, namely at 1000, 850, 700, 500, 400, 300, 250, 200, 150, 100, 70, 60, 50, 40, 30, 25, 20, 15, and 10 mbars. These data (altitude in km, ozone pressure in nanobars, air pressure in millibars, and air temperature in kelvin) are stored in the array, ECC, starting with the data for the 1000 mbar level as well as in the the type -506. and its continuation, type

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-507. pedigree records. Finally, Subroutine CARDS reads data for the ozone column content (atm-cm) from the ground up to 250, 125, and 62.5 mbar pressure levels storing these three values in ECCLM, for use in Subroutine RELATED. The ECC observations are generally the source of information for "base" values for use with the Datasonde profile.

For altitudes below the range covered by the Datasonde temperature-pressure profile, the Profile program uses air temperatures and air pressures from the ECC data. In Subroutine SLANTA air density is used in the computation of the slant air mass above various altitude levels. In Subroutine ALFEFF, air temperatures and densities are used in the computation of a weighted temperature so that a temperature-corrected ozone absorption coefficient may be obtained. In Subroutine OZDENS, air temperatures and air pressures are placed in the type 2xx. data records; the one-sigma error in ECC temperature is assumed to be 1.0 kelvin and the error in ECC pressure is assumed to be 0.7 mbar. In Subroutine CHECKS, the ozone column content between the ground and the "tie-on" altitude is added to that inferred from the Rocoz photometer, and the sum compared to the column content observed by the Dobson spectrophotometer. Finally, in Subroutine RELATD, tables are prepared for the user's convenience which include the ECC ozone content for standard layers and pressure levels.

Rocoz Photometer Observations

Raw data from the Rocoz photometer telemetry tape are digitized at the Wallops Flight Facility and processed by the RAW, EDIT, MERGE, and SMOOTH programs resulting in a SMOOTH tape, which is the input tape to the PROFILE program. The radar track of the photometer is likewise digitized at the Wallops Flight Facility, processed by the RADAR program, and combined with the photometer data in the MERGE program. The SMOOTH tape provides photometer current (counts) as a function of altitude and related information such as calibrations for instrument temperature and battery voltage, location of the sun, launch site and time, solar zenith angle, and noise content. Details of the tape formats and functions of the various programs are given in other sections of this document.

The SMOOTH tape is read by Subroutine TAPE. The Pedigree records are stored in the array, PED, for output to the Profile tape. The photometer data are placed in the array, SMOOTH(I,J,K), such that all data for S3 have subscript K=1, for S2, K=2, ...for S3/S0, K=4,...and for S1/S0, K=7. In Subroutine SECANG, the secant/Chapman-function is computed

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for the solar zenith angle at each altitude; details of this computation are given in the next paragraph. In Subroutine OZDENS the photometer values for two-km thick layers are interpreted in terms of the ozone density at the center of that layer and stored in the array SAVE. The method of computing ozone is given in the section on Ozone Algorithm. After all the data for the filter under consideration have been interpreted in terms of ozone densities, the results in SAVE are stored in the corresponding SMOOTH area for use later in the Profile program.

To convert column content from that in the slant path between the photometer and the sun to the corresponding vertical column content, the slant path content can be divided by the secant of the solar zenith angle. This is exact for a plane parallel atmosphere, but, for a spherical atmosphere, leads to error, particularly for solar zenith angles larger than 60 degrees. In Subroutine SECANG, if the cosine of the solar zenith angle is less than 0.5, approximations to the Chapman function are used for computation of the ratio of the vertical path to the slant path. The basic equations for the Chapman function and a table of values is given by S. Chapman (Proc. Phys. Soc., London, 43, 483-501, 1931); this discussion is extended and updated tables given in S. Chapman (Proc. Phys. Soc., London, B, 66, 710-712, 1953); a simplified form for the computation is provided by Fitzmaurice (Appl. Optics, 3, 640, 1954); the Fitzmaurice approximation was expressed in terms of a series expansion by K. Klenk of Systems and Applied Sciences Corporation (SASC), and described in their Sept. 1980 monthly report on Contract no. NAS5-25346, Task no. 41. The SASC expression for the Chapman function is

$$Ch = (X \pi/2)^{\frac{1}{2}} (a_1 t + a_2 t^2 + a_3 t^3 + a_4 t^4 + a_5 t^5)$$

with

$$X = (Re + h)/H, \quad t = 1/(1 + pY), \quad Y = (X/2)^{\frac{1}{2}} \cos z$$

where

Ch is the value of Chapman function,
 Re is the radius of the earth, km,
 h is the altitude above the spheroid, km,
 H is the scale height of component of interest, km,
 for both ozone and air, set to 5.0,
 z is the zenith angle,
 $\pi = 3.141593$,
 $a_1 = 0.254829$,
 $a_2 = -0.284496$,
 $a_3 = 1.421413$,
 $a_4 = -1.453152$,
 $a_5 = 1.061405$, and
 $p = 0.327591$.

The above expression is used if the cosine of the zenith

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angle is less than 0.2 (i.e. for angles greater than 78.5 degrees). For zenith angles between 60 and 78.5 degrees, a more simple approximation is used, namely,

$$Ch = (1. - T (1. - 3 T (1 - 5 T))) / \cos z$$

with

$$T = 0.5 \gamma^{-2}.$$

In the following table are given values for a precisely computed Chapman function at $X=1000$. for several different zenith angles and the values as computed by the above approximations. The precisely computed values are inferred from the tables provided by W. Swider Jr. and M. E. Gardner (On the Accuracy of Certain Approximations for the Chapman Function, AFCRL-67-0468, August 1967, 14p, Air Force Cambridge Research Laboratories, L.G.Hanscom Field, Bedford, Massachusetts)

Values of Chapman Function

zenith angle degrees	Chapman $X=1000$.	this $X=1000$.	this $X=1480$.	secant z
60.	1.994	1.992	1.994	2.000
70.	2.902	2.899	2.905	2.924
80.	5.590	5.598	5.643	5.759
90.	39.648	39.633	44.874	-----

Note that $X=1480$. corresponds to an altitude of 40 km and a scale height of 5 km.

Radar Tracks

Data for the radar track are digitized at the Wallops Flight Facility, smoothed by the Code 970 Eclipse computer (MESUP tape), converted to metric units by the RADAR Program, and merged with the Rocoz photometer data in the MERGE Program. Error in altitude for data from the WFF radars is assumed to be 10 m and is used in Subroutine OZDENS in the estimation of error in $d(\ln I)/dh$. Altitude error for observations at remote sites is probably larger.

Model Ozone Profile

A model ozone profile is provided by Subroutine MODEL for use in Subroutine SLANTA in its estimate of the ozone column above the top of the ozone profile from the Rocoz data under consideration, and, in Subroutine CHECKS, for comparison with the observed Rocoz ozone profile.

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Number densities (molecules m^{-3}) are from the mid-latitude, Northern hemisphere model provided in the U.S. Standard Atmosphere, 1976, based on an analysis by A. Krueger and R. Minzner and are stored in a DATA statement. Values are interpolated so as to provide an ozone number density at each km from 11 to 70 km. Subroutine MODEL assumes an overburden above 70 km of 5.35×10^{-6} atm-cm and infers the overburden at lower altitudes from the model density profile. To obtain the column content, the density is multiplied by 1.0×10^{-5} x 22.4136 liters per mole / 6.022169×10^{26} (Avogadro's number) and added to the column content at the previous altitude level. The total column above 0 km is 0.345 atm-cm. A more elegant method would be to use tables derived from satellite data to obtain a "first guess" profile appropriate for the latitude, season, and the column content as observed by the Dobson spectrophotometer.

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Effective Ozone Absorption Coefficient

Computations

Given values for the content of ozone and air in the slant path to the sun, characteristics of the filter, and the necessary reference tables, Subroutine ALFEFF returns values for the effective ozone absorption coefficient and the effective scattering coefficient.

The filter shape may be expressed in terms of its transmission as a function of wavelength. Such measurements have been made, in the past, at the Naval Weapons Center (NWC) at China Lake, California, and are now done at the Wallops Flight Facility. These tables may be read by Subroutine SHAPE and used in Subroutine ALFEFF to compute Aeff. The formulae are similar to those used by NWC as given by M. E. Hills and C. A. Flanagan (Calculation of Effective Ozone Absorption Coefficients for a Rocketborne Ozonesonde, NWC TP 5904, 41 pp, Naval Weapons Center, China Lake, Calif., March 1977). That is,

$$A_{eff} = \frac{-1}{X} \ln \frac{\sum I_0(L) Q(L) S(L) F(L) \exp(-A(L) X - B(L) M) dL}{\sum I_0(L) Q(L) S(L) F(L) \exp(-B(L) M) dL}$$

or for slant path ozone less than 1×10^{-5} atm-cm and slant air mass less than 0.01 atm, i.e., no overburden,

$$A_{eff} = \frac{\sum I_0(L) Q(L) S(L) F(L) A(L) dL}{\sum I_0(L) Q(L) S(L) F(L) dL}$$

where

- L is wavelength, at 0.1 nm intervals,
- I₀ is the flux of the sun at zero optical depth,
- Q is the detector responsivity,
- S is the diffuser transmission,
- F is the filter shape,
- A is the ozone absorption coefficient, per cm, base e,
- X is the slant path ozone overburden, atm-cm,
- B is the scattering coefficient, per atm., base e, and
- M is the slant path air mass, atm.

The ozone absorption coefficient is a function of temperature, particularly for wavelengths longer than about 270 nm. In Subroutine ALFEFF, a weighted temperature is computed, dependent on the air density for ten km above the altitude under consideration, and the ozone absorption coefficient interpolated at each wavelength from tables of the ozone absorption coefficient at several different temperatures.

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To obtain an effective scattering coefficient, a similar equation is used, that is,

$$B_{eff} = \frac{-1}{M} \ln \frac{\sum I_0(L) F(L) Q(L) S(L) \exp(-B(L) M) dL}{\sum I_0(L) F(L) Q(L) S(L) dL}.$$

The Solar spectral flux, Rayleigh scattering coefficients, ozone absorption coefficients, diffuser transmission, detector responsivity, and filter transmission tables are stored on disk and read by Subroutine INARRY. The diffuser transmission and detector responsivity are assumed to be the same for all photometers. The filter transmission is measured for each of the four filters in each photometer, and must be supplied for each flight. The filter shapes, for the flights up through RocoZ no. 315, are expressed only in terms of coefficients, and are read by Subroutine CARDS. For later flights, detailed filter shapes are also available, and may be read by Subroutine SHAPE.

Subroutine INARRY expects the disc data sets to have an initial 80-byte header followed by 1000 real numbers corresponding to wavelengths of 240.1 to 340.0 nm at 0.1 nm intervals. The header consists of 64 characters followed by 4 real (R*4) words. The real numbers are the range of wavelengths and the temperature, as applicable. The first part of the character string should identify the contents, including the parameter, the observer, and the date, as appropriate.

If McBride coefficients are available (not equal to zero), then Subroutine ALFEFF uses an approximation developed with NWC describing the dependence of Aeff on the ozone content of the slant path, namely,

$$A_{eff} = A_0 + 2. A_1 X + 3. A_2 X^2$$

where

X is the slant path ozone overburden, atm-cm,

A0 is the effective ozone absorption coefficient for no overburden, and

A1 and A2, as well as A0, are coefficients describing the change as a function of overburden.

The three coefficients, A0, A1, and A2, are obtained by computing Aeff for various overburdens and fitting the results to a polynomial, assuming that the effects of scattering on Aeff are negligible above about 20 km. The coefficients are part of the card (DATA5) input and are computed prior to running the PROFILE program.

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The effective scattering coefficient, B_{eff} , is set equal to value of B provided by the NWC analysis and is assumed to be constant over the range of air masses encountered in the reduction of the Roco observations. It is estimated that that the error due to this assumption is no more than 2% for altitudes above 20 km. The NWC analysis also provides the center wavelength and width at half height for each filter. These may be used, with the assumption of a gaussian filter shape, to estimate the effect of the temperature dependence on the A_{eff} .

Solar Flux

For both the solar flux and the ozone absorption coefficient, several different sets of data are available. For flights prior to no. 315, a "McBride" solar flux was used at the Naval Weapons Center (China Lake, California) in the computation of effective absorption coefficients for each filter. This is based on the average values for 0.1 nm intervals of the Furukawa compilation (Furukawa, P.M., P.L. Haagenson, and M.J. Scharberg, A composite, High-Resolution Solar Spectrum from 2080 to 3600 Å, NCAR-TN-26, 55p, 1967, National Center for Atmospheric Research, Boulder, Colorado) and is available as a disc data set for use with the Profile Program.

Rayleigh Scattering Coefficient

The Rayleigh scattering coefficient as a function of wavelength was likewise assembled by Dr. McBride and is available as a disc data set for use with the Profile Program.

Ozone Absorption Coefficients

The effective absorption coefficients computed by Dr. McBride were based on ozone absorption coefficients measured by E.C.Y. Inn and Y. Tanaka (Ozone Absorption Coefficients in the Visible and Ultraviolet Regions, Ozone Chemistry and Technology, Advances in Chemistry Series No. 21, pp263-68, 1959) for wavelengths shorter than 272 nm and from measurements at -44 C. reported by E. Vigroux (Contribution à l'étude expérimentale de l'absorption de l'ozone, Ann.Phys., 8, 709-62, 1953) for wavelengths longer than 290 nm, with an appropriate interpolation at intermediate wavelengths. This data set is available on disc for use by Subroutine INARRY. INARRY expects three sets of ozone

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absorption coefficients at three different temperatures (such as are expected to be available from the work of A. Bass). In Subroutine ALFEFF interpolation is made to obtain the ozone absorption coefficient corresponding to the air temperature weighted according to air density.

Diffuser Transmission

The transmission of the three stacked diffuser plates as a function of wavelength was measured a number of years ago, and the resulting curve has been used for all filters characterized by Dr. McBride. This is available as a disc data set for input to the Subroutine INARRY.

Detector Responsivity

The response of the detector was obtained many years ago (from the manufacturer ?), was used by Dr. McBride in his analyses, and is available as a disc data set for input to the Subroutine INARRY.

Filter Transmission

The shape of each filter (with the nickel sulfate hexahydrate crystal) is measured by means of a Cary 14 Dual Beam Spectrophotometer, and the measured transmission is used by Subroutine ALFEFF in the computation of the effective absorption coefficient.

For the filters calibrated in Dr. McBride's laboratory at the Naval Weapons Center(NWC), an NWC analysis provides the center wavelength and half-width, the effective absorption coefficient with no overburden (A0), and the coefficients, A1, A2, and B.

For the filters calibrated at the Rocoz Test and Calibration Laboratory at the Wallops Flight Facility, Subroutine SHAPE reads the data set containing the measured spectral transmission, and Subroutine ALFEFF computes effective ozone and scattering coefficients as a function of air temperature and air and ozone overburdens.

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Ozone Profile

Basis of Ozone Algorithm

The technique for converting the observed solar flux as a function of altitude to ozone content as a function of altitude was developed by Arlin Krueger (NASA, Goddard Space Flight Center) for use with his RocoZ photometer and was described in detail by Eugene Shaffer (Systems and Applied Sciences Corporation) in a draft report. This discussion is based primarily on that report, but adds the details of its implementation in the Profile Program.

The reduced RocoZ data consist of a flux of ultraviolet light in four different wavelength bands as a function of altitude. The wavelength bands are chosen over a range of ozone absorption coefficients. To compute the ozone profile, the following assumptions are made:

1. Dust particles cause a negligible attenuation of the direct sunlight.
2. No other absorbers are present in the stratosphere for the four wavelength bands.
3. Above 20 km, the diffuse component of the sunlight can be ignored.

With the above assumptions in mind, the intensity of the sunlight as a function of altitude can be written, using Beer's law, as

$$I(L,h) = I(L,\infty) \exp [A(L)u(h) - B(L)m(h)] \quad (1)$$

Where: $I(L,h)$ is the intensity at height h ,
 $I(L,\infty)$ is the intensity at top of the atmosphere,
 $A(L)$ is the ozone absorption coefficient,
 $u(h)$ slant path ozone from h to the sun,
 $B(h)$ Rayleigh scattering coefficient,
 $m(h)$ optical air mass between h and the sun,
 L is wavelength, and
 h is altitude.

Equation (1) can be rewritten as

$$\ln I(L,h) - \ln I(L,\infty) = -A(L)u(h) - B(L)m(h).$$

An expression for the ozone concentration at each height interval can be derived by differentiating the above expression with respect to altitude.

$$d \frac{\ln I(L,h)}{dh} = -A(h) \frac{du(h)}{dh} - B(h) \frac{dm(h)}{dh} \quad (2)$$

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The monochromatic ozone absorption coefficient and Rayleigh scattering coefficient must be replaced by effective coefficients which are now a function of the slant path total ozone and the air mass amounts.

A(L) is replaced by Aeff(u,m)
B(L) is replaced by Beff(u,m)

Effective coefficients are used because the optical filters have bandwidths wide enough that the wavelength dependence on various input parameters must be recognized. The slant path ozone amount, (u), and the optical air mass amount, (m), modify the spectral shape of the solar flux as a function of height.

The effective coefficients are substituted into equation (2) to yield

$$\frac{d \ln I(L,h)}{dh} = -A_{eff} \frac{du}{dh} - \frac{d(A_{eff})}{du} \frac{du}{dh} u - B_{eff} \frac{dm}{dh} \quad (3)$$

Equation (3) is rewritten to represent du/dh, the total amount of ozone in the height interval.

$$\frac{du}{dh} = \frac{-1}{A_{eff} + \frac{d(A_{eff})}{du} u} \left\{ \frac{d \ln I(L,h)}{dh} + B_{eff} \frac{dm}{dh} \right\} \quad (4)$$

Finite differences may be substituted for the derivatives, and equation (4) now can be solved iteratively for ozone amounts at any height level in the range of the Rocoz data.

The implementation of this solution in the Profile Program makes use of the following:

- The magnitude of the solar flux at the wavelengths of interest at any given altitude is taken to be proportional to the current from the photodiode detector as adjusted by the Rocoz electronics for variations in the flux at longer wavelengths entering the photometer, that is, I is proportional to the number of counts transmitted by the telemetry system for any particular filter. The constant of proportionality is not important since the difference of the logarithms is the parameter that is used.

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- One way to represent the effect on the ozone absorption coefficient is to use a quadratic function:

$$A_{\text{eff}}(u,m) = A_0 + A_1 u + A_2 u^2 + B_1 m + B_2 m^2$$

At typical rocket heights (20-60 km) the fourth and fifth terms in equation (3) are negligible due to the small air mass and are ignored in this discussion. The effective Rayleigh scattering term can be considered a linear function of the optical air mass. For heights of 20 to 60 km we represent the effective Rayleigh scattering as a constant, which for the filters in use here will have an error of no more than 2%. The constants in the quadratic equation may be calculated through use of the measured filter shape, solar spectrum, ozone absorption coefficients, Rayleigh scattering coefficients, and the spectral response of the Rocoz photometer, together with various assumed ozone and air overburdens. These constants have been calculated by Dr. William R. McBride for the filters that have been calibrated at the Naval Weapons Center at China Lake, California, and are available for use in the analysis of the Rocoz data for flights through 1982.

- It is noted that dm/dh is simply (air density x secant solar zenith angle).
- The Profile Program will process the Rocoz photometer data in terms of the observed count for each of the four filters (S3, S2, S1, and S0) or in terms of the ratio to the S0 filter (S3/S0, S2/S0, S1/S0). The use of ratios is preferable if there is appreciable common mode noise and/or if there is a change in the responsivity of the photometer as a function of time in flight.
- The range of altitude for each filter is chosen prior to running the Profile Program; it generally corresponds to optical depths between 0.05 and 3.0 and depends on the availability and quality of data, that is, both radar and telemetry data must be available, telemetry dropouts must be minimal, the attitude of the Rocoz must be reasonably stable, and the solar zenith angle should be less than 60 degrees. Data for solar zenith angles up to about 80 degrees can be processed, but the accuracy of the resulting ozone densities becomes increasingly uncertain.

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Implementation of the Ozone Algorithm

The RocoZ data is interpreted in terms of ozone densities by the Profile Program in subroutine OZDENS. The evaluation involves three altitude levels, spanning a total of 2 km, namely, top (T), center (C), and bottom (B), with the differentials evaluated for a layer centered at C. In the initial evaluation, estimates are used for ozone densities and ozone overburdens. After the initial evaluation of the ozone density at C, these estimates are updated and the ozone density at C recomputed until the change in the ozone density compared to its previous value is less than 0.1 %.

The steps necessary to interpret the input data are as follows:

1. The top (ALTT), center (ALTC), and bottom (ALTB) altitudes are identified, beginning with ALTT in km as provided in the array TOP, and ALTC and ALTB one and two km lower, respectively. After the determination of the ozone density at ALTC, ALTT, ALTC, and ALTB are each decremented by one km, ending with the layer for which ALTB corresponds to the value given in the array BASL.
2. SLANTA is called to provide the slant air mass (ASLTT, ASLTC, ASLTB) above each of the three altitudes and its rate of change evaluated at the center altitude (DMDHC). Slant air mass is in atmospheres. DMDHC is in atmospheres per km.
3. The rate of change of the natural logarithm of the intensity, $d(\ln(I))/dh$, (DLIDH) is evaluated from the observed intensity (or ratio to S_0) corresponding to ALTT and ALTB, the top and bottom of the three layers under consideration.
4. Estimates of the slant ozone overburden (UT, UC, UB) are made for each of the three altitudes. Initial estimates are taken from the model ozone profile contained in the array STD. Ozone values inferred from the rocket flight are used in the estimates for succeeding levels. Ozone overburden is in atm-cm.
5. Values at each altitude for the effective ozone absorption coefficient (ALFAT, ALFAC, ALFAB) and the effective Rayleigh scattering coefficient (BETAT, BETAC, BETAB) are obtained from subroutine ALFEFF.

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6. The slant ozone content between ALTT and ALTB in atm-cm (DELU) is computed using equation (5) and saved as (PDELU).
7. DELU is used to recompute the slant ozone for the bottom layer (UB), ALFAB and BETAB are recomputed, ALFAC is taken as the average of ALFAT and ALFAB, and BETAC is the average of BETAT and BETAB.
8. Steps 6 and 7 are repeated until DELU is within 0.1% of PDELU, usually requiring but one iteration.
9. Ozone density at ALTC is then $0.5 * \text{DELU} / (\secant \text{ of the solar zenith angle})$, in atm-cm/km.
10. The ozone density and a number of related values are saved in the type 1xx. and 2xx. Profile data records.
11. Steps 1-10 are repeated at the next lower altitude level until the range for a particular filter is completed.
12. Steps 1-11 are repeated for the next filter until all seven possibilities have been considered.

Profiles from Each Filter

As the ozone density is obtained at each altitude level from each filter (or from its ratio to the SO data) two data records are created and are included on the Profile Tape. (See the type 1xx. and 2xx. data records described in the chapter on Tape Formats.) The first record contains relevant parameters taken from the Smooth Tape and various elements calculated in the course of obtaining the ozone density. The second record is devoted to atmospheric parameters, that is, ozone values, air pressure and temperature, and associated errors. Selected values from these records are printed as tables.

PROFILE PROGRAM

Composite RocoZ Profile

The RocoZ photometer contains five filters, referred to as S0, S1, S2, S3, and Compensation, with S3 having the shortest center wavelength, S2, S1, and S0 at longer wavelengths, and the Compensation filter at an even longer wavelength for which the ozone absorption coefficient is very small. The signal from the detector with the Compensation filter is used as the reference in an automatic gain control system to continually change the gain of the amplifier for the detector associated with the S0-S3 filters, compensating for changes in total light input such as those due to changes in the direction of the axis of the photometer with respect to the sun.

Ozone profiles are derived independently from the data from each of the four filters (S0, S1, S2, S3). Each profile covers an altitude region of 10 to 25 km, usually with some overlap in altitude coverage. In Subroutine COMPST these independent profiles are combined to form a single profile attributable to this RocoZ flight. To obtain this composite profile, all available data for a particular altitude level are weighted by the inverse of the associated error and averaged. Ozone densities derived from filter ratios are not included.

For the convenience of the user, the ozone density profile is expressed in both atm-cm/km and number/m³ and is collated with air temperatures and pressures based on the Datasonde and the ECC sonde. In Subroutine CHECKS, the column content (atm-cm) at each altitude level is computed, based on an initial column content above the top level of the ozone profile taken from the ozone model (Subroutine MODEL), and integrating downward.

In Subroutine CHECKS the Composite data are used in a series of consistency checks before filling the remainder of the array with computed partial pressures and mixing ratios.

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Consistency Checks

To aid in estimating the quality of the data from a Rocoz flight and related observations, the data are checked for internal consistency. These checks include (1) comparison of the profiles from the various filters with each other, (2) comparison of the composite profile with a model, (3) comparison of the ozone column content measured by the Dobson spectrophotometer with the sum of the columns observed by the Rocoz photometer and the ECC sonde, (4) comparison of the slope deduced in the Smooth Program over a variable height interval with that deduced in the Profile Program over a 2 km interval, (5) comparison of the variations of the Compensation channel with those expected due to changes in solar zenith angle and overhead air mass, and (6) the drag coefficient as a function of altitude and Reynolds number.

The following discussion gives the basis for each check and the significance of the results.

Overlap Analysis

One way to examine the accuracy and precision of the ozone densities is to compare the profiles obtained from the different filters. In Subroutine COMPST data for the various filters are transferred to a single table; Subroutine CHECKS calls Subroutine OVERLP to systematically compare the data from the various filters and to compare data from a particular filter to data derived from the ratio of that filter to the S0 filter. For each of the 21 possible combinations, the two altitude profiles are compared by fitting the pairs of points to a straight line (Subroutine LINFIT), and computing its slope (B) and zero intercept (A), i.e.,

$$O3(\text{filter } y) = A + B \ O3(\text{filter } x).$$

One would look for a zero intercept that is small compared to the ozone value at the maximum altitude of the set of points, for a slope that is near 1.0, and for a correlation coefficient (R) that is near 1.0. An examination of the table may reveal whether one of the filters has substantially changed its spectral transmission since its calibration. Values of B that are markedly different from 1.0, but similar from flight to flight may indicate that one or more of the spectral data sets (solar flux, absorption coefficients, etc.) is not correct. One would expect that the values for A, B, and R for a filter paired with its ratio (e.g. S3 compared to S3/S0) would be very close to ideal.

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Comparison with Model

The ozone density and overburden (vertical column) as a function of altitude from the Rocoz Composite profile are compared with the values provided by Subroutine MODEL. Currently the model is for mid-latitudes and is from the U.S. Standard Atmosphere, 1976. It would be desirable to upgrade Subroutine MODEL to provide a profile that is typical of stated latitude and season, such as might be obtained from the analysis of global ozone data sets. Subroutine CHECKS computes the differences and prepares a table of the results.

One would expect most data from Wallops Island to be relatively close to the mid-latitude model, within the variability stated in the tables given in the U.S. Standard Atmosphere, 1976.

Total Ozone

The total ozone (vertical column content) is observed by the Dobson Spectrophotometer and may also be deduced from a combination of the ECC and Rocoz Composite profile. The ECC values are generally considered to be relatively accurate below the ozone density maximum. The Rocoz profiles are better at the higher altitudes.

From a preliminary examination of the data, a "tie-on" altitude is chosen, usually between 18 and 25 km; the column content from the ground to the "tie-on" altitude is obtained from the ECC data report and entered into the Profile Program (Subroutine CARDS). In Subroutine CHECKS, the column content above the "tie-on" altitude is obtained from the Rocoz Composite ozone profile. Errors are assumed to be 7% for the Dobson total ozone; 10% for the ECC segment, and as derived in the Profile Program for the Rocoz segment. The two segments are added, the associated errors derived, and the difference from the Dobson total is noted.

The two observations of total ozone should agree within their estimated errors. If the difference is larger, it may indicate temporal and spatial variability of ozone (particularly if maps from TOMS, the total ozone mapping spectrometer on Nimbus-7, indicate a substantial gradient in that area). A large difference may also indicate that one or more of the three systems involved did not perform as expected and has as yet unidentified errors. This check is sensitive only at altitudes where the ozone density is large, that is, in the lower stratosphere.

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Estimations of Slope

In the Smooth Program, all points in the vicinity of each integer altitude are considered, and a value of the intensity (I, number of counts) representative of that level is derived. The number of points considered range between 100 and 800; the altitude interval ranges between 1 and 9 km. In the process, a line of the form, $\ln(I) = A + B(h-h_b)$, is used, and the intercept (A) at the base altitude (h_b) and the slope (B) are calculated; A and B are then used to obtain the intensity at the altitude level under consideration.

In Subroutine OZDENS of the Profile Program, $d \ln(I)/dh$ is obtained by taking differences over a 2-km interval. For ideal data, the two values should be the same, at least within the error associated with each. Larger differences are probably related to the differing altitude resolution, but should be examined individually.

Variation of the Compensation Channel

A fraction of the light entering the Rocoz instrument is diverted through a Compensation filter to a separate detector. This is a relatively broad-band filter centered at about 375 nm, where the ozone absorption coefficient is several orders of magnitude less than that for the S0 filter. Variation of the signal from the detector is due primarily to changes in the angle of the sun with respect to the optical axis of the photometer, but is also affected by the amount of light scattered out of the optical path by molecules and aerosols. In the Smooth Program, the value of the Compensation signal is averaged over 99 filter rotations. In Subroutine CHECKS of the Profile Program, the average value (after taking into account changes in solar zenith angle) between 35 and 50 km is determined; the expected value at lower altitudes is computed, again taking into account the changes in solar zenith angle and, in addition, the loss of light expected due to Rayleigh scattering. The fractional loss is estimated by the method developed by R.W.Fraser (NASA/GSFC, quoted (incorrectly) in Thomas, R.W.L., W.A.Pearce, A.H.Holland, and D.U.Wright, Appl. Optics, 21, 2436-2441, 1982). The correct formula is:

$$f_c = 0.376 (\sec z)^{0.874} 10^{-h/16}$$

where

f_c is the fraction of light scattered out of the path,
 z is the solar zenith angle, and
 h is the altitude in km.

Differences between the predicted and the observed values of

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the average Compensation signal may be due to scattering by aerosols, changes in temperature of the photometer, or large (more than 60 degrees) solar zenith angles.

Drag Coefficient

The photometer is suspended from a Starute decelerator, deployed after ejection from the rocket body. The drag coefficient of the Starute and photometer can be computed using

$$C = (g - a) / (2 d v^2 A)$$

where

- C is the drag coefficient,
- g is the acceleration due to gravity,
- a is the observed vertical acceleration,
- d is air density,
- v is the observed vertical velocity, and
- A is the effective area of the Starute.

Because drag is a function of Reynolds number, this also is calculated and listed. That is,

$$Re = v D d / m$$

where,

- Re is the Reynolds number,
- D is the characteristic size,
- m is the dynamic viscosity, and
- d and v are as defined above.

The dynamic viscosity is computed by use of the formula given in the U.S. Standard Atmosphere, 1976, (p.19),

$$m = B T^{3/2} / (T + S),$$

where,

- B is a constant, equal to 1.458×10^{-6} kg/(s m K^{1/2}),
- T is temperature in kelvin, and
- S is Sutherland's constant, equal to 110.4 K.

The drag coefficient should vary smoothly as a function of Reynolds number. The observed values increase from about 1 near Apogee to about 1.4 near 20 km. This increase is similar to that for a sphere at similar Reynolds numbers. A substantial deviation from the smooth increase with decreasing Reynolds numbers could indicate problems in the altitude versus time data; A decrease in the magnitude of the drag coefficient could be due to a damaged Starute.

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Derived Ozone Values

The RocoZ data as analyzed in this set of programs is interpreted in terms of ozone density as a function of geometric altitude. Although expressed at 1 km intervals, the smoothing interval varies from 3 km at low altitudes to about 9 km near the top of the profile. The density profile is integrated from the top down to obtain the column content as a function of altitude.

For the convenience of the user, the ozone content is also expressed in other commonly used units, that is, as partial pressure, as mixing ratio, as layer content, and with altitude expressed in terms of pressure level. The associated error increases because it is necessary to use the observed air temperatures and pressures in the transformation of units, and the errors in such observations must be considered.

Column Content

The slant ozone (ozone in the path between the photometer and the sun) and the ozone overburden (vertical column above the photometer) are computed in Subroutine OZDENS and given to Subroutine ALFEFF for use in the computation of the effective ozone absorption coefficient. The initial value (at the highest altitude for which there is useful photometer data, that is, 1 km above the top altitude of the RocoZ ozone profile) is obtained from the model profile provided by Subroutine MODEL. Values of slant ozone at lower levels are obtained by adding the observed layer content. The vertical column for each level is obtained by dividing by the secant/Chapman-function of the solar zenith angle at that level, as provided by Subroutine SECANG. These values are computed independently for each filter, i.e., the initial slant ozone used in deriving an ozone profile from the S2 filter is taken from the model profile, not from the profile obtained by use of the S3 filter. The values used in the computations are included in the type 1xx. and 2xx. data records created by the Profile Program.

After ozone profiles are obtained corresponding to each of the filters of the photometer, a Composite RocoZ ozone profile is generated by Subroutines COMPST and CHECKS, as described in an earlier section of this document, and included in the type 300. data records. The initial value of the ozone overburden here is that from the ozone model, multiplied by the ratio of the ozone density in the Composite profile to that in the model profile. The density for each lower level is obtained by assuming the density in

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the 1 km layer is the average of the density at its top and base, and adding the layer content to the overburden already available for the top of the layer. These overburdens are the ones used by Subroutine CHECKS for comparison with the model overburdens and the Dobson total ozone observations.

Partial Pressure and Mixing Ratios

The ozone algorithm as implemented in Subroutine OZDENS expresses the ozone density at a given altitude level in terms of atm-cm/km. The following formulae are used in Subroutines OZDENS, CHECKS, and RELATD to express the ozone density in other units:

$$\begin{aligned}O(\#) &= O(\text{ack}) \times 10^{-5} \text{ A} / \text{V} \\O(\text{nb}) &= O(\text{ack}) \times 0.1 \text{ R}^* \text{ T} / \text{V}, \\O(\text{vmr}) &= O(\text{nb}) / \text{P}, \\O(\text{mmr}) &= 1.65714 \text{ O}(\text{vmr}),\end{aligned}$$

where

$O(\#)$ is ozone density in number/ m^3 ,
 $O(\text{ack})$ is ozone density in atm-cm/km,
 $O(\text{nb})$ is ozone density in nanobars,
 $O(\text{vmr})$ is ozone volume mixing ratio, parts per million,
 $O(\text{mmr})$ is ozone mass mixing ratio, parts per million,
 P is air pressure, millibars,
 A is Avogadro's number, 6.022169×10^{26} molecules/kmol,
 R^* is universal gas constant, $8314.32 \text{ N m} / (\text{K kmol})$,
 T is air temperature, kelvin, and
 V is volume of ideal gas at STP, $22.4136 \text{ m}^3/\text{kmol}$.

Content of Standard Pressure Layers

To facilitate the comparison of the Rocoz/ECC profiles with those from other sources, Subroutine RELATD prepares a table of layer contents, based on the Composite Rocoz profile and, at the lower altitudes, on the concurrent ECC sonde. Layer boundaries are expressed in milliatmospheres beginning at 1000 matm with the upper boundary at one-half the pressure of the lower boundary. The topmost layer is from 0.24 - 0 milliatm. The layer's ozone content (in milliatmosphere-cm) is the difference of the ozone overburdens at the layer boundaries, as interpolated from the data in the Rocoz Composite ozone table. The ozone content for layers for which the Rocoz profile is not complete is set to 0.

At altitudes in the troposphere and lower stratosphere, layer content is derived from the ECC sonde that was launched near the time of the Rocoz launch, using the column contents given in the ECC tabular listings.

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Ozone Values at Standard Pressure Levels

At 33 standard pressure levels ranging from 1000 mbar to 0.05 mbar, Subroutine RELATD displays ozone number densities interpolated from the RocoZ Composite profile and the ECC sonde, air temperatures from the Datasonde and the ECC sonde, geometric altitude at each pressure level, and the ozone mass mixing ratio. Where the various data sets overlap, two sets of temperature, ozone density, and mass mixing ratio are included. The standard pressure levels are at decimal multiples of 10, 15, 20, 30, 40, 50, and 70, and also include 250 and 850 mbar.

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Estimation of Errors

There are many sources of uncertainty which affect the ozone profiles obtained through use of observations from the Rocoz photometer, and the associated Datasonde, ECC sonde, and Dobson spectrophotometer. Besides errors related to the Rocoz photometer, there are temperature sensor errors, altitude (radar) errors, pressure (microbaroswitch or hypsometer) errors, and uncertainties due to atmospheric variability (air temperature, air pressure, and Rocoz photometer observations are not from the same vehicle), variability in aerosol content, and solar variability.

The error in the ozone density derived from the Rocoz photometer depends on the accuracy of the various tables used in the computation of the effective ozone absorption coefficient: the ozone absorption coefficient and its temperature dependence, the solar flux, the Rayleigh scattering coefficient, and the measured filter transmission, diffuser transmission, and detector responsivity. The error in the ozone densities also depend on the effectiveness of the compensation scheme, detector noise, noise introduced by the in-flight digitization, noise introduced by the telemetry and recording systems, the accuracy of the radar tracks, and approximations and assumptions made in the course of the data reduction.

The Profile Program attempts to evaluate many of these errors. However, it does not characterize errors in the computation of the effective ozone absorption coefficient, except as can be done by comparing the ozone densities from the different filters. Most errors are expressed as percent and all represent the one-sigma value.

Irradiance as a Function of Time

In this scheme of data analysis, the observed irradiance is always expressed in arbitrary units; no attempt is made to convert the arbitrary units to absolute fluxes. Ozone content is obtained by using the ratio of the radiance observed at the top of a chosen layer to that observed at the base of that layer and hence is independent of the absolute values of the radiances. The unit of irradiance is the number of counts (0 - 1000) at the input of the Rocoz telemetry transmitter and represents the solar flux received on a horizontal plane located at the altitude of the photometer.

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The errors in irradiance are handled in three different ways, depending on the time scale. The first group of errors have periods of well under one second, the second group have periods on the order of 1 to 100 seconds, and the last group are drifts over the 20 minutes of the flight.

The first group of errors relate to the determination of the value of a single observation. The output of the photodiode is sampled at precisely the time at which the filter is fully in the optical path and is held electronically for one rotation of the filter wheel. During approximately 600 ms required for one rotation, the signal on hold is sampled about 55 times. The design of the electronics restricts the decay of the signal to less than one count; the analog-to-digital conversion is designed to have an accuracy of ± 1 count. The extent of the decay and the short-term random component of the a/d conversion can be checked by a visual inspection of the listing of the telemetry data. Noise in the photometer electronics may correspond to several counts and noise introduced during the telemetry transmission and recording may be as much as full scale. In Subroutine AVG of the Edit Program, it is required that at least half of the samples be within 6 counts of each other, the remainder are discarded, and an average is taken of the selected values. Otherwise a dummy value (-99.) is used to indicate that no value is available for this filter for this rotation. No estimate is made of the error attributable to these sources alone.

The next group of errors are of somewhat lower frequency and are due primarily to low frequency components in the noise inherent in the photodiode and its current amplifier, to noise in the compensation circuitry, and possibly due to less than perfect optics such that azimuth dependent components may be present in the observed irradiance. In the Smooth Program, a value of the irradiance at each integer altitude is obtained from consideration of a number of observations in the vicinity of that altitude. The minimum number of points assembled by Subroutine SELECT is 100; the minimum altitude range is 1 km; at high altitudes the 100 points correspond to an altitude interval of about 8 km; at low altitudes several hundred points may be needed to cover one km altitude. In Subroutine LOGFIT, a straight line of the form, $\ln I = A + B (H - H_b)$, is fitted to this array of points and values of A and B (with standard deviations) are obtained. Here, I is the irradiance in terms of counts, H is the altitude of the point under consideration, and H_b is the lowest altitude in the interval under consideration. The irradiance at the integer altitude level is then computed using the computed values of A and B. This value of irradiance, A, B, the altitude bounds, and the

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standard deviations associated with A and B (σ_A and σ_B) are written on the Smooth Tape for input to the Profile Program. In Subroutine OZDENS of the Profile Program, the standard deviation of $\ln I$, $s_{\ln I}$, is computed using the formula, $s_{\ln I} = (\sigma_A^2 + (\sigma_B(H-H_b))^2)^{1/2}$. The error associated with the difference of $\ln I$ at the top and the base of the 2-km layer under consideration is then the rms sum of the errors associated with each $\ln I$.

The third group of errors are slow drifts that may be appreciable during the 15 to 30 minutes required for the Rocoz photometer to drop from its ejection altitude to near the tropopause (or over the horizon such that telemetry signals are no longer received). This includes changes in photodiode responsivity due to changes in temperature or length of time in operation, drifts in the zero level of the electronics, or slow changes in the absolute calibration of the a/d converter. One way of detecting some of these changes is to compare the ozone derived from the signal from a particular filter to the ozone derived from the ratio of that filter signal (counts) to the signal from the S0 filter, which is at a wavelength for which the ozone absorption coefficient is relatively small. In Subroutine OVERLP of the Profile Program, a comparison is made between the two profiles.

Altitude

The error associated with the radar data from the Wallops Flight Facility is stated to be 60 ± 30 feet. In Subroutine OZDENS of the Profile Program, the error in altitude is set to 20 m; this error, expressed in percent, is placed in the type 2xx. data record. The error in the vertical thickness of the layer under consideration is set to 14 m.

Air Temperature

Air temperature is obtained from the Datasonde at altitudes above about 20 km and from the ECC sonde at the lower altitudes. The error in the Datasonde temperatures is typically one degree but increases rapidly above 55 km, reaching 15 degrees at 70 km. To this must be added the uncertainty due to atmospheric variability. The formulae used for this is given in the earlier section on Datasonde Observations. The result, expressed in percent, is placed in the type 2xx. data record.

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At altitudes below about 20 km, air temperature is obtained from the meteorological sonde to which the ECC sensor is attached. The one-sigma error is assumed to be one kelvin.

Air Pressure

Air pressure is obtained from the meteorological sonde to which the ECC sensor is attached and is assumed to have an error of 0.7 mbar. At altitudes above about 20 km, pressures are derived from a "base pressure" and the datasonde temperature profile, as described in the earlier section on Datasonde observations. The error in the base pressure is that of the ECC sonde pressure plus errors due to atmospheric variability and in matching altitude levels; the error in base pressure is assumed to be 1 mbar. At higher altitudes the effect of temperature errors must be added to this. These estimates are made in Subroutine OZDENS, expressed as percent, and placed in the type 2xx. data records.

Ozone Density

In Subroutine OZDENS the error in the ozone density is set to the rms sum of the error in $d(\ln I)$ and the error in layer thickness, all expressed in percent and the value placed in the type 2xx. data record.

In Subroutine COMPST, the profiles from the individual filters are combined to provide a composite profile. At each altitude level the available values from the four filters are weighted inversely by the associated error. That is,

$$\begin{aligned}\text{Composite error} &= \text{sum}(1./\text{err}(i)) && \text{and} \\ \text{Composite density} &= \frac{\text{sum}(\text{density}(i)/\text{err}(i))}{\text{sum}(\text{err}(i))}\end{aligned}$$

where i refers to the values available at each level. The resulting composite density and error are placed in the type 300. data records.

Ozone Overburden

For the Composite data set, in Subroutine COMPST, the initial overburden is obtained by adjusting the column content given in the Ozone Model to the density at that level in the Composite profile. That is, at the top level,

$\text{Col}(\text{comp}) = \text{Col}(\text{model}) * \text{Density}(\text{comp}) / \text{Density}(\text{model})$
The error associated with this is the rms sum of the Composite density error and the estimated error in the scale

PROFILE PROGRAM

height of the model; this latter error is assumed to be 15%. The column content at the next lower level is obtained by adding the average density in that layer to the column at the top of the layer. The error at this level then is the rms sum of the error (in atm-cm) of the column at the top of the layer and the errors in the densities in the top half and bottom half of the layer. The column error is then converted to percent and stored in the type 300. data record.

Ozone Partial Pressure and Mixing Ratio

In Subroutine CHECKS the Composite data set is completed by computing the ozone partial pressure and volume mixing ratio. The error associated with the partial pressure is the rms sum of the percent errors in the ozone density and the air temperature. The error associated with the volume mixing ratio is the rms sum of the percent errors associated with the ozone partial pressure and the air pressure. The Composite data set is then transferred to the type 300. data records.

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Common Areas

The Profile Program uses seven named common areas to facilitate sharing of data among the various subroutines. The contents of each common area are described in this section. All variables are real (R*4) or integer (I*4) according to the usual naming convention, except where specifically indicated otherwise. The seven named common areas are SETUP, PROFLS, FSHAPE, CONSTT, DATAIN, COEFTS, and DATOUT.

COMMON/SETUP/TAPEIN,TAPOUT,NFIN,NFOT,INCLD(7),TOP(7),
BASE(7)

TAPEIN	R*8	Input Tape Volume Identifier
TAPOUT	R*8	Output Tape Volume Identifier
NFIN		File Number on input tape
NFOT		File Number on output tape
INCLD	(1)	03 process S3 filter
	(2)	02 process S2 filter
	(3)	01 process S1 filter
	(4)	00 process S0 filter
	(5)	30 process S3/S0 data
	(6)	20 process S2/S0 data
	(7)	10 process S1/S0 data
		any negative number - ignore this filter
TOP		highest altitude to be processed, km
BASE		lowest altitude to be processed, km

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COMMON/PROFLS/DSB(3),MXSND,NECC(2),ECCLM(3,2),SONDE(5,70)
ECC(4,19,2),STD(3,60)

DSB	(1)	base altitude, km, for use with Datasonde
	(2)	temperature (kelvin) at base altitude
	(3)	air pressure (mbar) at base altitude
MXSND		index of lowest altitude in SONDE
NECC		number of rows in ECC for each of 2 sondes
ECCLM	(1,x)	ozone column (atm-cm) up to 250 mbar
	(2,x)	ozone column (atm-cm) up to 125 mbar
	(3,x)	ozone column (atm-cm) up to 62.5 mbar
SONDE		for each altitude, starting at highest alt
	(1,x)	altitude, km, for Datasonde
	(2,x)	air temperature, kelvin
	(3,x)	air pressure, mbar, hypsometric value
	(4,x)	air density, derived from T and P, kg/m^3
	(5,x)	error, one sigma, in air temperature, k
ECC		data at standard pressure levels from ECCs beginning at 1000 mbar
	(1,x,y)	altitude, km
	(2,x,y)	air temperature, kelvin
	(3,x,y)	air pressure, mbar
	(4,x,y)	ozone partial pressure, nanobar
STD		values from model ozone profile
	(1,x)	altitude, km, starting at 70 km
	(2,x)	ozone number density, molecules/m^3
	(3,x)	ozone overburden, atm-cm

COMMON/FSHAPE/CW(7),BW(7),CMCBRD(4,7)

CW		center wavelength, nm, for each filter
BW		bandwidth at half-height, each filter
CMCBRD	(1,x)	λ_0 as given by NWC, McBride calibration
	(2,x)	A1 "
	(3,x)	A2 "
	(4,x)	Beta "

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COMMON/CONSTT/AVOGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,
RZRO

AVOGAD	6.022169 ²⁶ molecules, Avogadro's number per mole
VOLSTP	22.4136 liters per mole
RSTAR	8314.32 N m/(kmol K), universal gas const.
DGTORD	1.745329 ⁻² radians per degree
GRV45	9.806160 m/s ² acceleration of gravity at 45 degrees latitude
AIRM	28.964 kg/kmol, molecular weight for air
GRV	m/s ² accceleration of gravity at latitude of launch site
RZRO	km, radius of earth at latitude of launch

COMMON/DATAIN/NLAYRS,SECSZA(60),SMOOTH(20,60,7)

NLAYRS	number of altitude layers used in SMOOTH
SECSZA	secant/Chapman-function of solar zenith angle for each layer
SMOOTH	all of the data records from the Smooth tape, separated by filter Note that in Subroutine OZDENS, the Smooth records are replaced by the Profile data records for each filter

COMMON/COEFTS/GAMM(1000),BETA(1000),ABSZ(1000),ABST(800,2)

GAMM	product of solar flux, diffuser trans- mission, and detector responsivity from 2401 to 3400 angstroms
BETA	Rayleigh scattering coefficient, 2401-3400
ABSZ	ozone absorption coefficient, 2401-3400 A at room temperature
ABST	ozone absorption coefficient, 2601-3400 A at two lower temperatures

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COMMON/DATOUT/NSAV,PED(20,30),SAVE(20,60)

NSAV	The number of records in PED or SAVE to be written to the Profile output tape
PED	All the Pedigree records read from the Smooth tape or created in Profile
SAVE	Data records created by Profile Program

In Subroutine COMPST, this area is reassigned thus:

COMMON/DATOUT/NSAV,NDXTOP,NDXBAS,NLVLS,DM(17),WORK(20,89)

In Subroutines RELATD and PRTWRT, this common area is described as follows:

COMMON/DATOUT/NSAV,NDXTOP,NDXBAS,NLVLS,DM(10),DOBTM,DOBAM,DOBPM,PMDL(2),ECTIE,ECCOL,WORK(20,89)

NSAV	
NDXTOP	index in WORK or COMP (see below) for top of Rocoz ozone profile.
NDXBAS	index for lowest altitude of Rocoz profile
NLVLS	
DM(1)	Rocoz launch date, MMDDYY.
DM(2)	Rocoz launch time, HHMMSS.S
DM(3)	launch latitude, \pm degrees
DM(4)	launch longitude, degrees EAST
DM(5)	Rocoz flight number xxx.x
DM(6)	
DM(7-10)	launch site, EBCDIC characters
DM(11) DOBTM	date of Dobson observations, MMDDYY.
DM(12) DOBAM	Dobson data, morning, atm-cm
DM(13) DOBPM	Dobson data, evening, atm-cm
DM(14,15) PMDL	Model identification, EBCDIC characters
DM(16) ECTIE	tie-on altitude for ECC data, km
DM(17) ECCOL	ECC ozone column up to ECTIE, atm-cm
WORK	work space used in preparation of Composite ozone profile

In Subroutines RELATD and PRTWRT, WORK is further divided thus

COMMON/DATOUT/NSAV.....,COMP(20,70),TYP4(20,2),TYP5(10,34)

COMP	Rocoz composite ozone profile (type 300. data record)
TYP4	ozone content in std pressure layers (type 400. data record)
TYP5	ozone values at standard pressure levels (type 500. data record)

PROFILE PROGRAM

Input Data

The Profile Program uses the Smooth Tape as the source of data from the Rocoz photometer; the detailed description of this tape is given in the section on Tape Formats. DATA5 "cards" are the source of specific run options, calibration information, and observations from the Dobson spectrophotometer, the Datasonde, and ECC sondes. Data needed to compute effective absorption and scattering coefficients are stored on disc: solar flux, rayleigh scattering coefficients, ozone absorption coefficients at three temperatures, diffuser transmission, detector responsivity, and, for filters calibrated at the Wallops Flight Facility, filter shapes.

Card Input

For ease in identification, each card has a letter in the first column; this is not read by the Program. Approximately 100 cards are needed, depending upon the altitude range of the Datasonde and the number of ECC sondes.

<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
1		A One card required. <u>Tape and Filter IDs</u>	
2-7	F6.1	Flight number and segment	FLT(1)
10-17	A8	DT, Tape Volume Identifier, volume serial number for input (Smooth) tape	TAPEIN
18-20	I3	file number on input tape	NFIN
25-32	A8	DT, Tape Volume Identifier, output (Profile) tape	TAPOUT
33-35	I3	file number on output tape	NFOT
40-41	I2	month, filter calibration	MDY(1)
43-44	I2	day, filter calibration	MDY(2)
46-47	I2	day of month, filter calibration	MDY(3)
49-52	A4	filter manufacturer	MFG
54-58	I5	dddy, date of filter set assembly	ICAL
60-65	I6	filter set identification no.	ICLID

PROFILE PROGRAM

Card Input (continued)

<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
1		B Seven required. <u>Filter processing</u>	
3-4	I2	03, 02, 01, 00, 30, 20, or 10; use negative number (-1) to skip	INCLD(x)
5-9	F5.1	highest altitude to be used	TOP(x)
10-14	F5.1	lowest altitude to be used	BASE(x)
17-22	F6.2	center wavelength, nm	CW(x)
24-28	F5.2	bandwidth, nm	BW(x)
31-38	F8.4	McBride's A0	CMCBRD(1,x)
40-49	F10.5	McBride's A1	CMCBRD(2,x)
51-60	F10.5	McBride's A2	CMCBRD(3,x)
62-68	F7.5	McBride's B	CMCBRD(4,x)

- Notes:
- Values in INCLD must be in the order indicated.
 - For cards 5, 6, and 7, CW and BW are blanks.
 - The subscript, x, refers to card number (1-7)
 - The values of center wavelength, bandwidth, A0, A1, and A2 are also calculated for the filters calibrated at WFF; B is obtained for the center wavelength from the Rayleigh scattering table.

1		C One required. <u>Dobson data</u>	
3-4	I2	month, date of Dobson obs.	MDY(1)
6-7	I2	day of month, date of Dobson obs.	MDY(2)
9-10	I2.1	year, date of Dobson observations	MDY(3)
13-17	F5.1	AM value, in Dobson units	PED(3,6)
24-24	F5.1	PM value, in Dobson units	PED(4,6)

PROFILE PROGRAM

Card Input (continued)

<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
1		D One required. <u>Datasonde ID</u>	
3-10	A8	Datasonde flight number.	FLTID
13-14	I2	month, date of datasonde flight	MDY(1)
16-17	I2	day of month, date of datasonde	MDY(2)
19-20	I2	year, date of datasonde	MDY(3)
23-24	I2	hour, time of datasonde launch	IH
25-26	I2	minute, time of datasonde launch	IM
29-31	I3	minutes between datasonde and Rocoz launches	MDEL
34-40	F7.1	base altitude, meters	DSB(1)
43-48	F6.2	base temperature, C. or kelvin	DSB(2)
51-56	F6.2	base pressure, mbar	DSB(3)

Note: Base altitude, temperature, and pressure are obtained from the study of data from the nearly simultaneous ECC sondes and are used to calculate the pressures and densities at Datasonde altitudes.

1		E Max of 70 required. <u>Datasonde Data</u>	
3-8	F6.0	altitude of observation, m or km	ALT
11-16	F6.2	observed temperature, C. or kelvin	TEMP
19-22	F4.1	error in temperature, 2-sigma, deg	TERR

Notes:

- First card gives data for the highest altitude.
- Last card must set "altitude" to -1, to indicate end of data.
- If the Datasonde report does not include error estimate, use errors from F.Schmidlin (JGR,86, 9599,1981)

PROFILE PROGRAM

Card Input (continued)

<u>Columns</u>	<u>Format</u>	<u>Content</u>	<u>Variable</u>
1		F One required. <u>ECC sonde ID</u>	
3-10	A8	ECC sonde flight number.	FLTID
13-14	I2	month, date of ECC sonde flight	MDY(1)
16-17	I2	day of month, date of ECC sonde	MDY(2)
19-20	I2	year, date of ECC sonde	MDY(3)
23-24	I2	hour, time of ECC sonde launch	IH
25-26	I2	minute, time of ECC sonde launch	IM
29-34	F6.0	tie-on altitude, meters	TIEALT
37-43	F7.5	ozone column up to TIEALT, atm-cm	TIECOL

Note: If data from a second ECC sonde is available, a type F card for the second sonde follows the type G (data) cards for the first sonde.

1		G 19 required. <u>ECC sonde Data</u>	
3-7	I5	altitude, meters	KH
10-14	F5.1	ozone pressure, nanobars	ECC(4,I,1)
17-22	F6.1	air pressure, millibars	ECC(3,I,1)
25-29	F5.1	air temperature, C. or kelvin	ECC(2,I,1)

Note: Data are given at 19 standard pressure levels, namely, 1000., 850., 700., 500., 400., 300., 250., 200., 150., 100., 70., 60., 50., 40., 30., 25., 20., 15., and 10. If data are not available for a given pressure level, the altitude, ozone pressure, and temperature are to be set to 0.0 The first card is for 1000. mbar.

If data from a second ECC sonde are available, they follow the type F card identifying the flight.

1		H One required. <u>ECC Ozone Column</u>	
7-13	F7.5	ECC O3 column, up to 250 mbar	ECCLM(1)
20-26	F7.5	ECC O3 column, up to 125 mbar	ECCLM(2)
33-39	F7.5	ECC O3 column, up to 62.5 mbar	ECCLM(3)

Note: Column content is in atm-cm of ozone.

TAPE FORMATS

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TAPE FORMATS

RADAR TAPE FORMAT

Most tapes for flights through April 1982 (Roco flight no. 315) were prepared by the Wallops Station Meteorological Support program 1.1.2123. The "GE-625 Meteorological Support Format" (MESUP) is as follows:

Each physical record is composed of twenty-one twelve-character words. The word layout is in the following form:

```
  X X X X X X X X X X X S 0
  0 1 2 3 4 5 6 7 8 9 10 11
```

Character number 0 is the most significant character and character number 11 is the least significant character and will always be a zero. The sign position is fixed for all words and is in character position 10. The first word of each record is a system word recorded for tape identification and may be ignored in all processing.

The tape is recorded with word one character number 0 being recorded first. Each tape file will be followed by a tape mark. Inter-record gap is approximately three-fourths of an inch. Each tape will have a ten to twenty foot leader of blank tape before the beginning of tape (BOT) tinsel marker.

Tape Description and Parameters for JCL

7-track	UNIT=2400-7 or 7TRACK
no label	LABEL=NL
records are fixed length	RECFM=F
block size is 252 bytes	BLKSIZE=252
record length is 252 bytes	LRECL=252
density = 800 bpi	DEN=2
even parity	TRTCH=E
BCD characters	TRTCH=T (to EBCDIC)

TAPE FORMATS

Radar Tape Format

<u>Word Number</u>	<u>Character Positions</u>	<u>Data Content</u>	<u>Decimal point assumed between characters</u>
2	0-9	Elapsed time given in seconds.	5&6
3	0-9	Slant range from the origin in feet.	9&10
4	0-9	Azimuth from origin given in degrees.	5&6
5	0-9	Elevation from origin given in degrees.	5&6
6	0-9	Horizontal range from origin in feet.	9&10
7	0-9	North-South range from origin in feet.	9&10
8	0-9	East-West range from origin in feet	9&10
9		(Not used, contains zeros)	
10	0-9	Altitude above an oblate spheroid in feet.	9&10
11		(winds or zeros)	
12		(winds or zeros)	
13	0-9	Horizontal component of earth relative velocity vector in feet/second.*	9&10
14	0-9	East-West component of negative velocity vector in feet/second.*	9&10
15	0-9	North-South component of negative velocity vector in feet/second.*	9&10
16	0-9	Altitude component of velocity vector in feet/second.*	9&10
17		(Not used, contains zeros)	
18	0-9	Azimuth of the horizontal component of the negative velocity vector in degrees.*	5&6
19		(Not used, contains zeros)	
20		(Not used, contains zeros)	
21		(not used, contains zeros)	

* Velocity vector is defined as positive in the direction of target motion measured clockwise from North.

TAPE FORMATS

RADAR (1983) TAPE

Radar data for flights in 1983 and later are prepared on the Applications Directorate Eclipse computer at WFF and provide location in meters, latitude and longitude on a 9-track tape. This PASS1 tape may be listed by the Listrad Program. The Merge Program has been modified such that it can accept either this tape or the Reformatted Radar Tape produced by the Radar Program. When this, the Radar (1983) tape, is used, the Merge Program prepares the Radar Pedigree (Type -100.) record.

Tape Description and Parameters for JCL

9-track	UNIT=800
no label	LABEL=NL
records are fixed length and blocked	RECFM=FB
blocksize is 32 bytes	BLKSIZE=32
record length is 32 bytes	LRECL=32
density = 800 bpi	DEN=2

Radar (1983) Tape Format

All words are binary double precision, REAL*8.

Word Number	Data Content
1	Seconds since launch time
2	Altitude, meters
3	Latitude, degrees North
4	Longitude, degrees East

TAPE FORMATS

REFORMATTED RADAR TAPE

The Reformatted Radar Tape is a product of the Radar program. Like all tapes produced by this RocoZ set of programs, the first record is a "Pedigree" record giving the flight number, date of creation of this tape, and other RocoZ-related data entered via the DATA5 input unit. The program converts times to seconds after the hour instead of after launch and converts English units to metric units. Each file contains all available data for a single flight.

Tape Description and Parameters for JCL

9 track	UNIT=2400-9 or 9TRACK
standard label	LABEL=SL
records are fixed length	
and blocked	RECFM=FB
blocksize is 5200 bytes	BLKSIZE=5200
record length is 52 bytes	LRECL=52
tape density is 1600 bpi	DEN=3

Pedigree Record

Words 1-9 are R*4 real words; 10-13 are EBCDIC characters.

<u>Word</u>	<u>Content</u>	<u>Source</u>
1	-100.	Assigned
2	Flight Number	DATA5
3	VXX. where V indicates vehicle type: =1 rocket =2 balloon and XX indicates launch site: =01 Wallops Island, Virginia =02 Poker Flats, Alaska =03 Natal, Brazil =04 Marambio, Antarctica =05 Palestine, Texas	DATA5
4	MMDDYY. month, day, year of launch	DATA5
5	HHMMSS.S hour, minute, second of launch	DATA5
6	±XX.XXX latitude of launch site	DATA5
7	XXX.XXX longitude of launch, degrees WEST	DATA5
8	MMDDYY. date radar tape was received	DATA5
9	MMDDYY. date of creation of this tape	Computer
10-13	launch site, 16 EBCDIC characters	DATA5

TAPE FORMATS

Data Records (Reformatted Radar Tape)

All words are R*4 real words

<u>Word</u>	<u>Content</u>	<u>Unit</u>
1	time from hour prior to start of data	seconds
2	slant range	meters
3	azimuth from origin	degrees
4	elevation from origin	degrees
5	horizontal range from origin	meters
6	north-south range from origin	meters
7	east-west range from origin	meters
8	altitude above oblate spheroid	meters
9	horizontal component of velocity relative to the earth	meters/second
10	east-west component of velocity	meters/second
11	north-south component of velocity	meters/second
12	vertical velocity	meters/second
13	azimuth of horizontal component of velocity	degrees

The velocity vector is defined as positive in the direction of target motion measured clockwise from North.

TAPE FORMATS

TELEMETRY TAPE FORMAT

The telemetry tapes for the Roco2 flights have been produced by the "Digital Telemetry System (PDP 11/60): DITES" at the Wallops Flight Facility. NOTE THAT THE BYTES FROM THE PDP-11 MACHINE ARE PACKED MSB LAST.

Tape Description and Parameters for JCL

9-track	UNIT=2400-9 or 9TRACK
no label	LABEL=NL
record length is undefined	RECFM=U
block size is 2440 bytes	BLKSIZE=2440
density is 800 bpi	DEN=2

The "televent-11" data tapes from this WFF system consist of three different types of records. The first record of the Roco2 data tape is a Header Record that contains up to 80 ASCII characters. The second type of record is a Data Description Record which describes the data for the Roco2 data stream. The third type of record is the Data Record.

Header Record

<u>Word</u> <u>Number</u>	<u>Content</u>	<u>Description</u>
1	177776	-2 for DEC Fortran compatibility
2	NN	number of words in record
3	000000	0 to identify Header Record
4	B A	4-character stream identification
5	D C	(note order of characters)
6	N	tape number
7	B A	ASCII text. Each character in a
through		word is recorded most significant
46	Z Y	bit last.

TAPE FORMATS

Data Description Record

<u>Word No.</u>	<u>Content</u>	<u>Typical Value</u>	<u>Description</u>
1	177776	-2	-2 for DEC Fortran compatibility
2	N	20	number of words in record
3	177775	-3	-3 to identify Data Description Record
4	B A	PC	4-character Run Identifier from setup
5	D C	M4	of tape processing
6	B A	PC	4-character Stream Identifier (usually
7	D C	M4	the same as words 4 and 5
8	N	8	number of data words per frame
9	N	110	number of frames per buffer
10	N	0	scaling factor (normally = 0)
11	N	3	number of frame Merge words
12	N	11	number of words/frame
13	N	2	number of preface words above 8
14	N	0	buffer appendix size
15	N	1210	INPUT buffer size (words)
16	:	1220	OUTPUT buffer size (words)
17	N	0	frames/subframe number 1
18	N	0	frames/subframe number 2
19	N	0	recording mode (0=word; 1=byte)
20	020040		two ASCII blanks

Data Record

The data record consists of a 10-word preface, 110 11-word data frames, and no appendix.

Preface

<u>Word No.</u>	<u>Content</u>	<u>Typical Value</u>	<u>Description</u>
1	177776	-2	-2 for DEC Fortran compatibility
2	N	1220	record length (words)
3	N		block count
4	B A	PC	4-character Stream Identifier
5	D C	M4	
6	A P	10	A is no. of Appendix words (); P is no of Preface words ()
7	L M	1210	INPUT buffer size
8	S F		TFE status and frame information (see below for explanation)
9	N	110	number of frames per buffer
10	N	0	scaling factor (normally = 0)

TAPE FORMATS

Word no. 8: TFE status

<u>Bit</u>	<u>Content</u>
0-8	frame number of first search
9	sub-com 2 search on last buffer
10	sub-com 1 search on last buffer
11	frame search on last buffer
12	multiple search on one of below
13	sub-com 2 search flag
14	sub-com 1 search flag
15	frame search flag (most significant bit)

A hex value of 00 is normal; FF usually indicates missing frames.

Data Frame

<u>Word Number</u>	<u>Content</u>
1	S3 filter, counts
2	S2 filter, counts
3	compensation filter, counts
4	S1 filter, counts
5	S0 filter, counts
6	battery voltage, counts
7	marker pulse, counts
8	uncompensated value, counts
9	milliseconds (see below)
10	minutes and seconds (see below)
11	day of year, hour of day (GMT) (see below)

Word 9:

15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0
tenths of sec.				hundredths of s				thousandths s							

Word 10:

15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0
tens of min				units of min				tens of sec				units of sec.			

Word 11:

15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0
100's		tens of day				units of day				tens hr		units of hour			

TAPE FORMATS

EDITED OZONE DATA TAPE FORMAT

The Edited Ozone Data Tape is the product of the Edit Program. Following the single Pedigree record are Data records, one record for each rotation of the filter wheel. Battery voltage and temperature data are converted to engineering units; the remaining data are in telemetry counts. All words are R*4 real numbers.

Tape Description and Parameters for JCL

9 track	UNIT=2400-9 or 9TRACK
standard label	LABEL=SL
records are fixed length and blocked	RECFM=FB
blocksize is 8000 bytes	BLKSIZE=8000
record length is 80 bytes	LRECL=80
tape density is 1600 bpi	DEN=3

Edit Pedigree Record

<u>Word</u>	<u>Content</u>	<u>Source</u>
1	-200.	Assigned
2	XXX.S flight number.segment for rocket flights, S is 0	DATA5
3	Payload number	DATA5
4	MMDDYY. month, day, year that telemetry tape was received.	DATA5
5	MMDDYY. month, day, year for creation of this tape.	Computer
6	Battery calibration: volts (upper level)	DATA5
7	" " tm count " "	DATA5
8	" " volts (lower level)	DATA5
9	" " tm count " "	DATA5
10	Temperature calib.: degree C. (lower)	DATA5
11	" " tm count "	DATA5
12	" " degree C. (mid)	DATA5
13	" " tm count "	DATA5
14	" " degree C. (high)	DATA5
15	" " tm count	DATA5
16	0.0	
17	0.0	
18	0.0	
19	0.0	
20	0.0	

TAPE FORMATS

Edit Data Record

<u>Word</u>	<u>Content</u>	<u>Unit</u>
1	time since hour of tm word 1 (S0)	seconds
2	time since hour of tm word 2 (S1)	seconds
3	time since hour of tm word 4 (S2)	seconds
4	time since hour of tm word 5 (S3)	seconds
5	value of tm word 1 (S0)	counts
6	value of tm word 2 (S1)	counts
7	value of tm word 4 (S2)	counts
8	value of tm word 5 (S3)	counts
9	value of marker pulse (tm word 7)	counts
10	value of base level (tm word 7)	counts
11	compensation word (tm word 3) for S0	counts
12	compensation word (tm word 3) for S1	counts
13	compensation word (tm word 3) for S2	counts
14	compensation word (tm word 3) for S3	counts
15	length of this cycle	seconds
16	average length of last ten cycles	seconds
17	average value of word 3	counts
18	battery voltage (average over 110 frames)	volts
19	temperature (from marker pulse height)	degrees C.
20	number of frames in this cycle	count

TAPE FORMATS

MERGE TAPE FORMAT

The Merge Tape is the product of the Merge Program. The first record is the Pedigree record from the Reformatted Radar Tape; the second record is the Pedigree record from the Edited Ozone Tape. The third record is the Pedigree record created by the running of the Merge Program. The data records essentially replace the time information with altitude information. All words on this tape are R*4 real numbers.

Tape Description and Parameters for JCL

9 track	UNIT=2400-9 or 9TRACK
standard label	LABEL=SL
records are fixed length	
and blocked	RECFM=FB
blocksize is 8000 bytes	BLKSIZE=8000
record length is 80 bytes	LRECL=80
tape density is 1600 bpi	DEN=3

Merge Pedigree Record

<u>Word</u>	<u>Content</u>	<u>Source</u>
1	-300.	Assigned
2	XXX.S flight number.segment for rocket flights, S is 0	DATA5
3	MMDDYY. month, day, year for creation of this tape.	Computer
4	Apparent right ascension of the sun, hour	DATA5
5	" " " minutes	DATA5
6	" " " seconds	DATA5
7	" " " ,	
	difference between two days, seconds	DATA5
8	Apparent declination of the sun, degrees	DATA5
9	" " , minutes	DATA5
10	" " , seconds	DATA5
11	" " ,	
	difference between two days,seconds	DATA5
12	Apparent sidereal time, hour	DATA5
13	" " minutes	DATA5
14	" " seconds	DATA5
15	0.0	
16	0.0	
17	0.0	
18	0.0	
19	0.0	
20	0.0	

TAPE FORMATS

Merge Data Record

<u>Word</u>	<u>Content</u>	<u>Unit</u>	<u>Word on Edit Data Rec</u>
1	time since hour of tm word 1 (S0)	seconds	1
2	length of this cycle	seconds	15
3	number of samples in this cycle	count	20
4	temperature of instrument	degrees C.	19
5	value of tm word 1 (S0)	counts	5
6	value of tm word 2 (S1)	counts	6
7	value of tm word 4 (S2)	counts	7
8	value of tm word 5 (S3)	counts	8
9	value of marker pulse (tm word 7)	counts	9
10	battery voltage	volts	18
11	compensation word (tm word 3) for S0	counts	11
12	compensation word (tm word 3) for S1	counts	12
13	compensation word (tm word 3) for S2	counts	13
14	compensation word (tm word 3) for S3	counts	14
15	average value of compensation word	counts	17
16	altitude for tm word 1 (S0)	meters	
17	altitude for tm word 2 (S1)	meters	
18	altitude for tm word 4 (S2)	meters	
19	altitude for tm word 5 (S3)	meters	
20	solar zenith angle	degrees	

TAPE FORMATS

SMOOTH TAPE FORMAT

The Smooth Tape is the product of the Smooth Program. The first record is the Pedigree record from the Reformatted Radar Tape; the second record is the Pedigree record from the Edited Ozone Tape. The third record is the Pedigree record from the Merge Program. The fourth record is the Pedigree record created by the Smooth program. Each Smooth Data record provides data at one integer altitude for one filter. After data records for each of the four filters, similar information is given for S3/S0, S2/S0, and S1/S0. All words are R*4 real numbers.

Tape Description and Parameters for JCL

9 track	UNIT=2400-9 or 9TRACK
standard label	LABEL=SL
records are fixed length and blocked	RECFM=FB
blocksize is 4000 bytes	BLKSIZE=4000
record length is 80 bytes	LRECL=80
tape density is 1600 bpi	DEN=3

Smooth Pedigree Record

<u>Word</u>	<u>Content</u>	<u>Source</u>
1	-400.	Assigned
2	XXX.S flight number.segment for rocket flights, S is 0	DATA5
3	MMDDYY. month, day, year for creation of this tape.	Computer
4	zero offset for S0, counts	DATA5
5	zero offset for S1, counts	DATA5
6	zero offset for S2 at temp. of word 11	DATA5
7	zero offset for S3 at temp. of word 11	DATA5
8	maximum integer altitude to be processed	DATA5
9	minimum integer altitude to be processed	DATA5
10	minimum acceptable value of comp. word	DATA5
11	temperature (deg. C) for words 6 and 7	DATA5
12	temperature (deg. C) for words 13 and 14	DATA5
13	zero offset for S2 at temp. of word 12	DATA5
14	zero offset for S3 at temp. of word 12	DATA5
15	0.0	
16	0.0	
17	0.0	
18	0.0	
19	0.0	
20	0.0	

TAPE FORMATS

Smooth Data Record

<u>Word</u>	<u>Content</u>	<u>Unit</u>
1	filter position: 3., 2., 1., or 0. if ratio to S0: 30., 20., or 10.	
2	altitude level, H	kilometers
3	signal at XCEN, $I = \text{EXP}(A + B * (H - H_b))$	count or ratio
4	error = $(\text{SIGMAA}^2 + (H - H_b)^2 \text{SIGMAB}^2)^{1/2}$	See note.
5	solar zenith angle at XCEN	degrees
6	time at XCEN	seconds after hour
7	temperature of instrument	degrees C
8	average length of filter cycle (99 cycles)	seconds
9	battery voltage	volts
10	average compensation word (99 cycles)	counts
11	upper end of altitude interval	kilometers
12	lower end of altitude interval	kilometers
13	number of points used	count
14	estimated signal at H _b altitude, $= \text{EXP}(A)$	
15	standard deviation of A (SIGMAA)	
16	estimated absorption and scattering, $= -B$	
17	standard deviation of B (SIGMAB)	
18	standard deviation of fit to curve	
19	correlation coefficient	
20	number of points provided in altitude interval	

Note: In files created before Dec. 1983, word 4 is slope ($= B * I$).

TAPE FORMATS

PROFILE TAPE FORMAT

The Profile Tape is the product of the Profile Program and is intended to be suitable for the archival of data from the Rocoz flight. It includes not only the derived ozone profile, but also the related ECC and Datasonde data and the calibration constants used in the processing of the Rocoz data. The first group of records are Pedigree records, both those from preceding programs in the Rocoz data reduction system and created by the Profile program. The second group of records give ozone content as a function of altitude with values of various parameters developed in the computation. The third group of records give the ozone content in various units and altitude levels for the convenience of the user. The maximum number of records for a flight is 456. Most of the data are in R*4 real words except for some words in the Pedigree records which are in character (EBCDIC) format.

Tape Description and Parameters for JCL

9 track	UNIT=2400-9 or 9TRACK
standard label	LABEL=SL
records are fixed length and blocked	RECFM=FB
blocksize is 4000 bytes	BLKSIZE=4000
record length is 80 bytes	LRECL=80
tape density is 1600 bpi	DEN=3

TAPE FORMATS

Types of Records

<u>First Word</u>	<u>Content</u>	<u>Number of this type</u>
-100.	Pedigree: reformatted radar tape	1
-200.	Pedigree: edited telemetry tape	1
-300.	Pedigree: merge data tape	1
-400.	Pedigree: smooth data tape	1
-500.	filter: McBride coefficients	1
-501.	filter coeff; Dobson data	1
-502.	Datasonde flight ID and data	1
-503.	Datasonde data	3
-504.	ozone density model	1
-505.	ozone model, continued	3
-506.	ECC sonde ID and data	1
-507.	ECC data, continued	4
-506.	second ECC ID and data, if available	1
-507.	second ECC data, continued	4
-508.	source of data for solar flux	1
-509.	source of data for diffuser transmission	1
-510.	source of data for detector responsivity	1
-511.	source of Raleigh scattering coefficient	1
-512.	source of ozone absorption coeff., max temp.	1
-513.	source of ozone absorption coeff.,	1
-514.	source of ozone absorption coeff., min temp.	1

For each filter, at each altitude level, are two data records; the number of records per filter or filter ratio varies from 0 to 25.

- 1xx. intermediate values in the calculation of ozone
- 2xx. observed ozone with air temp., air press., etc.

The following records give derived profiles in various units:

300.	composite ozone profile, 1 km per record	10-60
400.	ozone layer content in 12 std. pressure layers	2
500.	ozone at standard (33) pressure levels, 2 levels per record.	17

Maximum number of records: 460.

TAPE FORMATS

Pedigree Records Created by Profile Program

Word Content

1 -500. RocoZ flight ID; filter ID and calibration
2 XXX.S flight number and segment
3 MMDDYY. month, day, year for creation of this tape
4 number of ECC sondes available: 0., 1., or 2.
5 AAAA (EBCDIC) manufacturer of filter set
6 DDDYY. day of year and year of set assembly
7 filter set identification number
8 MMDDYY. month, day, and year of filter calibration
9 S3 center wavelength, nm
10 S3 bandwidth, nm
11 S3 A0, ozone absorption coeff. from McBride's calibration
12 S3 A1, coeff. for rate of change due to ozone overburden
13 S3 A2, "
14 S3 beta, Rayleigh scattering coefficient
15 S2 center wavelength, nm
16 S2 bandwidth, nm
17 S2 A0, ozone absorption coeff. from McBride's calibration
18 S2 A1, coeff. for rate of change due to ozone overburden
19 S2 A2, "
20 S2 beta, Rayleigh scattering coefficient

1 -501. Dobson data; filter calibration data
2 MMDDYY. month, day, year of Dobson observations
3 AM data, Dobson units; 0.0 if unavailable
4 PM data, Dobson units; 0.0 if unavailable
5 0.0
6 0.0
7 0.0
8 0.0
9 S1 center wavelength, nm
10 S1 bandwidth, nm
11 S1 A0, ozone absorption coeff. from McBride's calibration
12 S1 A1, coeff. for rate of change due to ozone overburden
13 S1 A2, "
14 S1 beta, Rayleigh scattering coefficient
15 S0 center wavelength, nm
16 S0 bandwidth, nm
17 S0 A0, ozone absorption coeff. from McBride's calibration
18 S0 A1, coeff. for rate of change due to ozone overburden
19 S0 A2, "
20 S0 beta, Rayleigh scattering coefficient

TAPE FORMATS

Word Content

1	-502. Datasonde ID and data
2	initial altitude (top) of datasonde profile, km
3	end altitude (bottom) of datasonde profile, km
4	number of levels in datasonde profile
5	AAAA (EBCDIC) Datasonde flight identification
6	AAAA (EBCDIC) " (continued)
7	MMDDYY. month, day, year of datasonde flight
8	HHMM. hour, minute of datasonde launch
9	base altitude for pressure profile, kilometers
10	air pressure at base altitude, millibar
11	acceleration of gravity at latitude of launch site, m/s ²
12	earth radius at launch latitude, km
13	temperature at initial altitude, kelvin
14	temperature at next lower altitude, kelvin
15	"
16	"
17	"
18	"
19	"
20	"
1	-503. Datasonde temperature data, continued
2	temperature at next lower altitude, kelvin
3-20	"

There may be more than one type -503. record, depending on the number of levels at which data are available. Where no more levels are available, the remainder of the words in the record are set to 0.0

TAPE FORMATS

Word Content

1 -504. Model values for ozone overburden
 2 initial altitude of model, km (typically, 70.)
 3 altitude increment, km (typically, -1.)
 4 number of levels
 5 AAAA (EBCDIC) model identification
 6 AAAA (EBCDIC) (continued)
 7 altitude for initial overburden of ozone, km
 8 ozone overburden above altitude in word 7, number/m²
 9 ozone number density at the initial altitude, number/m³
 10 ozone number density at next lower altitude
 11-20 "

1 -505. Model values, continued
 2-20 ozone number density at next lower altitude, or padded
 with 0.0

There may be 0 - 3 type -505. records, depending upon the model in use.

1 -506. ECC flight ID and data
 2 tie-on altitude, typically 20 to 25 km
 3 ozone column content, ground to tie-on altitude, atm-cm
 4 number of levels of ECC data
 5 AAAA (EBCDIC) ECC sonde flight identification
 6 AAAA (EBCDIC) (continued)
 7 MMDDYY. month, day, year of ECC flight
 8 HHMM. hour, minute of ECC launch
 9 altitude, beginning near the ground, km
 10 air temperature, kelvin
 11 air pressure, mbar
 12 ozone partial pressure, nanobar
 13-20 repeat parameters of words 9-12 for increasing altitude
 levels.

Data are to be given at 19 standard pressure levels:

1000.	850.	700.	500.	400.	300.	250.	200.	150.	
100.	70.	60	50.	40.	30.	25.	20.	15.	10.

If data from a second ECC sonde are available, record types -506. and -507. are to be repeated for the second flight.

TAPE FORMATS

Word Content

1 -507. ECC data, continued
2 1. or 2., first or second ECC sonde
3 AAAA (EBCDIC) ECC sonde flight identification
4 AAAA (EBCDIC) (continued)
5-20 repeat (altitude, temperature, pressure, ozone)
 as needed for the remaining standard pressures.

There may be up to four cards of this type for each ECC sonde.

1 -508. source of data for solar flux
2-17 alphanumeric description of data
18 initial wavelength of data, A.
19 end wavelength of data, A.
20 0.0

1 -509. source of data for diffuser transmission.
2-17 alphanumeric description of data.
18 initial wavelength of data, A.
19 end wavelength of data, A.
20 0.0

1 -510. source of data for detector responsivity.
2-17 alphanumeric description of data
18 initial wavelength of data, A.
19 end wavelength of data, A.
20 0.0

1 -511. source of data for Rayleigh scattering coefficient
2-17 alphanumeric description of data
18 initial wavelength of data, A.
19 end wavelength of data, A.
20 0.0

1 -512. source of data for ozone absorption coefficient,
 room temperature.
2-17 alphanumeric description of data
18 initial wavelength of data, A.
19 end wavelength of data, A.
20 temperature, K

TAPE FORMATS

1 -513. source of data for ozone absorption coefficient,
lower than than in Pedigree record -512.
2-17 alphanumeric description of data
18 initial wavelength of data, A.
19 end wavelength of data, A.
20 temperature, K

1 -514. source of data for ozone absorption coefficient,
lowest available temperature.
2-17 alphanumeric description of data
18 initial wavelength of data, A.
19 end wavelength of data, A.
20 temperature, K

TAPE FORMATS

Data Records Created by Profile Program

Word Content

1	10f. for word 5 in counts; 1f0. word 5 as ratio to S0 f = filter number: 3, 2, 1, or 0
2	h, altitude, km
3	compensation channel, counts
4	secant/Chapman-function for solar zenith angle
5	(I), intensity at altitude, h, counts or ratio to S0
6	slant ozone overburden, atm-cm
7	slant air mass overburden, atm
8	effective ozone absorption coefficient at h, alpha-eff
9	effective Rayleigh scattering coefficient at h, beta-eff
10	$d(\ln I)/dh$
11	$d \text{ alpha-eff}/d \text{ slant-ozone}$
12	$d \text{ slant-air}/dh$
13	optical depth due to slant ozone
14	optical depth due to slant air
15	Fraser correction (for scattered light)
16	noise for delta ($\ln I$)
17	delta-h used by Smooth in deriving $I(\text{top}) - I(\text{base})$
18	B, (absorption + scattering) from Smooth
19	std. dev. of B
20	photometer temperature, degree C
1	20f. from this filter only; 2f0. from ratio to S0 f= filter number: 3, 2, 1, or 0
2	h, altitude, km
3	error in h, percent
4	HHMMSS.S, hours, minutes, seconds, time, GMT
5	solar zenith angle, degrees
6	noise in ozone density, percent, (from $d(\ln I)/dh$ noise)
7	ozone density, atm-cm/km ³
8	ozone density, number/m ³
9	ozone vertical overburden, atm-cm
10	ozone vertical overburden, number/m ²
11	air temperature, kelvin
12	error in air temperature, percent
13	air pressure, millibar
14	error in air pressure, percent
15	air density, number/m ³
16	air, vertical column, atm.
17	ozone, partial pressure, nanobar
18	ozone volume mixing ratio
19	seconds after the hour
20	record number, except for last for this filter, then =-1.

Note: All errors are for one standard deviation.

TAPE FORMATS

The following records appear after all 1rf. and 2rf. records for all filters and ratios have been written.

Word Content

- | | |
|----|---|
| 1 | 300. Composite Ozone Table (based on all RocoZ filters) |
| 2 | h, altitude, km |
| 3 | ozone density, atm-cm/km |
| 4 | ozone density, number/m ³ |
| 5 | ozone density, error, percent |
| 6 | ozone vertical column, atm-cm |
| 7 | ozone vertical column, error, percent |
| 8 | air temperature, kelvin |
| 9 | air temperature, error, percent |
| 10 | air pressure, millibar |
| 11 | air pressure, error, percent |
| 12 | ozone partial pressure, nanobar |
| 13 | ozone partial pressure, error, percent |
| 14 | ozone volume mixing ratio, ppm |
| 15 | ozone volume mixing ratio, error, percent |
| 16 | HMMSS.S, hours, minutes, seconds, GMT |
| 17 | time, seconds after the hour |
| 18 | number of filters and/or ratios used at this altitude |
| 19 | solar zenith angle, degrees |
| 20 | 0.0; for last record, -1. |

Note: There is one type 300. record for each integer altitude covered by the RocoZ photometer profile.

- | | |
|-------|--|
| 1 | 400. These records contains ozone content in 12 standard pressure layers, derived from the Composite Ozone Table given in the type 300. records; where no RocoZ data are available, ECC data are used. If neither is available, words at that level are set to 0.0 |
| 2 | 1., the first of two type 400. records |
| 3 | air pressure at top of layer, milliatmospheres |
| 4 | ozone content between above pressure altitude and the next pressure altitude, milliatm-cm |
| 5-20 | repeat of words 3 and 4 for the next pressure altitude. |
| 1 | 400. Second record, ozone content in layers |
| 2 | 2. the second record of this type |
| 3-8 | continuation of (air pressure at top, ozone content) |
| 9 | 1000. |
| 10-20 | 0.0 |

Standard pressure altitudes are at $1000./2^{(nth \text{ power})}$ as follows:

0.0	0.24	0.49	0.98	1.95	3.9	7.8	15.6
31.	62.	125.	250.	1000.			

TAPE FORMATS

Word Content

- 1 500. Ozone values at 33 standard pressures levels from
 Rocoz Composite Table or, at low altitudes, from
 ECC observations.
- 2 level number, 1. through 33.
- 3 standard pressure, lowest value for which ozone data are
 available, millibar
- 4 altitude corresponding to pressure in preceding word, km
- 5 air temperature from datasonde, kelvin
- 6 Rocoz Composite ozone, number/m³
- 7 Rocoz Composite ozone mass mixing ratio
- 8 air temperature from ECC sonde, kelvin
- 9 ECC sonde ozone, number/m³
- 10 ECC sonde ozone mass mixing ratio
- 11 500.
- 12 level number
- 13-20 repeat of 3-10 for this level,
 or padded with 0.0 to fill out the record

Standard pressure levels are, in millibars:

0.10	0.15	0.20	0.30	0.40	0.05	0.07
1.0	1.5	2.0	3.0	4.0	0.50	0.70
10.0	15.0	20.0	30.0	40.0	50.0	70.0
100.0	150.0	200.0	250.0	300.0	400.0	500.0
850.0	1000.0					700.0

If Rocoz, ECC, or datasonde observations are not available at any given pressure level, the corresponding words are set to 0.0.

PROGRAM LISTINGS

JCL and DATA5 Cards	IV-2
Fortran Listings	IV-21
Output Listings	IV-189

26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.RAW.CNTL

MEMBER=JCL

```
//Z8SACRAM JOB (L3006,620,3),'RAW FLT 325',TIME=(0,30)
//* RAW.CNTL(JCL) COMPILES AND RUNS THE RAW PROGRAM USING A
//* VS FORTRAN COMPILER.
//*
/*JOBPARM LINES=20,QUEUE=FETCH
// EXEC FORTVC,PARM=(XREF,NOFIPS)
//SYSIN DD DSN=Z8SAC.RAW.CNTL(RAW),DISP=SHR
// EXEC LINKGOV,REGION.GO=192K
/*
//GO.FT10F001 DD UNIT=(800,,DEFER),LABEL=(,NL,,IN),VOL=SER=ERTAPI,
// DCB=(RECFM=U,BLKSIZE=2440,DEN=2),DISP=(OLD,KEEP)
//GO.DAT5 DD *
KA2130 02 1 0325 (TAPEIN, FILE 0, VERSION, FLT #)
001 0025 0030 0000 (# SAMPLES, BEGIN REC., END REC., INCREMNT)
0000.0 0000.0
/* EXEC NOTIFYTS
```

*** END OF MEMBER *** 18 RECORDS PROCESSED *****

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26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.RAM.CNTL

MEMBER=JCLL

```
//Z8SACRAW JOB (L3006,620,4),'RAM 329',TIME=(0,30)
/** RAM.CNTL(JCLL) USES THE LIB.LOAD01 (OBJECT CODE) VERSION OF
/** THE RAM PROGRAM, IN WHICH THE CODE WAS COMPILED WITH A VS
/** FORTRAN COMPILER.
/**
/**JOBPARM QUEUE=FETCH,LINES=20
//GO EXEC PGM=MRAM,REGION=512K
//STEPLIB DD DSN=Z8SAC.LIB.LOAD01,DISP=SHR
//FT06F001 DD SYSOUT=*
//SYSUDUMP DD SYSOUT=*
//SYSABEND DD SYSOUT=*
//FT05F001 DD DDNAME=DATA5
/*
//GO.FT10F001 DD UNIT=(800,,DEFER),LABEL=(4,NL,,IN),VOL=SER=ERTAPI,
// DCB=(RECFM=U,BLKSIZE=2440,DEN=2,EROPT=SKP),DISP=(OLD,KEEP)
//GO.DAT5 DD *
KA2125 04 1 0329 (TAPEIN, FILE #, VERSION #, FLT #)
040 0001 0003 0050 (# SAMPLES, BEGIN REC #, END REC #, INCREMENT)
0000.0 0000.0
/*
// EXEC NOTIFYTS
```

*** END OF MEMBER *** 22 RECORDS PROCESSED *****

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26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.RADAR.CNTL

MEMBER=JCL

```
//Z8SACRAD JOB (L3006,620,4),'SAC RADAR 291',TIME=(1,0)
//** RADAR.CNTL(JCL) COMPILES AND RUNS THE RADAR PROGRAM USING
//** A FORTRAN H COMPILER. (NOTE: THIS JCL CAN ONLY BE USED ON
//** MESSUP RADAR TAPES)
//**
//** EXEC OFORTH, PARM=XREF
//** SOURCE.SYSIN DD DSN=Z8SAC.RADAR.CNTL(RADAR), DISP=SHR
//** EXEC OLINKG0H, REGION.G0=200K
//** GO.FT10F001 DD UNIT=(2400-7,,DEFER), LABEL=(,NL,,IN), VOL=SER=ERTAPI,
//** DCB=(RECFM=F, BLKSIZE=252, DEN=2, TRTCH=ET, LRECL=252, EROPT=ACC),
//** DISP=(OLD,KEEP)
//** GO.FT11F001 DD UNIT=(2400-9,,DEFER), LABEL=(,SL,,OUT), VOL=SER=ERTAPO,
//** DCB=(RECFM=FB, BLKSIZE=5200, DEN=3, LRECL=52), DISP=(NEW,KEEP)
//** GO.DAT15 DD *
//** KA2131 10 01 02 1680.00 291 00/00/81
//** KA2113 11 01
//** 101. 02/26/81 162800.0 +37.850 -75.480 HALLOPS ISLAND
//**
//** EXEC NOTIFYTS
```

*** END OF MEMBER *** 20 RECORDS PROCESSED *****

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26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.RADAR.CNTL

MEMBER=JCLCPY

```
//Z8SACRAD JOB (L3006.620,4),'COPY RADAR 291',TIME=(1,0)
//*
//* RADAR.CNTL(JCLCPY) COMPILES AND RUNS THE COPY1 VERSION OF THE
//* RADAR PROGRAM, USING A FORTRAN H COMPILER.
//*
/*JOBPARM QUEUE=FETCH
// EXEC OFORTH,PARM=XREF
//SOURCE.SYSIN DD DSN=Z8SAC.RADAR.CNTL(COPY1),DISP=SHR
// EXEC OLINKG0H,REGION=GO=200K
//GO.FT10F001 DD UNIT=(2400-9,,DEFER),LABEL=(,SL,,IN),VOL=SER=ERTAP1,
// DCB=(RECFM=FB,BLKSIZE=5200,DEN=3,LRECL=52,EROPT=ACC),
// DISP=(OLD,KEEP),DSN=Z8SACRAD.R0000005
//GO.FT11F001 DD UNIT=(2400-9,,DEFER),LABEL=(,SL,,OUT),VOL=SER=ERTAP0,
// DCB=(RECFM=FB,BLKSIZE=5200,DEN=3,LRECL=52),DISP=(NEW,KEEP),
// DSN=Z8SAC.RADAR291
//GO.DATAS DD *
KA2113 10 01 01 1680.00
KA2115 11 01
/* EXEC NOTIFYTS
```

*** END OF MEMBER *** 20 RECORDS PROCESSED *****

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26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.RADAR.CNTL

MEMBER=JCLL

```
//Z8SACDRR JOB (L3006,620,10),'SACRAD 312,314,315',TIME=(0,30)
/**
/** RADAR.CNTL(JCLL) USES THE LIB.LOAD01 (OBJECT CODE) VERSION
/** OF THE RADAR PROGRAM, WHICH WAS COMPILED WITH A FORTRAN H
/** COMPILER. THIS JCL ALSO ALLOWS ONE TO RUN MULTIPLE FLIGHTS.
/** (NOTE: THIS JCL CAN ONLY BE USED ON MESSUP RADAR TAPES)
/**
/**JOBPARM LINES=20,QUEUE=FETCH
/**STEP1 EXEC OLINKGOH,REGION,GO=200K
/**LINK.SYSLIB DD DSN=Z8SAC.LIB.LOAD01,DISP=SHR
/**LINK.SYSLIN DD *
/**INCLUDE SYSLIB(MRAD)
ENTRY MRAD
//GO.FT10F001 DD UNIT=(2400-7,,DEFER),LABEL=(,NL,,IN),VOL=SER=ERTAPI,
// DCB=(RECFM=F,BLKSIZE=252,DEN=2,TRTCH=ET,LRECL=252,EROPT=ACC),
// DISP=(OLD,KEEP)
//GO.FT11F001 DD UNIT=(2400-9,,DEFER),LABEL=(22,SL,,OUT),
// DCB=(RECFM=FB,BLKSIZE=5200,DEN=3,LRECL=52),DISP=(NEW,KEEP),
// VOL=SER=ERTAPO,DSN=Z8SAC.RADAR312
//GO.DATAS DD *
KA2130 10 01 02 0420.00 312 07/20/82
KA2120 11 22
102. 06/11/82 000700.0 65.120 -147.480 POKER FLATS, AK
/**
/** EXEC GO,STEP=STEP1,REGION,GO=200K
//GO.FT10F001 DD UNIT=(2400-7,,DEFER),LABEL=(,NL,,IN),VOL=SER=ERTAPI,
// DCB=(RECFM=F,BLKSIZE=252,DEN=2,TRTCH=ET,LRECL=252,EROPT=ACC),
// DISP=(OLD,KEEP)
//GO.FT11F001 DD UNIT=(2400-9,,DEFER),LABEL=(23,SL,,OUT),
// DCB=(RECFM=FB,BLKSIZE=5200,DEN=3,LRECL=52),DISP=(NEW,KEEP),
// VOL=SER=ERTAPO,DSN=Z8SAC.RADAR314
//GO.DATAS DD *
KA2131 10 01 02 1920.00 314 07/20/82
KA2120 11 23
102. 06/11/82 233200.0 65.120 -147.480 POKER FLATS, AK
/**
/** EXEC GO,STEP=STEP1,REGION,GO=200K
//GO.FT10F001 DD UNIT=(2400-7,,DEFER),LABEL=(,NL,,IN),VOL=SER=ERTAPI,
// DCB=(RECFM=F,BLKSIZE=252,DEN=2,TRTCH=ET,LRECL=252,EROPT=ACC),
// DISP=(OLD,KEEP)
//GO.FT11F001 DD UNIT=(2400-9,,DEFER),LABEL=(24,SL,,OUT),
// DCB=(RECFM=FB,BLKSIZE=5200,DEN=3,LRECL=52),DISP=(NEW,KEEP),
// VOL=SER=ERTAPO,DSN=Z8SAC.RADAR315
//GO.DATAS DD *
KA2132 10 01 02 1200.00 315 07/20/82
KA2120 11 24
102. 06/12/82 232000.0 65.120 -147.480 POKER FLATS, AK
/**
```

*** END OF MEMBER *** 48 RECORDS PROCESSED *****

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26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.RADAR.CNTL

MEMBER=LISTJCL

```
//Z8SACRD2 JOB (L3006,620,4),'LIST RADAR 324',TIME=(1,0)
//*
//* RADAR.CNTL(LISTJCL) COMPILES AND RUNS THE LISTRAD PROGRAM
//* (THE RADAR PROGRAM USED FOR ALL PASS1 RADAR TAPES), USING A
//* VS FORTRAN COMPILER.
//*
//*JOBPARM QUEUE=FETCH
// EXEC FORTVC,PARM=XREF
//SYSIN DD DSN=Z8SAC.RADAR.CNTL(LISTRAD),DISP=SHR
// EXEC LINKGOV,REGION,GO=200K
//GO.FT10F001 DD UNIT=(800,,DEFER),LABEL=(2,ML,,IN),VOL=SER=ERTAPI,
// DCB=(RECFM=FB,BLKSIZE=32,DEN=2,LRECL=32,EROPT=ACC),
// DISP=(OLD,KEEP)
//GO.DATAS DD *
324 102783. KA2126 02 (FLT 0, LAUNCH DATE WDDYY., TAPEIN, FILE 0)
// EXEC NOTIFYS
```

*** END OF MEMBER *** 17 RECORDS PROCESSED *****

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26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.RADAR.CNTL

MEMBER=LISTJCLL

```
//Z8SACRAD JOB (L3006,620,4),'LIST RADAR 329',TIME=(1,0)
//*
//* RADAR.CNTL(LISTJCLL) USES THE LIB LOAD01 (OBJECT CODE) VERSION
//* OF THE LISTRAD PROGRAM (THE RADAR PROGRAM USED FOR ALL PASS1
//* RADAR TAPES), WHICH WAS COMPILED WITH A VS FORTRAN COMPILER.
//*
//*JOBPARM QUEUE=FETCH
//GO EXEC PGM=LISTRAD,REGION=512K
//STEPLIB DD DSN=Z8SAC.LIB.LOAD01,DISP=SHR
//FT06F001 DD SYSOUT=*
//SYSUDUMP DD SYSOUT=*,SPACE=(CYL,(1,1))
//SYSABEND DD SYSOUT=*,SPACE=(CYL,(1,1))
//FT05F001 DD DDNAME=DATA5
//
//GO.FT10F001 DD UNIT=(800,,DEFER),LABEL=(2,ML,,IN),VOL=SER=ERTAPI,
// DCB=(RECFM=FB,BLKSIZE=32,DEM=2,LRECL=32,EROPT=ACC),
// DISP=(OLD,KEEP)
//GO.DATAS DD *
329 020984. KAZ125 02 (FLT 0, LAUNCH DATE MDDYY., TAPEIN, FILE 0)
//
// EXEC NOTIFYTS
```

*** END OF MEMBER *** 21 RECORDS PROCESSED *****

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26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.RADAR.CNTL

MEMBER=SPJCL

```
//Z8SACRDR JOB (L3006,620,3),'SACRAD 316',TIME=(0,30)
//**
//** RADAR.CNTL(SPJCL) USES THE LIB LOAD01 (OBJECT CODE) VERSION
//** OF THE RADAR PROGRAM, WHICH WAS COMPILED WITH A FORTRAN M
//** COMPILER. (NOTE: THIS JCL CAN ONLY BE USED ON MESSUP RADAR TAPES)
//**
//** JOBPARM LINES=20,QUEUE=FETCH
//** EXEC OLINKGM,REGION=GO=200K
//** LINK.SYSLIB DD DSN=Z8SAC.LIB.LOAD01,DISP=SHR
//** LINK.SYSLIN DD *
//** INCLUDE SYSLIB(NRAD)
//** ENTRY MRAD
//** GO.FT10F001 DD UNIT=(800,,DEFER),LABEL=(,ML,,IN),VOL=SER=ERTAPI,
//** DCB=(RECFM=F,BLKSIZE=252,DEN=2,LRECL=252,EROPT=ACC),
//** DISP=(OLD,KEEP)
//** GO.FT11F001 DD UNIT=(2400-9,,DEFER),LABEL=(25,SL,,OUT),
//** DCB=(RECFM=FB,BLKSIZE=5200,DEN=3,LRECL=52),DISP=(NEW,KEEP),
//** VOL=SER=ERTAP0,DSN=Z8SAC.RADAR316
//** GO.DATAS DD *
//** KA2127 10 01 02 1500.00 316 09/15/83
//** KA2120 11 25
//** 101. 08/23/83 162500.0 37.850 -75.480 HALLOPS ISLAND
//**
//** EXEC NOTIFYTS
```

*** END OF MEMBER *** 24 RECORDS PROCESSED *****

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MEMBER=JCL

26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.EDIT.CNTL

```
//Z8SACEDT JOB (L3006,620,4),'EDIT FLT 320',TIME=(1,00)
//* EDIT.CNTL(JCL) COMPILES AND RUNS THE EDIT PROGRAM USING A
//* FORTRAN H COMPILER.
//*
//*JOBPARM LINES=20,QUEUE=FETCH
// EXEC OFORTH,PARM=XREF
//SOURCE.SYSIN DD DSN=Z8SAC.EDIT.CNTL(EDIT),DISP=SHR
// EXEC OLINKG0H,REGION=GO=300K
// GO.PLOTTAPE DD DCB=(,DEN=1),LABEL=(,BLP,,OUT),
// UNIT=(7TRACK,,DEFER),DISP=NEW,VOL=SER=KA2110,DSN=NULLFILE
//GO.FT10F001 DD UNIT=(800,,DEFER),LABEL=(4,NL,,IN),
// DCB=(RECFM=U,BLKSIZE=2440,DEN=2,EROPT=ACC),VOL=SER=ERTAPI,
// DISP=(OLD,KEEP)
//GO.FT15F001 DD UNIT=(2400-9,,DEFER),LABEL=(15,SL,,OUT),
// DCB=(RECFM=FB,DEN=3,BLKSIZE=8000,LRECL=80),
// VOL=SER=ERTAPO,DISP=(NEW,KEEP),DSN=Z8SAC.EDIT320
//GO.DATAS DD *
KA2130 INPUT 10 04
KA2115 OUTPUT 15 05 080
00.629 105 373 128 030 (DELTAT,IREC,MPEAK,LPEAK,LIMIT)
6.5 654.00 5.6 564.00 (B1,V1,B2,V2)
-19.0 9.78 23.0 4.03 50.0 1.71 (TEMP CAL. - T(I),VT(I),I=1,3)
320.0 479. 10/24/83 (FLT. #, PAYLOAD #, DATE RAW TAPE REC'D)
// EXEC NOTIFYS
```

*** END OF MEMBER ***

26 RECORDS PROCESSED

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26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.EDIT.CNTL

MEMBER=JCLL

```
//Z8SACEDT JOB (L3006,620,4),'EDIT 329',TIME=(1,0)
//*
** EDIT.CNTL(JCLL) USES THE LIB.LOAD01 (OBJECT CODE) VERSION
** OF EDIT, WHICH WAS COMPILED WITH A FORTRAN H COMPILER.
**
*JOBPARM QUEUE=FETCH,LINES=20
** EXEC OLINKGOH,REGION=GO=300K
**LINK.SYSLIB DD DSN=Z8SAC.LIB.LOAD01,DISP=SHR
** DD DSN=SYS2.WOLFLOT,DISP=SHR
**LINK.SYSLIN DD *
INCLUDE SYSLIB(MEDIT)
ENTRY MEDIT
/*
//GO.PLOTTAPE DD DCB=(,DEN=1),LABEL=(,BLP,,OUT),
// UNIT=(7TRACK,,DEFER),DISP=NEW,VOL=SER=KA2110,DSN=NULLFILE
//GO.FT10F001 DD UNIT=(800,,DEFER),LABEL=(4,NL,,IN),
// DCB=(RECFM=U,BLKSIZE=2440,DEN=2,EROPT=SKP),VOL=SER=ERTAPI,
// DISP=(OLD,KEEP)
//GO.FT15F001 DD UNIT=(2400-9,,DEFER),LABEL=(37,SL,,OUT),
// DCB=(RECFM=FB,DEN=3,BLKSIZE=8000,LRECL=80),
// VOL=SER=ERTAPO,DISP=(NEW,KEEP),DSN=Z8SAC.EDIT329
//GO.DATAS DD *
KA2125 INPUT 10 04
KA2122 OUTPUT 15 37 080
00.649 093 559 143 030 (DELTAT,IREC,MPEAK,LPEAK,LIMIT)
6.5 648.00 5.6 540.00 (B1,V1,B2,V2)
-20.0 9.95 23.0 4.24 50.0 1.77 (T(1),VT(1),...T(3),VT(3))
329.0 490. 03/05/84 (FLT.NO.,PAYLOAD,DATE TAPE R'CD)
/*
// EXEC NOTIFYTS
```

*** END OF MEMBER ***

30 RECORDS PROCESSED

26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.EDIT.CNTL

MEMBER=SPECJCL

```
//Z8SACEDT JOB (L3006,620,2),'SPECIAL EDIT 306',TIME=(0,30)
/*
/* THIS JCL IS USED IN SPECIAL CASES WHERE ONE WANTS TO
/* RUN THE LIB LOAD01 (OBJECT CODE COMPILED WITH FORTRAN H
/* COMPILER) VERSION OF EDIT BUT WANTS TO USE A SEPARATE
/* SOURCE CODE SUBROUTINE (BLOCK1, IN THIS CASE). IN
/* EDIT.CNTL(BLOCK1), ONE CAN STOP PROCESSING AFTER A CERTAIN
/* RECORD HAS BEEN REACHED.
/*
/*JOBPARM QUEUE=FETCH,LINES=20
/*SOURCE EXEC OFORTH,PARM=XREF
/*SOURCE.SYSIN DD DISP=SHR,DSN=Z8SAC.EDIT.CNTL(BLOCK1)
/*LOAD EXEC OLINKGOH,REGION=GO=300K
/*LINK.SYSLIB DD DSN=Z8SAC.LIB.LOAD01,DISP=SHR
/* DD DSN=SYS2.HOLFPLOT,DISP=SHR
/*LINK.OBJECT DD *
/* INCLUDE SYSLIB(MEDIT)
/* ENTRY MEDIT
/*
/*GO.PLOTTAPE DD DCB=(,DEN=1),LABEL=(,BLP,OUT),
/* UNIT=(7TRACK,,DEFER),DISP=NEW,VOL=SER=KA2110,DSN=NULLFILE
/*GO.FT10F001 DD UNIT=(800,,DEFER),LABEL=(,NL,,IN),
/* DCB=(RECFM=U,BLKSIZE=2440,DEN=2,EROPT=ACC),VOL=SER=ERTAPI,
/* DISP=(OLD,KEEP)
/*GO.FT15F001 DD DUMMY,
/* DCB=(RECFM=FB,DEN=3,BLKSIZE=8000,LRECL=80),
/* VOL=SER=ERTAP0,DISP=(NEW,KEEP),DSN=Z8SAC.EDIT306
/*GO.DATAS DD *
KA2126 INPUT 10 01
KA2144 OUTPUT 15 01 080
00.609 113 557 145 030
6.5 652.00 5.6 562.00
-20.0 10.02 22.0 4.23 50.0 1.76
306.0 460. 09/13/82
/*
/* EXEC NOTIFYS
```

*** END OF MEMBER *** 36 RECORDS PROCESSED *****

ORIGINAL COPY
OF POOR QUALITY

```

//Z8SACHER JOB (L3006,620,4),'MERGE FLT 321',TIME=(0,30)
//* MERGE.CNTL(JCL) COMPILES AND RUNS THE MERGE PROGRAM USING
//* A VS FORTRAN COMPILER.
//*
/*JOBPARM QUEUE=FETCH
// EXEC FORTVC,PARM=(XREF,NOFIPS,NOTRMFLG)
//SYSLIN DD DSN=Z8SAC.MERGE.CNTL(MERGE),DISP=SHR
// EXEC LINKGOV,REGION,GO=450K
//GO.FT15F001 DD UNIT=(2400-9,,DEFER),LABEL=(29,SL,,IN),
// VOL=SER=EDITED,DCB=(RECFM=FB,DEN=3,BLKSIZE=8000,LRECL=80),
// DISP=(OLD,KEEP),DSN=Z8SAC.EDIT321
//GO.FT10F001 DD UNIT=(2400-9,,DEFER),LABEL=(1,SL,,OUT),
// VOL=SER=MERGED,DCB=(RECFM=FB,DEN=3,BLKSIZE=8000,LRECL=80),
// DISP=(NEW,KEEP),DSN=Z8SAC.MER321
//GO.FT16F001 DD UNIT=(800,,DEFER),LABEL=(1,ML,,IN),
// VOL=SER=RADAR,DCB=(RECFM=FB,DEN=2,BLKSIZE=32,LRECL=32),
// DISP=(OLD,KEEP),DSN=Z8SAC.RAJAR321
//GO.DAT5 DD *
KA2122 29 15 00 (EDIT VOLSER #, FILE #, UNIT #)
KA2138 01 10 (MERGE VOLSER #, FILE #, UNIT #)
KA2126 01 16 02 (RADAR VOLSER #, FILE #, MODE)
321.0
1 WFC-1 CRR-2 NTL-3 PRL-4 0000.0 001 00 321 OCT. 27, 1983 1624Z
14.00 03.00 7.16 230.83 (RH,RM,RS,RACOR)
-12.00 30.00 39.00 -1221.40 (DD,DM,DS,DECOR)
2.00 19.00 8.88 16.00 (SH,SM,SS,HOURL)
0000.0 0000.0
0000.0 0000.0
0000.0 0000.0
/* THE FOLLOWING DATA LINES ARE USED FOR THE NEW PASS1 RADAR TAPES,
/* (FLIGHTS 316 AND ON) TO READ IN RADAR PEDIGREE INFORMATION DUE TO
/* THE RADAR TAPES BEING READ DIRECTLY INTO THE MERGE PROGRAM WITHOUT
/* BEING PREVIOUSLY REFORMATTED BY THE RADAR PROGRAM. THESE DATA
/* LINES ARE READ WHEN MODE 2 IS SPECIFIED. THE FOLLOWING FIELDS ARE:
/*
/* -100,FLT #,LAUNCH VEHICLE/SITE,LAUNCH DATE,LAUNCH TIME,LATITUDE,
/* LONGITUDE,DATE RADAR TAPE REC'D
//GO.FT20F001 DD *
-100. 321. 101. 102783. 162400.0 37.850 -75.480 021584.
HALLOPS ISLAND 1440.00 (SITE,STIME)
/* EXEC NTSO

```

*** END OF MEMBER *** 43 RECORDS PROCESSED *****

ORIGINAL FILED
OF POOR QUALITY

26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.MERGE.CNTL

MEMBER=JCLL

```

//Z8SACMER JOB (L3006,620,4),'MERGE FLT 329',TIME=(0,30)
//* MERGE.CNTL(JCLL) USES THE LIB.LOAD01 (OBJECT CODE) VERSION
//* OF THE MERGE PROGRAM, IN WHICH THE CODE WAS COMPILED WITH A
//* VS FORTRAN COMPILER.
//*
//JOBPARM QUEUE=FETCH
//GO EXEC PGM=MERGE,REGION=512K
//STEPLIB DD DSN=Z8SAC.LIB.LOAD01,DISP=SHR
//SYSDUMP DD SYSOUT=*
//SYSABEND DD SYSOUT=*
//FT05F001 DD DDNAME=DATA5
//GO.FT15F001 DD UNIT=(2400-9,,DEFER),LABEL=(37,SL,,IN),
// VOL=SER=EDITED,DCB=(RECFM=FB,DEN=3,BLKSIZE=8000,LRECL=80),
// DISP=(OLD,KEEP),DSN=Z8SAC.EDIT329
//GO.FT10F001 DD UNIT=(2400-9,,DEFER),LABEL=(36,SL,,OUT),
// VOL=SER=MERGED,DCB=(RECFM=FB,DEN=3,BLKSIZE=8000,LRECL=80),
// DISP=(NEW,KEEP),DSN=Z8SAC.MER329
//GO.FT16F001 DD UNIT=(800,,DEFER),LABEL=(2,NL,,IN),
// VOL=SER=RADAR,DCB=(RECFM=FB,DEN=2,BLKSIZE=32,LRECL=32),
// DISP=(OLD,KEEP),DSN=Z8SAC.RADAR329
//GO.DATAS DD *
KA2122 37 15 00 (EDIT VOLSER #, FILE #, UNIT #)
KA2117 36 10 (MERGE VOLSER #, FILE #, UNIT #)
KA2125 02 16 02 (RADAR VOLSER #, FILE #, UNIT #, MODE)
329.0
1 MFC-1 CRR-2 NTL-3 PRL-4 0000.0 001 00 329 FEB. 09, 1984 1845Z
21.00 27.00 21.67 238.59 (RH,RH,RS,RACOR)
-14.00 59.00 52.90 1148.10 (DD,DM,DS,DECOR)
9.00 13.00 07.43 18.00 (SH,SM,SS,HOURL)
0000.0 0000.0
0000.0 0000.0
0000.0 0000.0
//* THE FOLLOWING DATA LINES ARE USED FOR THE NEW PASS1 RADAR TAPES,
//* (FLIGHTS 316 AND ON) TO READ IN RADAR PEDIGREE INFORMATION DUE TO
//* THE RADAR TAPES BEING READ DIRECTLY INTO THE MERGE PROGRAM WITHOUT
//* BEING PREVIOUSLY REFORMATTED BY THE RADAR PROGRAM. THESE DATA
//* LINES ARE READ WHEN MODE 2 IS SPECIFIED. THE FOLLOWING FIELDS ARE:
//*
//* -100.,FLT #,LAUNCH VEHICLE/SITE,LAUNCH DATE,LAUNCH TIME,LATITUDE,
//* LONGITUDE,DATE RADAR TAPE REC'D
//GO.FT20F001 DD *
-100. 329. 101. 020984. 184500.0 37.850 -75.480 030584.
MALLOPS ISLAND 2700.00 (SITE,STIME)
// EXEC NTSO

```

*** END OF MEMBER *** 47 RECORDS PROCESSED *****

ORIGINAL PAGE 18
OF POOR QUALITY

MEMBER=JCL

26JUL84 13.53.47 - VOL=SACC09, DSN=Z8SAC.SM00.CNTL

```

//Z8SACSM0 JOB (L3006,620,7),'SMOOTH FLT 326',TIME=(0,30)
//** SMOO.CMTL(JCL) COMPILES AND RUNS THE SMOOTH PROGRAM USING
//** A FORTRAN H COMPILER.
//**
//**JOBPARM QUEUE=FEICH
// EXEC OFORTH,PARM='XREF'
//SOURCE.SYSIN DD DSN=Z8SAC.SM00.CNTL(SMOOTH),DISP=SHR
// EXEC OLINKGOH,REGION.GO=300K
//LINK.SYSLIB DD DSN=SYS2.MOLFPLOT,DISP=SHR
//**
//GO.PLOTTAPE DD DCB=(,DEN=1),LABEL=(,BLP,,OUT),UNIT=(7TRACK,,DEFER),
// DISP=NEW,VOL=SER=KA2110,DSN=NULLFILE
//GO.FT10F001 DD UNIT=(2400-9,,DEFER),LABEL=(33,SL,,IN),
// DCB=(RECFM=FB,BLKSIZE=8000,LRECL=80),VOL=SER=ERTAPI,
// DISP=(OLD,KEEP),DSN=Z8SAC.MER326
//GO.FT15F001 DD UNIT=(2400-9,,DEFER),LABEL=(2,SL,,OUT),
// DISP=(NEW,KEEP),DCB=(RECFM=FB,BLKSIZE=4000,LRECL=80),
// VOL=SER=ERTAPO,DSN=Z8SAC.SM00326
//GO.FT03F001 DD UNIT=SYSDA,SPACE=(TRK,(58,5)),DISP=(NEW,DELETE),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=7280),DSN=MERGEXX
//GO.DAT5 DD *
KA2117 33 10 80
KA2138 02 15
00(MODE=1-INSTRUM, 0-NONE, -1-STATIST ) 1-(50 REFERENCE; 0-NO,1-YES)00000190
69.0 13.0 213. 0051 (ALT. RANGE-KM,COMPAN.# BAD MERGE RECS)
0000.0 0000.0 0000.4 0001.4 (ZERO OFFSETS: S0,S1,S2,S3)
0014.0 0002.0 0000.4 0001.3 (TA,TB,S2B,S3B)
326.
//** EXEC NTSO

```

*** END OF MEMBER *** 31 RECORDS PROCESSED *****

ORIGINAL FILED
OF POOR QUALITY

26JUL84 08.53.47 - VOL=SACC09, DSN=Z8SAC.SM00.CNTL

MEMBER=JCLL

```
//Z8SACSMO JOB (L3006,620,6),TEST2 SMOOTH 327',TIME=(0,30)
//* SMOO.CNTL(JCLL) USES THE LIB.LOAD01 (OBJECT CODE) VERSION
//* OF THE SMOOTH PROGRAM, WHICH WAS COMPILED WITH A FORTRAN H
//* COMPILER.
//*
//*JOBPARM QUEUE=FETCH
// EXEC OLINKG0H,REGION.G0=300K
// LINK.SYSLIB DD DSN=SYS2.MOLFPLOT,DISP=SHR
// LINK.SYSLIB DD DSN=Z8SAC.LIB.LOAD01,DISP=SHR
// LINK.SYSLIN DD *
// INCLUDE SYSLIB(MSMOOT)
// ENTRY MSMOOT
//
//GO.PLOTTAPE DD DCB=(,DEN=1),LABEL=(,BLP,,OUT),UNIT=(7TRACK,,DEFER),
// DISP=NEW,VOL=SER=KA2110,DSN=NULLFILE
//GO.FI10F001 DD UNIT=(2400-9,,DEFER),LABEL=(34,SL,,IN),
// DISP=(OLD,KEEP),DCB=(RECFM=FB,BLKSIZE=8000,LRECL=80),
// VOL=SER=ERTAPI,DSN=Z8SAC.MER327
//GO.FI15F001 DD UNIT=(2400-9,,DEFER),LABEL=(3,SL,,OUT),
// DISP=(NEW,KEEP),DCB=(RECFM=FB,BLKSIZE=4000,DEN=3,LRECL=80),
// VOL=SER=ERTAPO,DSN=Z8SAC.SM00327
//GO.FI03F001 DD UNIT=SYSDA,SPACE=(TRK,(58,5)),DISP=(NEW,DELETE),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=7280),DSN=MERGEXXX
//GO.DAT05 DD *
KA2117 34 10 80
KA2123 03 15
00(MODE1-INSTRUM, 0-NONE,-1-STATIST ) 1-(SO REFERENCE; 0-NO,1-YES)
66.0 10.0 208. 0058 (ALT. RANGE-KM,COMPAN.# BAD MERGE RECS)
0000.0 0002.0 0011.0 0021.0 (ZERO OFFSETS: S0,S1,S2,S3)
0011.0 0011.0 0011.0 0021.0 (TA,TB,S2B,S3B)
327.
//
// EXEC NTS0
```

*** END OF MEMBER *** 34 RECORDS PROCESSED *****

ORIGINAL COPY
OF POOR QUALITY

MEMBER=JCL1325

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

```
//L3EIRPRO JOB (L3006,620,4),' FLT 325 PROFILE',TIME=(2,00)
//*JOBPARM QUEUE=FETCH
// EXEC OFORTH,PARM='NCAL,XREF'
//SOURCE.SYSIN DD DSN=L3EIR.PROF.CNTL(PROFILE),DISP=SHR
//          DD DSN=L3EIR.PROF.CNTL(DIMARRY),DISP=SHR
// EXEC OLINKGOH,REGION=GO=300K
//LINK.SYSLIB DD DSN=SYS2.WOLFLOT,DISP=SHR
//          DD DSN=L3EIR.LIB.LOAD01,DISP=SHR
//*
//GO.FT09F001 DD SYSOUT=A
//GO.FT10F001 DD UNIT=(2400-9,,DEFER),LABEL=(10,SL,,IN),
//VOL=SER=ERTAP1,DISP=(OLD,KEEP),DSN=ZASAC.SMOO325,
//DCB=(RECFM=FB,DEN=3,BLKSIZE=4000,LRECL=80,EROPT=SKP)
//GO.FT15F001 DD UNIT=(2400-9,,DEFER),LABEL=(10,SL,,OUT),
//DCB=(RECFM=FB,DEN=3,BLKSIZE=4000,LRECL=80),VOL=SER=ERTAP0,
//DISP=(NEW,KEEP),DSN=L3EIR.PROF325
//*
//* THE FOLLOWING DISK FILES WILL ONLY BE USED WHEN NOT PRECEDED BY
//* 'X': (IN ORDER TO USE THESE DISK FILES, CHANGE 'XGO' TO 'GO')
//*GO.FT31F001 DD DSN=L6VBZ.MCFLUX,DISP=SHR,LABEL=(,,,IN)
//*GO.FT32F001 DD DSN=L6VBZ.DIFFSR,DISP=SHR,LABEL=(,,,IN)
//*GO.FT33F001 DD DSN=L6VBZ.DETECT,DISP=SHR,LABEL=(,,,IN)
//*GO.FT34F001 DD DSN=L6VBZ.RAYLEIGH,DISP=SHR,LABEL=(,,,IN)
//*GO.FT35F001 DD DSN=L6VBZ.MCARIDE,DISP=SHR,LABEL=(,,,IN)
//*GO.FT36F001 DD DSN=L6VBZ.BAS,DISP=SHR,LABEL=(,,,IN)
//*GO.FT37F001 DD DSN=L6VBZ.BASS243,DISP=SHR,LABEL=(,,,IN)
//*GO.DAT5 DD *
A 325.0 KA2116 010 KA2113 010 00/00/83 BARR 00000 000489
B 03 58.0 39.0 2653.0 133.0 194.8620 -3073.27000 -23416.40000 2.07930
B 02 49.0 30.0 2923.0 91.0 32.7789 -72.54570 158.06100 1.36420
B 01 44.0 19.0 3008.0 71.0 8.2503 -3.86985 2.06072 1.20600
B 00 40.0 19.0 3067.0 68.0 3.1370 -0.50358 .07242 1.10980
B 00 58.0 39.0 191.7250 -3072.76650 -23416.47242 0.96950
B 20 49.0 30.0 29.6419 -72.04212 157.98858 0.25440
B 10 44.0 19.0 5.1134 -3.36627 1.98830 0.09620
C 11/22/83 260.0 253.0 DOBSON DATA AND VALUES - MILLI-ATM-CM
D 11-0771 11/22/83 1530 060 18666.0 205.10 70.00 DATASONDE
E 70000. -38.70 15.0 ALT(M) TEMP C ; TEMP ERROR (TWO SIGMA). DEG.
E 69000. -40.60 13.0 IF NOT GIVEN WITH PROFILE, ERROR MAY BE TAKEN
E 68000. -40.70 11.4 FROM SCHMIDLIN, JGR,86,9599,1981.
E 67000. -36.90 9.9 ALTITUDE MUST BE DESCENDING.
E 66000. -33.10 8.6
E 65000. -28.90 7.5
E 64000. -26.10 6.3
E 63000. -23.80 5.4
E 62000. -21.90 4.6
E 61000. -19.70 3.9
E 60000. -20.20 3.3
E 59000. -18.00 3.9
E 58000. -14.60 2.6
E 57000. -11.40 2.3
E 56000. -16.70 2.0
E 55000. -17.80 1.8
E 54000. -16.50 1.8
E 53000. -16.80 1.8
E 52000. -16.70 1.8
```

ORIGINAL
OF POU

00000580
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00000660
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00000730
00000740
00000750
00000760
00000770
00000780

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1.1
1.1
1.0
1.0

-15.70
-16.40
-17.70
-19.10
-20.20
-20.60
-21.80
-23.80
-23.30
-26.50
-30.90
-33.10
-35.90
-36.50
-38.50
-41.50
-40.80
-42.60
-45.00
-45.50

51000.
50000.
49000.
48000.
47000.
46000.
45000.
44000.
43000.
42000.
41000.
40000.
39000.
38000.
37000.
36000.
35000.
34000.
33000.
32000.
31000.

```
30000. -46.90 0.9
29000. -48.60 0.9
28000. -52.70 0.9
27000. -54.60 0.9
26000. -56.30 0.9
25000. -59.20 0.9
24000. -59.80 0.9
23000. -62.00 0.9
22000. -62.20 0.9
21000. -63.50 0.9
20000. -64.20 0.9
F -1.
  4A0326 11/22/83 1500 22000. 0.09096 1ST ECC SONDE
    167 27.5 1000. 289.0
    1532 38.6 850. 283.5
    3121 26.0 700. 273.1
    5758 21.1 500. 259.4
    7415 17.1 400. 247.0
    9439 17.5 300. 233.2
    10661 19.0 250. 225.2
    12128 11.1 200. 221.7
    13963 10.3 150. 213.8
    16458 21.2 100. 208.0
    18607 66.3 70. 205.1
    19543 90.4 60. 208.9
    20669 114.5 50. 212.1
    22056 134.6 40. 212.9
    23858 145.1 30. 216.4
    25013 130.4 25. 216.4
    26440 110.2 20. 220.0
    28308 84.1 15. 222.5
    31008 61.0 10. 230.6
H250. 0.02635 125. 0.03328 62.5 0.05307 COLUMN CONTENT UP TO STATED PR
F 4A0327 11/22/83 1720 22000. 0.08950 2ND ECC SONDE
    160 17.7 1000. 290.1
    1530 35.9 850. 285.4
    3126 26.7 700. 274.3
    5768 20.4 500. 259.3
    7422 17.3 400. 247.2
    9447 15.2 300. 232.5
    10670 22.7 250. 226.0
    12134 9.9 200. 221.9
    13966 8.6 150. 213.0
    16438 19.2 100. 207.4
    18594 80.5 70. 208.4
    19539 89.7 60. 211.3
    20667 110.5 50. 211.1
    22043 127.0 40. 211.9
    23855 132.5 30. 216.6
    25023 116.6 25. 219.9
    26465 85.3 20. 220.9
    28373 66.7 15. 227.2
    31111 41.1 10. 233.8
H250. 0.02589 125. 0.03190 62.5 0.05299 COLUMN CONTENT UP TO STD PRES'S
// EXEC NOTIFYS
```

ORIGINAL FILED
OF POOR QUALITY

PROGRAM LISTINGS

RAW	IV-22
RAW	IV-22
RADAR.	IV-29
COPY1	IV-29
LISTRAD	IV-33
RADAR	IV-34
EDIT	IV-39
BLOCK1	IV-39
EDIT.	IV-42
MERGE.	IV-63
MERGE	IV-63
SMOOTH	IV-80
SMOOTH	IV-80
PROFILE	IV-101
ALFEFF	IV-101
CARDS	IV-109
CFTWRT	IV-115
CHECKS	IV-118
COMPST	IV-127
DATSND	IV-131
DINARRY	IV-134
INARRY	IV-135
LINFIT	IV-138
MODEL	IV-141
OVERLP	IV-144
OVRBRD	IV-147
OZDENS	IV-150
PROFILE	IV-159
PRTPED	IV-162
PRTPRF	IV-163
PRTSAV	IV-164
PRTSMT	IV-166
PRTWRT	IV-168
RELATD	IV-173
SECANG	IV-176
SHAPE	IV-178
SLANTA	IV-179
TAPE	IV-182
TAPWRT	IV-185

PRECEDING PAGE BLANK NOT FILMED

```

*****
READ RAM OZONE (M.F.C.)      4/17/78      6/01/81      10/25/82
EDITION: 2
LANGUAGE:  FORTRAN
COMPUTER:  IBM 360/75, 360/      3081
OPERATING SYSTEM:  G. S. F. C.
PROGRAMMER:  EUGENE H. SHAFFER/SASC      TEMARI
S. COOKE,    CHANGED MWRD=0 TEST; AFTER REC 210,      E. REED
              PRINT ONLY 1 OUT OF 100; ADDED EOF      3/3/83
              STATEMENT
              ADDED INCR; LIST FIRST DATA; MODIFIED      4/18/83
              FORMATS
*****

```

PURPOSE:
A PROGRAM TO READ AND DUMP THE RAM DIGITAL DATA THAT
HAS BEEN DIGITIZED AT THE COMPUTER FACILITIES OF HALLOPS
SPACE FLIGHT CENTER.

VARIABLES:

NAME	TYPE	I/O	DESCRIPTION
------	------	-----	-------------

INTERNAL			
DIF	R#4	0	TIME DIFFERENCE BETWEEN BLOCKS
ELAPSE	R#4	0	ELAPSED TIME FROM LAUNCH OF BLOCK
IDBEGIN	IN#4	I	BEGINNING RECORD NUMBER
ID	IN#1	I	HEADER RECORD INFORMATION
IDAY	IN#4	I	JULIAN DAY
IHR	IN#4	I	HOUR OF THE DAY
INPUT	IN#1	I	DATA INFORMATION
IMIN	IN#4	I	MINUTE OF THE HOUR
ISEC	IN#4	I	SECOND OF THE MINUTE
MSEC	IN#4	I	MILLI-SECONDS OF THE SECOND
ISTOP	IN#4	I	LAST RECORD NUMBER
IUNIT	IN#4	I	TAPE UNIT NUMBER
LD	IN#1	I	DATA INFORMATION RECORD
NF	IN#4	I	FILE NUMBER OF TAPE
NX	IN#4	I/O	R#4 FORM OF DATA
SEC	R#4	0	TOTAL NUMBER OF SECONDS
TAPEIN	IN#1	I	INPUT TAPE
TIME	R#4	0	ELAPSED TIME OF EACH RECORD
INCR	IN#4	I	INCREMENT BETWEEN PRINTED SAMPLES

SUBROUTINES CALLED

```

MOUNT
FREAD
TIME1

```

LOGICAL#1 IN1(2),OUT1(2),TAPEIN(6)

ORIGINAL FILE IS
OF POOR QUALITY

ORIGINAL FILED
OF POOR QUALITY

```
INTEGER*2 INPUT(1220), IN2, OUT2, ID(46), LD(20)  
INTEGER*4 NX(1220)  
EQUIVALENCE (IN1(1), IN2), (OUT1(1), OUT2)  
LSTM = 110
```

C
C

```
C READ IN TAPE INFORMATION.
```

```
READ (5,1000) TAPEIN,NF, IVER,NFLIT  
READ (5,1010) ISAMP, IBEGIN, ISTOP, INCR  
READ (5,1020) TIMES, TIME2  
WRITE (6,2030)  
WRITE (6,2040)  
WRITE (6,2030)  
WRITE(6,2050) NFLIT, TAPEIN, NF, IVER  
IF(IVER.EQ.1) WRITE(6,2051) ISAMP, IBEGIN, ISTOP, INCR  
IF(IVER.EQ.2) WRITE(6,2052) TIMES, TIME2  
WRITE (6,2050)
```

C
C

```
C INITIALIZE PARAMETERS.
```

```
C IUNIT=10
```

00000510
00000520
00000530
00000532
00000540
00000550
00000560
00000570
00000580
00000590
00000600
00000610
00000620
00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700


```

L=0
IDAY=0
IMR=0
IMIN=0
ISEC=0
NCOUNT=0
SEC=0.

C MOUNT TAPE AND READ THE HEADER AND DATA INFORMATION RECORDS.
C
CALL MOUNT (1,IUNIT,TAPEIN,MF)
CALL FREAD (ID,IUNIT,LEN,M999,M100)
CALL BCD5(ID,LD,40)
DO 10 I=2,6
  IN2=ID(I)
  OUT1(2)=IN1(1)
  OUT1(1)=IN1(2)
  ID(I)=OUT2
  WRITE(6,2060) ID(3),ID(2),ID(6),LD(4),LD(5),(LD(I),I=7,46)
10 CONTINUE
CALL FREAD (LD,IUNIT,LEN,M999,M200)
CALL BCD5(LD(4),ID(4),8)
DO 20 I=1,28
  IN2=LD(I)
  OUT1(2)=IN1(1)
  OUT1(1)=IN1(2)
  LD(I)=OUT2
20 WRITE(6,2065) LD(3),LD(2),(LD(I),I=8,19),(ID(J),J=4,7)
200 CONTINUE

C READ IN DATA.
C
30 CALL FREAD (INPUT,IUNIT,LEN,M999,M200)
  I=L+1
C THE FOLLOWING STATEMENT . IF(L .LE. N) * CAN BE USED ON DIFFERENT
C FLIGHTS TO SKIP BEGINNING RECORDS.
  IF (L .LE. 24) GO TO 30
  CALL BCD5(INPUT(4),ID(1),2)
  CALL BCD5(INPUT(5),ID(2),2)
  DO 300 I=1,1220
    IN2=INPUT(I)
    OUT1(2)=IN1(1)
    OUT1(1)=IN1(2)
    INPUT(I)=OUT2
  300 NX(I)=INPUT(I)
  WRITE(6,2070) L,INPUT(2),INPUT(3),ID(1),ID(2),(INPUT(K),K=6,8)
  NX(1220)=NX(1220)+1

C COMPUTE TIME OF CURRENT BLOCK.
C
CALL TIME1 (1,NX(19),IDAY,IMR,IMIN,ISEC,SEC)
CALL TIME1 (2,NX(20),IDAY,IMR,IMIN,ISEC,SEC)
CALL TIME1 (3,NX(21),IDAY,IMR,IMIN,ISEC,SEC)
TIME=(60.*(FLOAT(IMIN)))+(FLOAT(ISEC))+SEC
N=0
DO 320 I=11,1210,11

```

ORIGINAL PAGE 18
OF POOR QUALITY

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320 IF(INCJ(I).EQ.0 .OR. INPUT(I).EQ.1023) N = N +1
    WRITE(6,2020) IDAY,IHR,IMIN,ISEC,SEC,N
    IF (LSTN.GT.50 .AND. N.LE.50) GO TO 330
    IF (L .LT. IBEGIN .AND. IVER .EQ. 1) GO TO 200
    IF (L .EQ. 1 .AND. IVER .EQ. 2) GO TO 200
330 LSTN = N
    ISTART=1)
    IEND=18
    IF (TIME .LT. TIMES.AND. IVER.EQ.2) GO TO 200
    IF (TIME.GT.TIME2.AND. IVER.EQ.2) GO TO 999
    WRITE OUT INFORMATION FOR EACH FRAME OF DATA.
    C
    C
    WRITE(6,2010)
    DO 350 I=1,110
    CALL TIME1(1,NX(ISTART+8),IDAY1,IHR1,IMIN1,ISEC1,SEC1)
    CALL TIME1(2,NX(ISTART+9),IDAY1,IHR1,IMIN1,ISEC1,SEC1)
    TIME=(60*IMIN1+ISEC1)+SEC1
    WRITE(6,2000) IDAY,IHR,IMIN1,ISEC1,SEC1,TIME,
    + (NX(I)),II=ISTART,IEND)
    ISTART=IEND+4
    00001334
    00001336
    00001337
    00001338
    00001340
    00001350
    00001420
    00001430
    00001450
    00001460
    00001470
    00001480
    00001490
    00001500
    00001510
    00001520
    00001530
    00001540
    00001550
    00001560
    00001570

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```

IEND=ISTART+7
350 CONTINUE
  IF (L .GE. ISTOP .AND. IVER .EQ. 1) GO TO 500
  GO TO 200
500 IBEGIN=IBEGIN+INCR
  ISTOP=ISTOP+INCR
  IF (IBEGIN.LT. 210) GO TO 510
  IBEGIN = IBEGIN + INCR
  ISTOP = ISTOP + INCR
510 NCOUNT=NCOUNT+1
  IF (NCOUNT.LT. ISAMP) GO TO 200
999 CONTINUE
  WRITE (6,2999) L
  STOP
1000 FORMAT (6A1,2X,I2,2X,I1,2X,I4)
1010 FORMAT (I3,2X,I4,2X,I4,1X,I4)
1020 FORMAT (F6.1,2X,F6.1)
2000 FORMAT (1X,5X,4(I5,2X),F6.4,3X,F10.4,8(3X,I6))
2010 FORMAT ('S',7X,'SI',5X,'COMP',7X,'S4',7X,'S5',5X,'BATT
1'S0',7X,'S1',5X,'COMP',7X,'S4',7X,'S5',5X,'BATT
2'UNCOMP')
2050 FORMAT('0','FLIGHT NUMBER',I6,3X,'TAPE ',6A1,2X,'FILE ',I3,10X,
1'PRINT VERSION',I5)
2030 FORMAT (1X,100('X'))
2040 FORMAT('/',1X,'PROGRAM TO SAMPLE RAW OZONE TAPE (REVISED OCT.1982)',
1/)
2051 FORMAT('0','PRINT',I4,' SAMPLES, RECORDS',I5,' TO',I5,
1' EVERY ',I5,' RECORDS')
2052 FORMAT(1X,'PRINT FROM',F7.2,' TO',F7.1,' SECONDS')
2060 FORMAT('0','RECORD',I6,' HAS',I6,' WORDS. TAPE',I6,2X,2A2,2X,40A2)
2065 FORMAT('0','RECORD WORDS DT/FR FR/BF SCALE MR/FR WD/FR PRE 8',
1'BFAPP INPUT OUTPUT 17 18 19 RUN STREAM',/,1X,I4I6,2X,
2A2,3X,2A2/)
2070 FORMAT(1X,I4,I6,' WORDS, BLOCK',I6,' STREAM ',2A2,' PR/AP',I6,
1' DATA BF',I6,' STAT ',22)
2020 FORMAT('+',80X,'START',I4,' D',I3,' HR',I3,' MN',I3,'+',F6.3,
1' SEC. WD1=0,F',I4)
2999 FORMAT('OEOF AFTER RECORD',I7)
END
C*****
C SUBROUTINE TIME1 4/3/78 6/1/81
C PROGRAMMER: EUGENE H. SHAFFER TEWARI
C
C PURPOSE:
C TO COMPUTE THE ELAPSED TIME FROM LAUNCH OF EACH
C BLOCK OF DATA.
C
C CALLING SEQUENCE:
C CALL TIME1 (M,LX,IDAY,IHR,IMIN,ISEC,SEC)
C
C *****
C
C VARIABLES:
C NAME TYPE I/O DESCRIPTION
C ---- --
C INTERNAL IDAY I*4 0 DAY OF THE YEAR
C

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C      IHR      I*4      0      HOUR OF THE DAY      00002140
C      IMIN     I*4      0      MINUTE OF THE HOUR     00002150
C      ISEC     I*4      0      SECOND OF THE MINUTE    00002160
C      LX       I*4      I      TIME WORD TO BE ANALYSED 00002170
C      M        I*4      I      INDICATOR FOR TYPE OF TIME WORD 00002180
C      SEC      R*4      0      TOTAL NUMBER OF SECONDS 00002190
C*****00002200
C*****00002210
C*****00002220
C*****00002230
C*****00002240
C*****00002250
C*****00002260
C*****00002270
C*****00002280
C*****00002290
C*****00002300
C*****00002310
C*****00002320
C*****00002330
C*****00002340

C      SUBROUTINES CALLED
C      SHFTR,SHFTL
C*****
C      SUBROUTINE TIME1 (M,LX,IDAY,IHR,IMIN,ISEC,SEC)
C      INTEGER SHFTR,SHFTL
C      IF (LX .LT. 0) LX=65535+LX
C      IF (M .EQ. 2) GO TO 200
C      IF (M .EQ. 3) GO TO 300
C      100 CONTINUE

```

26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.RAW.CNTL

MEMBER=RAW

```
C      COMPUTE NUMBER OF MILLI-SECONDS
C
C      JSEC=((SHFTR(SHFTL(LX,28),28))+(SHFTR(SHFTL(LX,20),28))*10)
C      + (SHFTR(LX,12)*100)
C      SEC=(FLOAT(JSEC))/1000.
C      GO TO 500
C      200 CONTINUE
C
C      COMPUTE THE NUMBER OF MINUTES AND SECONDS
C
C      IMIN=((SHFTR(SHFTL(LX,17),29))*10)+(SHFTR(SHFTL(LX,20),28))
C      ISEC=(SHFTR(SHFTL(LX,24),28))*10+(SHFTR(SHFTL(LX,28),28))
C      GO TO 500
C      300 CONTINUE
C
C      COMPUTE THE NUMBER OF DAYS AND HOURS
C
C      IDAY=(SHFTR(LX,14)*100)+(SHFTR(SHFTL(LX,18),28))*10)
C      + (SHFTR(SHFTL(LX,22),28))
C      IHR=(SHFTR(SHFTL(LX,26),30))*10+(SHFTR(SHFTL(LX,28),28))
C      500 CONTINUE
C      RETURN
C      END
```

*** END OF MEMBER *** 257 RECORDS PROCESSED

ORIGINAL PAGE 1
OF POOR QUALITY

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*****
RADAR COPY1 PROGRAM  4/07/83
*****
LANGUAGE:          FORTRAN
COMPUTER:          IBM 3081
OPERATING SYSTEM:  G.S.F.C.
PROGRAMMER:        SHIRLEY COOKE
*****
PURPOSE:
  THIS PROGRAM COPIES VARIOUS RADAR OUTPUT RECORDS FROM
  ORIGINAL RADAR OUTPUT TAPE. (ORIGINAL OUTPUT TAPE
  NEEDS MODIFYING; THIS PROGRAM COPIES THOSE RECORDS
  WHICH DO NOT REQUIRE ANY CHANGES.)
*****
*****
VARIABLE LIST
*****
NAME      TYPE  I/O  DESCRIPTION
----      -
IUNIT     Ix4   I    INPUT TAPE UNIT NUMBER
IUNIT2    Ix4   I    OUTPUT TAPE UNIT NUMBER
NF        Ix4   I    INPUT TAPE FILE NUMBER
NF2       Ix4   I    OUTPUT TAPE FILE NUMBER
R(13)     Rx4   I    NUMBER OF FILES ON INPUT TAPE
TIME      Rx4   I    RADAR DATA ARRAY
TAPEIN(6) Lx1   I    TIME CORRECTION
TAPOUT(6) Lx1   I    INPUT TAPE NAME
PED(13)   Rx4   I    PEDIGREE ARRAY NAME
*****
SUBROUTINES CALLED
MOUNT
FREAD
RPDATO
FWRITE
*****
INTEGER ERROR(50)
LOGICAL*1 TAPOUT(6),TAPEIN(6)
LOGICAL*4 SITE(4)
EQUIVALENCE (PED(10),SITE(1))
DIMENSION R(13),IYMD(3),IDATE(3),PED(13)
*****
C READ IN INPUT AND OUTPUT TAPE INFO.
C
C READ (5,1020) TAPEIN,IUNIT,NF,NFILE,STIME
C WRITE (6,2020) TAPEIN,IUNIT,NF
C READ (5,1000) TAPOUT,IUNIT2,NF2
C WRITE (6,1030) TAPOUT,IUNIT2,NF2
C
C MOUNT TAPES, AND INITIALIZE VARIABLES.
C CALL MOUNT(1,IUNIT,TAPEIN,NF)
*****

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00000744
00000746
00001360
00001370
00001380
00001390
00001400
00001410

```

CALL MOUNT(2,IUNIT2,TAPOUT,NF2)
KNTRC = 0
KNTRR = 0
LINES = 0

C READ PEDIGREE FROM INPUT TAPE AND MAKE MODIFICATIONS TO
C CURRENT DATE.
CALL FREAD(PED,IUNIT,LEN,8122,8124)
CALL RPDAT0(1,IYMD)
PED(9) = IYMD(2)*10000 + IYMD(3)*100 + IYMD(1)

C MAKE PRINTOUT OF PEDIGREE AND COPY IT ONTO NEW RADAR OUTPUT TAPE.
WRITE(6,2065) (PED(KZ),KZ=1,9),SITE
CALL FWRITE(PED,IUNIT2,LEN)
WRITE(6,2035) NFILE, STIME

C PRINT HEADINGS.
WRITE(6,2060)
WRITE(6,2045)
WRITE(6,2050)

C READ INPUT TAPE DATA AND MAKE PRINTOUT OF IT. COPY DATA ONTO
C OUTPUT TAPE.

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OF POOR QUALITY

```

100 CONTINUE
CALL FREAD(R,IUNIT,LEN,&150,&130)
CALL FWRITE(R,IUNIT2,LEN)
KNTREC = KNTREC + 1
LINES = LINES + 1
IF (LINES .LE. 78) GO TO 120
LINES = 1
WRITE (6,2055)
WRITE (6,2045)
WRITE (6,2050)
120 WRITE (6,2010) R
122 GO TO 100
122 WRITE (6,2122)
STOP
124 WRITE (6,2124)
STOP
130 CONTINUE
KNTERR = KNTERR + 1
WRITE (6,2040)
ERROR(KNTERR) = KNTREC + 1
GO TO 100
150 CONTINUE
WRITE (6,2030) KNTREC,KNTERR
IF (KNTERR .LE. 0) GO TO 200
WRITE (6,2070)
DO 160 I=1,KNTERR
  WRITE (6,2075) ERROR(I)
CONTINUE
160 WRITE (6,2080)
2000 FORMAT(1X,6A1,6X,12,3X,12)
1010 FORMAT(12X,F10.4,2X,F10.0,A1,1X,2(F10.4,A1,1X),
1 3(F10.0,A1,1X),12X,F10.0,A1,1X,24X,
2 4(F10.0,A1,1X),12X,F10.4,A1,1X)
1020 FORMAT(1X,6A1,6X,12,3X,12,3X,12,4X,F7.2,3X,13,3X,12,1X,12,1X,12)
1030 FORMAT(1X,2X,TAPEOUT: ',6A1,5X,UNIT: ',13,5X,'FILE: ',13)
1035 FORMAT(1X,F4.0,2X,12,1X,12,1X,12,2X,F8.1,2X,F7.3,2X,F8.3,2X,4A4)
2010 FORMAT(1X,F10.4,F10.1,2F10.4,8F10.1,F10.4)
2020 FORMAT(1X,2X,TAPEIN: ',6A1,5X,UNIT: ',13,5X,'FILE: ',13)
2030 FORMAT(1X,5X,'NUMBER OF RECORDS WRITTEN: ',15,/,
1 1X,5X,'NUMBER OF ERROR RECORDS: ',15,/,
2035 FORMAT(1X,5X,'NUMBER OF FILES TO PROCESS: ',13,/,
1 1X,5X,'TIME CORRECTION: ',F9.2,/,/)
2040 FORMAT(1X,'RADAR 2040: TAPE RECORD ERROR, PROCESSING CONTINUING')
2045 FORMAT(1X,'SECONDS ',4X,'SLANT ',3X,'AZIMUTH ELEVATION',
1 6X,'HOR ',6X,'N-S ',6X,'E-W ',2X,'ALTITUDE ',7X,'HOR ',7X,
2 'E-W ',7X,'N-S ',6X,'VERT ',3X,'HOR VEL ')
- 2050 FORMAT(1X,'AFTER HOUR ',2X,'RANGE DEGREES DEGREES ',5X,
1 'RANGE ',4X,'RANGE ',4X,'RANGE DBL.SPH.',7X,'VEL ',7X,'VEL ',
2 7X,'VEL ',6X,'VEL ',3X,'AZIMUTH')
2055 FORMAT(1X,'DISTANCE IN METERS, VELOCITIES IN METERS/SECOND',/)
2060 FORMAT(40X,'VEH/LOC ',5X,'FLT DATE ',5X,'GNT TIME',
2065 FORMAT(1X,'LAT ',6X,'LONG ',5X,'TAPE RCD ',5X,'RUN DATE ',5X,
1 5X,'LAUNCH LOCATION',/,
2 'LAUNCH LOCATION',/,
3 1X,1X,F5.0,5X,F4.0,5X,F4.0,8X,F7.0,5X,F8.1,3X,F7.3,2X,F8.3,
4 4X,F7.0,6X,F7.0,5X,4A4,/)
2070 FORMAT(1X,5X,'THE FOLLOWING ARE RECORD NUMBERS OF RECORDS WITH INP00001940

```



```

-UT ERRORS; ,/)
2075 FORMAT(1X,30X,15)
2080 FORMAT(//,1X,120('X'))
2122 FORMAT (1X, ' PEDIGREE NOT FOUND IN FIRST RECORD. ' )
2124 FORMAT (1X, ' ERROR IN READING PEDIGREE RECORD. ' )
STOP
END

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```

00001950
00001960
00001970
00001972
00001974
00001980
00001990

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*** END OF MEMBER *** 141 RECORDS PROCESSED *****

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26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.RADAR.CNTL

MEMBER=LISTRAD

```
C      RADAR.CNTL(LISTRAD)
C
C      S. COOKE          OCT., 1983
C
C      LISTRAD PRINTS OUT THE WORDS ON THE INPUT RADAR TAPE (USED
C      FOR ALL PASSI TAPES FOR FLIGHTS AFTER 315, EXCLUSIVE)
C
C      LOGICAL#1 TAPEIN(6)
C      REAL#8 RADAR(4)
C
C      IREC = 6
C      READ AND PRINT OUT HEADING INFORMATION.
C      READ(5,1000) IFLT,DATE,TAPEIN,NFILE
C      1000 FORMAT(1X,13,2X,F7.0,2X,6A1,2X,12)
C      WRITE(6,2000) IFLT,DATE,TAPEIN,NFILE
C      2000 FORMAT('1 FLIGHT NO. ',13,5X,'DATE LAUNCHED (MMDDYY.): ',
C      X F7.0,5X,'INPUT TAPE NO.: ',6A1,5X,'FILE NO.: ',12,/)
C      WRITE(6,2010)
C      2010 FORMAT(1X,'SEC ELAPSED',4X,'HEIGHT',4X,'LATITUDE',2X,
C      X 'LONGITUDE',/)
C
C      MOUNT INPUT TAPE
C      CALL MOUNT(1,10,TAPEIN,NFILE)
C
C      READ AND PRINT OUT EACH RECORD.
C      DO 50 N = 1,3000
C      CALL FREAD(RADAR(1),10,LEN,300,400)
C      WRITE(6,2050) (RADAR(L),L=1,4)
C      2050 FORMAT(2X,F8.2,4X,F9.2,2X,F9.4,2X,F9.4)
C      IREC = IREC + 1
C      50 CONTINUE
C      GO TO 999
C      300 WRITE(6,2300) IREC
C      2300 FORMAT(1X,'END OF FILE AFTER RECORD ',I6)
C      GO TO 999
C      400 WRITE(6,2400) IREC
C      2400 FORMAT(1X,'INPUT TAPE ERROR AFTER RECORD ',I6)
C      999 STOP
C      END
```

*** END OF MEMBER *** 39 RECORDS PROCESSED

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MEMBER=RADAR
OR
POOR QUALITY

26JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.RADAR.CNTL

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00000010
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00000100
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RADAR PROGRAM 9/ /78 REVSD: 6/13/80 02/14/83
EDITION: 1
LANGUAGE: FORTRAN
COMPUTER: IBM 360/75, 360/91 3081
OPERATING SYSTEM: G. S. F. C.
PROGRAMMER: EUGENE H. SHAFFER/SASC TENARI E. REED S. COOKE

PURPOSE:
A PROGRAM TO READ THE DIGITIZED RADAR DATA TAPE AND
TO RE-FORMAT THE DATA AND WRITE THE DATA TO A SCRATCH
TAPE TO BE USED LATER BY THE "MERGE" PROGRAM.

VARIABLES:
NAME

INTERNAL
C
IUNIT
IUNIT2
NF
NF2
NF1
R(13)
SI-S12
STIME
TAPEIN(6)
TAPOUT(6)
IDATE(3)
LMO
LDY
LYR
SITE(16)

TYPE I/O DESCRIPTION

R*4 I CONVERSION FACTOR
I*4 I INPUT TAPE UNIT NUMBER
I*4 I OUTPUT TAPE UNIT NUMBER
I*4 I INPUT TAPE FILE NUMBER
I*4 I OUTPUT TAPE FILE NUMBER
I*4 I NUMBER OF FILES ON INPUT TAPE
R*4 I PEDIGREE ARRAY/RADAR DATA ARRAY
R*4 I PARITY INDICATOR
R*4 I TIME CORRECTION
L*1 I INPUT TAPE NAME
L*1 I OUTPUT TAPE NAME
I*4 I/O DATE TAPE REC'D
I*4 I/O LAUNCH MONTH
I*4 I/O LAUNCH DAY
I*4 I/O LAUNCH YEAR
L*1 I/O LAUNCH SITE NAME

SUBROUTINES CALLED
MOUNT
FREAD
RPDAT0
FWRITE

LOGICAL*1 TAPOUT(6), MINUS*1-*, S1, S2, S3, S4, S5, S6, S7, S8, S9, S10,
* S11, S12, TAPEIN(6), DATE(10), OK*.TRUE./
LOGICAL*4 SITE(4)

READ IN INPUT AND OUTPUT TAPE INFO AND STARTING TIME INFO.
EQUIVALENCE (R(10), SITE(1))

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00000720
00000730
00000740
00000750

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DIMENSION R(13), IYMD(3), IDATE(3)
READ (5,1020) TAPEIN, IUNIT, NF, NFILE, STIME, IFLT, IDATE
WRITE (6,2020) TAPEIN, IUNIT, NF
READ (5,1000) TAPOUT, IUNIT2, NF2
WRITE (6,1030) TAPOUT, IUNIT2, NF2
CALL RPDATE(1, IYMD)
R(1) = -100
R(2) = IFLT
R(8) = IDATE(1)*10000 + IDATE(2)*100 + IDATE(3)
R(9) = IYMD(2)*1000 + IYMD(3)*100 + IYMD(1)
READ (5,1035) R(3), LMO, LDY, LYR, (R(K), K=5,7), SITE
R(4) = LMO*10000 + LDY*100 + LYR
WRITE (6,2065) (R(KZ), KZ=1,13)
WRITE (6,2035) NFILE, STIME
WRITE (6,2060)
WRITE (6,2045)
WRITE (6,2050)
CALL MOUNT (1, IUNIT, TAPEIN, NF)
CALL MOUNT (2, IUNIT2, TAPOUT, NF2)
CALL FWRITE(R, IUNIT2, LEN)
C REMIND INPUT UNIT TO AVOID A SECOND OPEN ATTEMPT ON SAME UNIT

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C (MOUNT ALREADY OPENED THE UNIT AND FORTRAN READ WILL TRY AGAIN.)
CALL REMIND (IUNIT)
C= .3048
I=1
LINES=8
SAME=0.
KNTREC = 0
KNTERR = 0

C READ IN RADAR INFO FROM INPUT TAPE.
C
C
100 CONTINUE
  READ(10,1010,END=110,ERR=115)R(1),R(2),S1,R(3),S2,R(4),S3,
  * R(5),S4,R(6),S5,R(7),S6,R(8),S7,R(9),S8,R(10),S9,R(11),
  * S10,R(12),S11,R(13),S12
  IF(OK) GO TO 102
  OK= TRUE.
  GO TO 100
102 R(1)=R(1)+STIME
  IF(R(1).EQ.SAME) GO TO 100

C CHECK PARITY
C
C
  IF(S1.EQ.MINUS)R(2)=-1*R(2)
  IF(S2.EQ.MINUS)R(3)=-1*R(3)
  IF(S3.EQ.MINUS)R(4)=-1*R(4)
  IF(S4.EQ.MINUS)R(5)=-1*R(5)
  IF(S5.EQ.MINUS)R(6)=-1*R(6)
  IF(S6.EQ.MINUS)R(7)=-1*R(7)
  IF(S7.EQ.MINUS)R(8)=-1*R(8)
  IF(S8.EQ.MINUS)R(9)=-1*R(9)
  IF(S9.EQ.MINUS)R(10)=-1*R(10)
  IF(S10.EQ.MINUS)R(11)=-1*R(11)
  IF(S11.EQ.MINUS)R(12)=-1*R(12)
  IF(S12.EQ.MINUS)R(13)=-1*R(13)
  R(2)=CHR(2)
  DO 105 J=1,8
    R(J+4)=CHR(J+4)
105 CONTINUE

C PRINT OUT THE REFORMATTED RADAR DATA AND WRITE IT ON THE OUTPUT
C TAPE.
C
C
  CALL FWRITE (R,IUNIT2,LEN)
  KNTREC=KNTREC+1
  LINES=LINES+1
  IF(LINES.LE.78) GO TO 108
  LINES=1
  WRITE(6,2055)
  WRITE(6,2045)
  WRITE(6,2050)
  108 WRITE (6,2010)R
    SAME=R(1)
    GO TO 100
  110 CONTINUE
    WRITE(6,2000)I
    IF(NFILE.EQ.I)GO TO 120

```

```

00000760
00000770
00000780
00000790
00000800
00000810
00000820
00000830
00000840
00000850
00000860
00000870
00000880
00000890
00000900
00000910
00000920
00000930
00000940
00000950
00000960
00000970
00000980
00000990
00001000
00001010
00001020
00001030
00001040
00001050
00001060
00001070
00001080
00001090
00001100
00001110
00001120
00001130
00001140
00001150
00001160
00001170
00001180
00001190
00001200
00001210
00001220
00001230
00001240
00001250
00001260
00001270
00001280
00001290
00001300
00001310
00001320

```

ORIGINAL PAGE
OF POOR QUALITY

```

NUFIL=MF+I
REWIND IUNIT
CALL POSN(1,IUNIT,NUFIL)
CALL REWIND (IUNIT)
I=I+1
GO TO 100
115 CONTINUE
KNTERR=KNTERR+1
WRITE(6,2040)
OK=.FALSE.
GO TO 100
120 CONTINUE
WRITE (6,2030) KNTREC,KNTERR
1000 FORMAT(1X,6A1,6X,12,3X,12)
1010 FORMAT(12X,F10.4,2X,F10.0,A1,1X,2(F10.4,A1,1X),
      * 3(F10.0,A1,1X),12X,F10.0,A1,1X,24X,
      * 4(F10.0,A1,1X),12X,F10.4,A1,1X)
1020 FORMAT (1X,6A1,6X,12,3X,12,3X,12,4X,F7.2,3X,13,3X,12,1X,12)
1030 FORMAT(1X,2X,'TAPEOUT: ',6A1,5X,'UNIT: ',13,5X,'FILE: ',13)
1035 FORMAT (1X,F4.0,2X,12,1X,12,1X,12,2X,F8.1,2X,F8.3,2X,4A4)
2000 FORMAT(10X,'RADAR 2000: END OF FILE NO. ',14)

```

00001330
00001340
00001350
00001360
00001370
00001380
00001390
00001400
00001410
00001420
00001430
00001440
00001450
00001460
00001470
00001480
00001490
00001500
00001510
00001520
00001530

MEMBER=RADAR

26JUL84 08.52.34 - VOL=SACC10, DSN=ZBSAC.RADAR.CNTL

2010 FORMAT (1X,F10.4,F10.1,2F10.4,8F10.1,F10.4)
2020 FORMAT ('1',2X,'TAPEIN:',6A1.5X,'UNIT:',13,5X,'FILE:',13)
2030 FORMAT ('/',1X,5X,'NUMBER OF RECORDS WRITTEN:',14,/,
1 1X,5X,'NUMBER OF ERROR RECORDS:',14,/,
2 1X,120(' '),/)
2035 FORMAT (1X,5X,'NUMBER OF FILES TO PROCESS:',13,/,
1 1X,5X,'TIME CORRECTION:',F9.2,///)
2040 FORMAT(10X,'RADAR 2040: TAPE RECORD ERROR, PROCESSING CONTINUING')
2045 FORMAT(1X,' SECONDS ',4X,' SLANT ',3X,'AZIMUTH ELEVATION',
1 6X,'HOR ',6X,'N-S ',6X,'E-W ',2X,'ALTITUDE',7X,'HOR ',7X,
2 'E-W ',7X,'N-S ',6X,'VERT ',3X,'HOR VEL ',)
2050 FORMAT(1X,' AFTER HOUR ',2X,'RANGE DEGREES DEGREES',5X,
1 'RANGE ',4X,'RANGE ',4X,'RANGE OBL.SPH.',7X,'VEL',7X,'VEL',
2 7X,'VEL',6X,'VEL ',3X,'AZIMUTH')
2055 FORMAT('1')
2060 FORMAT(40X,'DISTANCE IN METERS, VELOCITIES IN METERS/SECOND')
2065 FORMAT ('/',1X,11X,'FLT',5X,'VEN/LOC',5X,'FLT DATE',5X,'GMT TIME',
1 5X,'LAT',6X,'LONG',5X,'TAPE RCD',5X,'RUN DATE',5X,
2 'LAUNCH LOCATION',/,
3 1X,1X,F5.0,5X,F9.0,5X,F4.0,8X,F7.0,5X,F8.1,3X,F7.3,2X,F8.3,
4 4X,F7.0,6X,F7.0,5X,4A4,/,
STOP
END

*** END OF MEMBER *** 178 RECORDS PROCESSED

XX

ORIGINAL
OF POOR QUALITY

```

C
C SUBROUTINE BLOCK(ICODE)
C
C BLOCK READS THE OZONE TM TAPE AND CONVERTS ALL TIME WORDS
C *** IN THIS VERSION OF BLOCK, PROCESSING MAY BE STOPPED ***
C *** AFTER REACHING A SPECIFIC RECORD. ***
C
C EUGENE SHAFFER(SASC) 3/78 KRISHNA TEHARI 6/81
C E. REED/G.BATLUCK 10/82
C
C ICODE =0 NO PROBLEM
C 1 END OF FILE
C
C COMMON/LABEL1,IREC,DELTAT,MPEAK,LPEAK,LIMIT
C COMMON /LABEL3/DATA(1210),INPUT(1220)
C COMMON/LABEL5/OUTX(20)
C
C LOGICAL X1 IN1(2),OUT1(2)
C INTEGER*4 SHFTR,SHFTL,DATA
C INTEGER*2 INPUT,IN2,OUT2
C REAL*4 RATA(1210)
C EQUIVALENCE (IN1(1),IN2),(OUT1(1),OUT2),(RATA(1),DATA(1))
C DATA NREC/0/
C
C ICODE=0
C
C READ IN RAW SIGNAL DATA.
C
C DO 20 I=1,IREC
C NREC=NREC+1
C CALL FREAD(INPUT,10,LEN,8110,810)
C IF(NREC.GE.IREC) GO TO 30
C GO TO 20
C 10 WRITE(6,2010) NREC
C 20 CONTINUE
C 30 J=0
C
C THE FOLLOWING STATEMENT (NREC.GT.XXX) IS TO BE USED TO STOP
C PROCESSING CERTAIN FLIGHTS AFTER REACHING A SPECIFIC RECORD.
C IF (NREC.GT.136) GO TO 110
C CONVERT TO IBM FORMAT
C DO 80 NZ=11,1220
C J=J+1
C IN2=INPUT(NZ)
C OUT1(2)=IN1(1)
C OUT1(1)=IN1(2)
C INPUT(NZ)=OUT2
C 80 DATA(J)=INPUT(NZ)
C CONVERT TIME WORDS TO (9) DDDHH,(10) MMSS, (11) SECONDS (REAL)
C DO 90 J=9,1208,11
C MILLISECONDS
C LX=DATA(J)
C IF(LX.LT.0) LX=LX+65535
C JSEC=((SHFTR(SHFTL(LX,28),28))+(SHFTR(SHFTL(LX,20),28)*10)
C + (SHFTR(LX,12)*100))
C SEC=(FLOAT(JSEC))/1000.
C MINUTE AND SECOND

```



```

LX=DATA(J+1)
IF (LX.LT. 0) LX = LX + 65535
IMIN=((SHFTR(SHFTL(LX,17),29))%10)+(SHFTR(SHFTL(LX,20),28))
C THE FOLLOWING LINE (RE: NREC 1900 OR 1901) IS FOR FLT 295 ONLY.
C IF (NREC.EQ.1900 .OR. NREC.EQ.1901) IMIN = 8
ISEC=((SHFTR(SHFTL(LX,24),28))%10)+(SHFTR(SHFTL(LX,28),28))
DATA(J+1) = 100*IMIN+ISEC
C DAY AND HOUR
LX=DATA(J+2)
IF (LX.LT. 0) LX = LX + 65535
IDAY=((SHFTR(LX,14)%100)+(SHFTR(SHFTL(LX,18),28))%10)
+ (SHFTR(SHFTL(LX,22),28))
IHR=((SHFTR(SHFTL(LX,26),30)%10)+(SHFTR(SHFTL(LX,28),28))
DATA(J) = 100*IDAY+IHR
RATA(J+2) =SEC
90 CONTINUE
GO TO 999
110 ICODE=1
NREC=NREC-1
WRITE(6,2020)NREC
2010 FORMAT(1X,'BLOCK 2010: READ ERROR IN RECORD' ,I6)

```

```

00000550
00000560
00000570
00000580
00000590
00000600
00000610
00000620
00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700
00000710
00000720
00000730
00000740
00000750

```

ORIGINAL FILE
OF POOR QUALITY

26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.EDIT.CNTL

MEMBER=010CK1

2020 FORMAT(1X,'BLOCK 2020' END OF FILE AFTER RECORD',I6)
999 RETURN
END

00000760
00000770
00000780

*** END OF MEMBER ***

80 RECORDS PROCESSED

```

C EDIT OZONE PROGRAM
C A PROGRAM TO READ THE DIGITIZED OZONE TAPE FROM WALLOPS FLIGHT
C FACILITY. EDIT THE DATA AND REFORMAT THE DATA ON AN OUTPUT TAPE.
C
C EUGENE SHAFFER(SASC)      3/78      10 BIT DATA
C KRISHNA TEMWARI          6/81
C E. REED/BATLUCK          12/82
C S. COOKE                 02/83      ADDED CMPAVE & PEDIGREE
C                               11/83      CHANGED FREAD FOR READING ID
C                               04/20/83 AND INPU ARRAYS
C                               MODIFICATION TO CYCLE
C B. ALLEN
C
C VARIABLES:
C NAMES          TYPE  I/O  DESCRIPTION
C
C COMMON/LABEL1/
C DELTAT         R#4      I      AVERAGE TIME OF FILTER WHEEL CYCLE
C IREC           I#4      I      NUMBER OF FIRST RECORD TO BE PROCESSED
C MPEAK          I#4      I      HIGH MODE OF MARKER CHANNEL
C LPEAK          I#4      I      LOW MODE OF MARKER CHANNEL
C LIMIT          I#4      I      ACCEPTABLE RANGE OF MARKER CHANNEL
C
C COMMON/LABEL3/
C DATA          I#4      I      INPUT DATA
C INPUT          I#2      I      INPUT DATA
C
C COMMON/LABEL5/
C OUTX           R#4      0      OUTPUT ARRAY
C *****
C SUBPROGRAMS CALLED
C MOUNT, FREAD, FWRITE, CONVRT, CYCLE, SWITCH, BCD5, CMOVE, RPDAT0
C
C *****
C COMMON/LABEL1/IREC, DELTAT, MPEAK, LPEAK, LIMIT
C COMMON /LABEL3/ DATA(1210), INPUT(1220)
C COMMON /LABEL5/ OUTX(20)
C COMMON/CAL/B1, V1, B2, V2, T(3), VT(3)
C
C LOGICAL*1 TAPEIN(6), TAPOUT(6), ID(92), LD(40), IOIN(6), IOOUT(6)
C LOGICAL*1 INPU(92)
C INTEGER*2 INPUT, ID2(46), LD2(20), SWITCH
C INTEGER*4 DATA, TSTBUF(610)
C DIMENSION IYMD(3), IDATE(3)
C EQUIVALENCE(ID(1), ID2(1)), (LD(1), LD2(1)), (INPU(1), INPUT(1))
C
C NOUT=0
C OUTX(1) = 0.
C CALL CMOVE(OUTX(1), OUTX(2), 76)
C TMFR=0.01125
C
C READ IN AND WRITE OUT INPUT DATA.
C
C WRITE (6,2000)
C READ (5,1000) TAPEIN, IOIN, IUNIT1, NF1

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ORIGINAL
OF RECORD

00000490
00000500
00000510
00000520
00000530
00000540
00000550
00000570
00000580
00000590
00000600
00000610
00000620
00000630
00000640
00000642
00000650
00000652
00000660
00000670
00000680

READ (5,1000) TAPOUT,IOOUT,IUNIT2,NF2,LEN2
WRITE (6,2010) TAPEIN,IOIN,IUNIT1,NF1
WRITE (6,2010) TAPOUT,IOOUT,IUNIT2,NF2,LEN2
WRITE (6,2020)
READ (5,1010) DELTAT,IREC,MPEAK,LPEAK,LIMIT
IF(IREC.LT.1) IREC=1
WRITE (6,2030)DELTAT,IREC,MPEAK,LPEAK,LIMIT

C MOUNT INPUT AND OUTPUT TAPES.

CALL MOUNT (1,IUNIT1,TAPEIN,NF1)
CALL MOUNT (2,IUNIT2,TAPOUT,NF2)

READ IN HEADER RECORD AND DATA DESCRIPTION RECORD.

LEN = 0

CALL FREAD (TSTBUF(1),10,LEN,8900,8910)
CALL CMOVE(TSTBUF(1),ID(1),92)
N=SWITCH(ID2(2))
NT=SWITCH(ID2(6))
CALL BCD5(ID,INPU,92)

C C
C C
C C

```

WRITE(6,2012)N,NT,INPUT(4),INPUT(5),(INPUT(I),I=7,46)
50 CONTINUE
LEN = 0
CALL FREAD (TSTBUF(1),10,LEN,8900,8920)
CALL CHOVE(TSTBUF(1),LD(1),40)
NFR = SWITCH(LD2(9))
N=SWITCH(LD2(16))
WRITE(6,2014)NFR,N
CALL CONVRT(I,I,I,I,I,I)
C COMPUTE AND PRINT PEDIGREE.
OUTX(1)=-200.
CALL RPDAT0(1,IYMD)
OUTX(5)=IYMD(2)*10000 + IYMD(3)*100 + IYMD(1)
OUTX(6)=B1
OUTX(7)=V1
OUTX(8)=B2
OUTX(9)=V2
OUTX(10)=T(1)
OUTX(11)=VT(1)
OUTX(12)=T(2)
OUTX(13)=VT(2)
OUTX(14)=T(3)
OUTX(15)=VT(3)
READ (5,1020)OUTX(2),OUTX(3),IDATE
OUTX(4)=IDATE(1)*10000 + IDATE(2)*100 + IDATE(3)
DO 20 I=16,20
OUTX(I)=0.0
20 CONTINUE
WRITE (6,2070)
WRITE (6,2080)(OUTX(KL),KL=1,15)
CALL FWRITE(OUTX,IUNIT2,LEN2)
WRITE(6,2050)
LINE=1
C READ IN RAW SIGNAL DATA.
C
C 200 CALL CYCLE(WCODE,NERR)
IF(NCODE.NE.0) GO TO 990
C WRITE THE OUTPUT ARRAY AND WRITE OUT DATA ON TAPE AND PRINTER.
C
CALL FWRITE(OUTX,15,LEN2)
NOUT=NOUT+1
IXPECT=OUTX(15)/TMFR
IF(MOD(LINE,70).EQ.0) WRITE(6,2050)
WRITE(6,2060)OUTX,IXPECT
LINE=LINE+1
GO TO 200
C END OF FILE
900 WRITE(6,2900)
GO TO 990
C ERROR IN HEADER RECORD
910 WRITE(6,2910)
GO TO 50
-C ERROR IN DATA DESCRIPTION RECORD
920 WRITE(6,2920)
GO TO 200

```

ORIGINAL
OF POOR QUALITY

```

C PROGRAM TERMINATION
990 WRITE(6,2990)NOUT,NERR
STOP
1000 FORMAT (6A1,2X,6A1,2X,12,2X,12,2X,12,2X,13)
1010 FORMAT (F6.3,4(2X,13))
1020 FORMAT (F5.1,2X,F4.0,1X,3(1X,12))
2000 FORMAT (1X,120('X'),//,33X,'PROGRAM:  EDIT -- REVISED  ',INFO:',
1 'FEBRUARY 22, 1983',//,1X,120('X'),//,1X,29X,'TAPE',INFO:',
2 'NAME I/O UNIT FILE# RECORD LEN.',//)
2010 FORMAT (1X,43X,6A1,3X,6A1,4X,12,7X,12,11X,13)
2012 FORMAT('0',:HDR1:',16,'WORDS. TAPE NUMBER',14,
1 'STREAM',1X,2A2,2X,40A2)
2014 FORMAT('0',:HDR2:',16,'FRAMES PER RECORD',18,
X 'WORDS PER RECORD')
2020 FORMAT(/,1X,120('X'),//,1X,29X,'INPUT DATA:  DELTAT ',
1 'RECORD HPEAK LPEAK RANGE',//)
2030 FORMAT (1X,44X,F6.3,6X,13,8X,13,7X,13,7X,13)
2040 FORMAT(/,1X,120('X'),//)
2050 FORMAT('1',:T1(SEC) T2(SEC) T3(SEC) T4(SEC) T5(SEC) AVG1',
1 'AVG2 AVG4 AVG5 MRKR BASE CMP1 CMP2 CMP4 CMP5 DELPK',
2 'DELAY CHAV BATV TR C SM EX',//)

```

```

00001010
00001020
00001030
00001040
00001050
00001055
00001060
00001070
00001080
00001080
00001090
00001100
00001110
00001120
00001125
00001130
00001140
00001150
00001160
00001170
00001180
00001190

```

ORIGINAL
OF POOR QUALITY

ORIGINAL FILE
OF POOR QUALITY

```

00001200
00001210
00001212
00001214
00001216
00001218
00001220
00001222
00001224
00001226
00001228
00001230
00001240
00001244
00001250
00001252
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00001280
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00001430
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00001450
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00001470
00001480
00001490
00001500
00001510
00001520
00001522
00001524
00001530
00001540
00001550
00001560

2060 FORMAT(1X,4F10.3,4F6.1,6F5.0,2F6.3,1F5.0,F5.2,F5.1,F4.0,I3)
2070 FORMAT(//,1X,55X,'BATTERY CALIBRATION',21X,
1 'TEMPERATURE CALIBRATION',//,
2 1X,7X,'FLT/LG',2X,'PAYLOAD',3X,'TAPE RCD',3X,'RUN DATE',4X,
3 2C'VOLTS',3X,'TM CT',3X),2('DEG C',2X,'TM VOLTS',2X),'DEG C',
4 2X,'TM VOLTS',//,
5 1X,47X,'(UPPER)',9X,'(LOWER)',29X,'(UPPER)',/,
2080 FORMAT(1X,1X,F5.0,2X,F5.1,4X,F4.0,2(4X,F7.0),5X,
1 2(F5.1,2X,F6.2,3X),2(F5.1,4X,F6.2,3X),F5.1,4X,F6.2,//)
2900 FORMAT(1X,'MAIN 2900: EOF FOR HEADER OR DATA DESC RECORD')
2910 FORMAT(1X,'MAIN 2910: ERROR IN READING DATA RECORD')
2920 FORMAT(1X,'MAIN 2920: ERROR IN READING DATA DESCRIPTION RECORD')
2990 FORMAT(1X,'MAIN 2990:',I8,' RECORDS WRITTEN.',I8,
X ' AVERAGES SET TO -99.',//,11X,' PROGRAM END')
END
C *****
C FUNCTION SWITCH(X)
C REED/BATLUCK NOV. 1982
C SWITCH INTERCHANGES THE BYTES OF THE I*2 WORDS TO MAKE THEM
C COMPATIBLE WITH IBM STRUCTURE.
C INTEGER*2 X,T,SWITCH,Z
C LOGICAL*1 A(2),B(2)
C EQUIVALENCE(Z,A(1)),(T,B(1))
C Z=X
C B(1) = A(2)
C B(2) = A(1)
C SWITCH = T
C RETURN
C END
C *****
C SUBROUTINE CONVRT(BATTV,TEMPC,AVG6,HAVG7,MODE)
C
C CONVERT READS IN CALIBRATION DATA FOR BATTERY VOLTAGE AND PAYLOAD
C TEMPERATURE, AND APPLIES IT TO AVERAGE VALUES OF WORD 6 AND MARKER.
C
C OCT. 22, 1982 EDITH REED G. BATLUCK
C
C ARGUMENTS
C BATTV VOLTAGE FROM PAYLOAD BATTERY, NOMINAL 6V
C TEMPC PAYLOAD TEMPERATURE, DEGREES CELSIUS
C AVG6 AVERAGE VALUE OF WORD 6 DURING ONE FILTER CYCLE
C VOLT7
C HAVG7 AVERAGE VALUE OF MARKER PULSE (WORD 7)
C MODE=1 READ IN CALIBRATION DATA
C =2 CALCULATE BATTV AND TEMPC
C
C DIMENSION TMPICAL(71),ADJ(3),TMP(3)
C COMMON/CAL/B1,V1,B2,V2,T(3),VT(3)
C
C DATA TMPICAL/9.961,9.857,9.748,9.636,9.519,9.399,9.280,9.156,
1 9.029,8.898,8.764,8.633,8.497,8.358,8.216,8.071,7.931,7.787,
2 7.640,7.491,7.341,7.192,7.042,6.892,6.742,6.594,6.445,6.296,
3 6.147,6.000,5.853,5.709,5.564,5.422,5.281,5.143,5.005,4.870,

```

ORIGINAL FILED
OF POOR QUALITY

00001570
00001580
00001590
00001600
00001605
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001740
00001750
00001760

4 4.736,4.603,4.476,4.361,4.226,4.104,3.984,3.867,3.753,3.642,
5 3.532,3.426,3.321,3.220,3.121,3.025,2.930,2.838,2.750,2.656,
6 2.580,2.499,2.419,2.343,2.269,2.197,2.126,2.059,1.992,1.929,
7 1.866,1.807,1.747/

```
C      IF(MODE.EQ.2) GO TO 200
C      READ IN CALIBRATION VALUES          BATTV = C1 +C2*WORD 6
      READ(5,1000) B1,V1,B2,V2
      C2=(B1-B2)/(V1-V2)
      C1=B1-C2*V1
      WRITE(6,2000)C1,C2
C      READ IN TEMPERATURE CALIBRATION VALUES
      READ(5,1010)(T(I),VT(I),I=1,3)
C      CALCULATE ADJUSTMENT FACTORS
      DO 40 I=1,3
      IT=T(I)+21.05
      DO 20 J=1,71
      JT=J
      IF(JT.GE.IT) GO TO 30
20 CONTINUE
30 ADJ(I)=VT(I)/TMPCAL(JT)
```


ORIGINAL FILE
OF POOR QUALITY

```

40 CONTINUE
C  ADJUST TEMPERATURE CALIBRATION CURVE AND CONVERT TO COUNTS
  DO 80 I=1,2
    IA=T(I)+20.05+I
    IB=T(I+1)+21.05
    C=((ADJ(I+1)-ADJ(I))/(T(I+1)-T(I)))
    DO 60 J=IA,IB
      60  TMPCAL(J)=TMPCAL(J)*((J-IA)*C+ADJ(I))
    80 CONTINUE
    DO 100 I=1,3
      J=T(I)+21.05
      100  TMP(I)=TMPCAL(J)
    WRITE(6,2010)(T(I),VT(I),ADJ(I),I=1,3)
    GO TO 999
C  CONVERT WORDS
200 CONTINUE
  BATTV = C1+C2*AVG6
  IF(HAVG7.LE.0.) GO TO 999
  VOLT7=HAVG7/100.0
  DO 240 I=2,71
    IF(VOLT7.LT.TMPCAL(I)) GO TO 240
    TA=TMPCAL(I-1)
    TD=TMPCAL(I)-TA
    TMPA=I-21
    TEMPC=(VOLT7-TA)/TD+TMPA
    GO TO 999
240 CONTINUE
  TEMPC = 50.+5.*(TMPCAL(71)-VOLT7)/(TMPCAL(66)-TMPCAL(71))
  WRITE(6,2020) BATTV,TEMPC,AVG6,HAVG7
999 RETURN
1000 FORMAT(2(F5.1,F8.2))
1010 FORMAT(3(F5.1,F8.2))
2000 FORMAT('0','BATTERY VOLTAGE = ',F5.1,' +',F6.3,' WORD-6 COUNTS')
2010 FORMAT('0','TEMPERATURE C VOLTS ADJUSTMENT TO SER NO 400 CURVE',
1  ' TMPCAL',/3(1X,F11.1,F9.3,F7.3/))
2020 FORMAT(1X,'CONVERT 2020: ',4F10.2)
END
C *****
C  SUBROUTINE BLOCK(ICODE)
C  BLOCK READS THE OZONE TM TAPE AND CONVERTS ALL TIME WORDS
C  EUGENE SHAFFER(SASC)      3/78      KRISHNA TEWARI      6/81
C  E. REED/G.BATLUCK        10/82
C  ICODE =0 NO PROBLEM
C  1 END OF FILE
C  COMMON/LABEL1/IREC,DELTAT,MPEAK,LPEAK,LIMIT
C  COMMON /LABEL3/DATA(1210),INPUT(1220)
C  COMMON/LABEL5/OUTX(20)
C  LOGICAL*1 IN1(2),OUT1(2)
C  INTEGER*4 SHFTR,SHFTL,DATA
C  INTEGER*2 INPUT,IN2,OUT2
C  REAL*4 RATA(1210)

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EQUIVALENCE (IN1(1),IN2),(OUT1(1),OUT2),(DATA(1),DATA(1))
DATA NREC/0/
C
C      ICODE=0
C      READ IN RAW SIGNAL DATA.
C
      DO 20 I=1,IREC
      NREC=NREC+1
      LEN = 0
      CALL FREAD(INPUT(1),10,LEN,8110,810)
      IF(NREC.GE.IREC) GO TO 30
      GO TO 20
      10 WRITE(6,2010) NREC
      20 CONTINUE
      30 J=0
C THE FOLLOWING STATEMENT (NREC.GT.XXX) IS TO BE USED TO STOP
C PROCESSING CERTAIN FLIGHTS AFTER REACHING A SPECIFIC RECORD.
C IF (NREC.GT.95) GO TO 110
C CONVERT TO IBM FORMAT
      DO 80 NZ=11,1220

```

```

      J=J+1
      IN2=INPUT(NZ)
      OUT1(2)=INI(1)
      OUT1(1)=INI(2)
      INPUT(NZ)=OUT2
      80 DATA(J)=INPUT(NZ)
      C CONVERT TIME WORDS TO (9) DDHMM,(10) MMSS, (11) SECONDS (REAL)
      DO 90 J=9,1208,11
      C MILLISECONDS
      LX=DATA(J)
      IF(LX.LT.0) LX=LX+65535
      JSEC=((SHFTR(SHFTL(LX,28),28))+(SHFTR(SHFTL(LX,20),28)*10)
      + (SHFTR(LX,12)*100))
      SEC=(FLOAT(JSEC))/1000.
      C MINUTE AND SECOND
      LX=DATA(J+1)
      IF(LX.LT.0) LX=LX + 65535
      IMIN=((SHFTR(SHFTL(LX,17),29))*10)+(SHFTR(SHFTL(LX,20),28))
      C THE FOLLOWING LINE (RE: NREC 1900 OR 1901) IS FOR FLT 295 ONLY.
      C IF (NREC.EQ.1900 .OR. NREC.EQ.1901) IMIN = 8
      ISEC=((SHFTR(SHFTL(LX,24),28))*10)+(SHFTR(SHFTL(LX,28),28))
      DATA(J+1) = 100*IMIN+ISEC
      C DAY AND HOUR
      LX=DATA(J+2)
      IF(LX.LT.0) LX=LX + 65535
      IDAY=((SHFTR(SHFTL(LX,14)*100)+(SHFTR(SHFTL(LX,18),28))*10)
      + (SHFTR(SHFTL(LX,22),28))
      IHR=((SHFTR(SHFTL(LX,26),30)*10)+(SHFTR(SHFTL(LX,28),28))
      DATA(J) = 100*IDAY+IHR
      RATA(J+2) =SEC
      90 CONTINUE
      GO TO 999
      110 ICODE=1
      NREC=NREC-1
      WRITE(6,2020)NREC
      2010 FORMAT(1X,'BLOCK 2010: READ ERROR IN RECORD',I6)
      2020 FORMAT(1X,'BLOCK 2020: END OF FILE AFTER RECORD',I6)
      999 RETURN
      END
      C *****
      C SUBROUTINE CYCLE(NCODE,NERR)
      C
      C CYCLE FILLS THE ARRAY 'KEEP' WITH DATA READ BY BLOCK, AND WHICH
      C HAS ACCEPTABLE VALUES FOR WORD7 (MARKER/REFERENCE). TIME SPAN
      C FOR EACH OF THE 4 FILTERS IS DETERMINED AND AVERAGE VALUES
      C OBTAINED.
      C
      C E. REED/G. BATLUCK OCTOBER 1982
      C S. COOKE 2/14/83
      C
      C ARGUMENTS:
      C NCODE =0 NO PROBLEM
      C NCODE =1 END OF FILE ON INPUT TAPE
      C NERR = -1 PROBLEMS IN OBTAINING AVERAGES
      C NERR = NUMBER OF AVERAGES SET TO -99.
      C OUTX IS WRITTEN ON THE EDIT OZONE TAPE. CONTENTS OF RECORD IS (R*4)

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C WORD 1 S0 (WORD 1) SEC SINCE START HOUR 11 S0 (1) VALUE OF COMP WORD 00002930
C 2 S1 2 SEC SINCE START HOUR 12 S1 (2) VALUE OF COMP WORD 00002940
C 3 S2 4 SEC SINCE START HOUR 13 S2 (4) VALUE OF COMP WORD 00002950
C 4 S3 5 SEC SINCE START HOUR 14 S3 (5) VALUE OF COMP WORD 00002960
C 5 S0 1 AVERAGE VALUE COUNTS 15 LENGTH OF CYCLE (SECONDS) 00002970
C 6 S1 2 AVERAGE VALUE COUNTS 16 LENGTH OF CYCLE 10 C AVERAGE 00002980
C 7 S2 4 AVERAGE VALUE COUNTS 17 AVE VAL OF COMPMORD 00002990
C 8 S3 5 AVERAGE VALUE COUNTS 18 BASE 10 C AVERAGE 00003000
C 9 MARKER PULSE AVERAGE VALUE COUNT 19 BATTERY VOLTAGE (VOLTS) 00003010
C 10 BASE LEVEL AVERAGE VALUE COUNTS 20 TEMPERATURE DEG CELSIUS 00003020
C 00003030
C 00003040
C 00003050
C 00003060
C 00003070
C 00003080
C 00003090
C 00003100
C 00003110
C 00003120
C 00003130

IS INDEX FOR DATA ARRAY
KS INDEX OF LAST VALID DATA IN KEEP ARRAY

C KEEP:
C 1 - WORD 1 S0 5 - WORD 5 S3
C 2 - WORD 2 S1 6 - WORD 7 MARKER/BASE
C 3 - WORD 3 COMP 7 - WORD 8 UNCOMP
C 4 - WORD 4 S2 8 TIME - ELAPSED SEC.
C INTEGER #2 INPUT
C INTEGER #4 DATA,KEEP(8,200)

```

```

C      DIMENSION TIME(8,200),RATA(11,110),COMP(4)
COMMON/LABEL1/IREC,DELTA,T,MPEAK,LPEAK,LIMIT
COMMON/LABEL3/DATA(11,110),INPUT(1220)
COMMON/LABEL5/OUTX(20)

C      EQUIVALENCE (DATA(1,1),RATA(1,1)),(KEEP(1,1),TIME(1,1)),
X(COMP(1),OUTX(11))
DATA IFLAG/1,IS/0,KS/0,PASTIM/0.,NSIX/0/

C      IF(IFLAG.NE.-1) GO TO 10
MPHI = MPEAK +LIMIT
MPLO = MPEAK -LIMIT
LPHI = LPEAK +LIMIT
LPLO = LPEAK -LIMIT
CYEN=DELTA
MERR=0
INIT = 0
LASTDM = 0
LASTMS = 0
IFLAG = 1

C      C FILL KEEP/TIME WITH VALUES
10 IF(IS.NE.0) GO TO 40
20 IF (MCODE.EQ.1) GO TO 990
CALL BLOCK(MCODE)
IF(MCODE.EQ.1) GO TO 900
IF(NSIX.NE.0) SAVE6=FLOAT(KSIX)/NSIX
NSIX=0
IS = 0
KSIX=0

C      SELECT FRAMES
40 IS = IS +1
IF(IS.GT.110) GO TO 20
IDM = DATA(9,IS)
IMS = DATA(10,IS)
IF (IMS.LT. LASTMS .AND. IDM.EQ. LASTDM) GO TO 40
LASTDM = IDM
LASTMS = IMS
I=DATA(7,IS)
IF((I.GE.LPLO.AND.I.LE.LPHI).OR.(I.GE.MPLO.AND.I.LE.MPHI))GO TO 60
GO TO 40

60 KS=KS+1
C      MOVE INTO KEEP
DO 65 J=1,5
KEEP(J,KS)=DATA(J,IS)
KEEP(6,KS) = I
KEEP(7,KS)=DATA(8,IS)
SEC = (60*(DATA(10,IS)/100)+MOD(DATA(10,IS),100))+RATA(11,IS)
IF((SEC+3300.)LT.PASTIM)SEC=SEC+3600.
TIME(8,KS)=SEC
PASTIM=SEC
C      DATA FOR BATTERY VOLTAGE
J=DATA(6,IS)
WRITE(6,2946) KS,IS,I,(KEEP(JZ,KS),JZ=1,7),SEC,J,NSIX,KSIX
IF(J.LE.0.OR.J.GE.1023) GO TO 70
NSIX=NSIX+1

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```
KSIX=KSIX+J
70 IF(KS.LT.200) GO TO 40
   KLIM=200
C FIND BEGIN AND END OF CYCLE(ONE FILTER WHEEL ROTATION)
C FIND BASE
100 J=0
   K=100
   IF(K.GT.KLIM) K=KLIM
   DO 110 I=1,K
   IA=KEEP(6,I)
   IF(KEEP(6,I).GT.LPHI) GO TO 110
   J=I
C   WRITE(6,2947) J,IA,K
   GO TO 115
110 CONTINUE
   IF(J.EQ.0) GO TO 910
C FIND START OF MARKER PULSE
115 IM=0
   DO 120 I=J,KLIM
   IZ=KEEP(6,I)
   IF(KEEP(6,I).LT.MPLO) GO TO 120
```

26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.EDIT.CNTL

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IM=I
TM=TIME(8,I)
WRITE(6,2948) I,IZ,J,KLIM,IZ,IM,TM
GO TO 125
120 CONTINUE
GO TO 920
C FIND END OF MARKER PULSE
125 NM=0
DO 130 I=IM,KLIM
IC=KEEP(6,I)
IF(KEEP(6,I).GT.LPHI) GO TO 130
IB=I
TB=TIME(8,I)
NM=I-1
WRITE(6,2949)I,IC,IM,TB
GO TO 135
130 CONTINUE
IF(NM.EQ.0) GO TO 930
C FIND END OF CYCLE
135 NB=0
DO 140 I=IB,KLIM
ID=KEEP(6,I)
IF(KEEP(6,I).LT.MPLO) GO TO 140
IM2=I
TM2=TIME(8,I)
NB=I-1
WRITE(6,2951)I,ID,IM2
GO TO 150
140 CONTINUE
IF(NB.EQ.0) GO TO 910
IF((NB-IB).LT.3) GO TO 945
150 CTIME=TM2-TM
NSAMP = IM2-IM+1
WRITE(6,2941) CTIME,CTEN,MPEAK,LPEAK,LIMIT,MPL0,LPHI
IF(CTIME.LT.(0.7*CTEN).OR.CTIME.GT.(1.3*CTEN)) GO TO 940
C COMPUTE AVERAGE VALUES
C MARKER PULSE
CALL AVG(KEEP,6,IM,NM,SAVEM)
IF(SAVEM.LT.0.) NERR=NERR+1
C BASE
CALL AVG(KEEP,6,IB,NB,SAVED)
IF(SAVED.LT.0.) NERR=NERR+1
C S0 (WORD 1)
CALL AVG(KEEP,1,IM,NB,SAVEZ)
IF(SAVEZ.LT.0.) NERR=NERR+1
C S1 (WORD 2)
T=TIME(8,IB)+0.94*CTIME
DO 210 I=IM2,KLIM
IF(TIME(8,I).LT.T) GO TO 210
IN1=I
GO TO 215
210 CONTINUE
IN1=KLIM
215 CALL AVG(KEEP,2,IB,IN1,SAVE1)
IF(SAVE1.LT.0.) NERR=NERR+1
C WRITE(6,2952) SAVEM,SAVED,SAVEZ,SAVE1,T,IN1
C S2 (WORD 4)

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BSTIME=TIME(8,IM2)-TIME(8,IB)
T=TIME(8,IB)+0.333*BSTIME
DO 220 I=IB,NB
IF(TIME(8,I).LT.T) GO TO 220
I2=I
I2=TIME(8,I2)
WRITE(6,2953) IB,I2,T,T2,TIME(8,I)
GO TO 222
220 CONTINUE
222 T=T2 + .88*CTIME
DO 224 I=IM2,KLIM
IF(TIME(8,I).LT.T) GO TO 224
IN2=I-1
WRITE(6,2954) IM2,IN2,TIME(8,IN2)
GO TO 226
224 CONTINUE
IN2=KLIM
226 CALL AVG(KEEP,4,I2,IN2,SAVE2)
IF(SAVE2.LT.0.) NERR=NERR+1
C S3 (WORD 5)
T=TIME(8,IB)+0.667*BSTIME

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DO 230 I=12,NB
IF(TIME(8,I).LT.T) GO TO 230
I3=I
T3=TIME(8,I)
WRITE(6,2955) SAVE2,T,I3,I3
GO TO 232
230 CONTINUE
232 T=T3+0.82*CTIME
DO 234 I=1M2,KLIM
IF(TIME(8,I).LT.T) GO TO 234
I3=I-1
GO TO 236
234 CONTINUE
WRITE(6,2970) I,IM2,KLIM,TIME(8,I),T,I3
FORMAT (1X,'CYCLE 2970: ',3I5,2F12.4,I5)
I3 = KLIM
236 CALL AVG(KEEP,5,I3,I3,SAVE3)
WRITE(6,2980) SAVE3
FORMAT (1X,'CYCLE 2980: ',F10.4)
IF(SAVE3.LT.0.) NERR=NERR+1
IF(NERR.GT.300) GO TO 950
C OBTAIN TEMPERATURE AND BATTERY VOLTAGE
C WRITE(6,2956) I3,SAVE3,SAVE6
CALL CONVRT(OUTX(18),OUTX(19),SAVE6,SAVEM,2)
C UPDATE 10-CYCLE AVERAGES FOR CYCLE LENGTH,MARKER VALUE, AND BASE
IF (INIT.EQ.1 .AND. (TM-PASTM).GT.25.) INIT = 0
CALL TENAVE(CTIME,CTEN,SAVEM,TENN,SAVE6,TENB,INIT)
INIT = 1
PASTM = TM
WRITE(6,2957) TENM,TENB
MPHI=TENN+LIMIT
MPLO=TENN-LIMIT
LPHI=TENB+LIMIT
LPLO=TENB-LIMIT
C FIND CORRESPONDING VALUE OF COMP CHANNEL FOR EACH
CALL COMPHD(KEEP,IM,IB,I2,I3,NB,COMP,CMPAVE)
C WRITE(6,2958) COMP,KLIM
C MOVE UP DATA IN KEEP/TIME
KLIM=200-IM2+2
J=4*(KLIM)*8
C WRITE(6,2944) (KEEP(KM,1),KM=1,8)
CALL CHOVE(KEEP(1,IM2-1),KEEP(1,1),J)
C WRITE(6,2945)(KEEP(KV,1),KV=1,8)
C WRITE(6,2945)(KEEP(KV,KLIM),KV=1,8),KLIM
KS=KLIM
C FILL OUTX
OUTX(1)=TM
OUTX(2)=TB
OUTX(3)=T2
OUTX(4)=T3
OUTX(5)=SAVEZ
OUTX(6)=SAVE1
OUTX(7)=SAVE2
OUTX(8)=SAVE3
OUTX(9)=SAVEM
OUTX(10)=SAVEB
OUTX(15)=CTIME

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00005200
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00005270
00005280
00005290

```
OUTX(16)=CTEN
OUTX(17)=CMPAVE
OUTX(20)=NSAMP
C  WRITE(6,2943) (OUTX(KP),KP=1,10),(OUTX(KZ),KZ=15,18)
GO TO 999
C ODDS AND ENDS
C END OF FILE FROM BLOCK-MOVE UP AND PROCESS DATA STILL IN KEEP/TIME
900 KLIM=201-NB
J=KLIM*32
CALL CHOVE(KEEP(1,NB),KEEP(1,1),J)
GO TO 100
C 100 CONSECUTIVE BASE VALUES - MOVE UP AND REFILL KEEP/TIME
910 IF(K.LT.100) GO TO 990
CALL CHOVE(KEEP(1,100),KEEP(1,1),3232)
KS=101
GO TO 40
C NO MARKER PULSE - MOVE UP AND REFILL KEEP/TIME
920 IF (KLIM.NE. 200) GO TO 990
CALL CHOVE(KEEP(1,200),KEEP(1,1),32)
KS=1
GO TO 40
```

```

C NO BASE AFTER MARKER PULSE
930 IF (KLIM.NE. 200) GO TO 990
    KLIM=200-IM
    IF (KLIM.GE.150) GO TO 933
    IF (KLIM.LE. 0) KLIM = 1
    K=32*KLIM
    J=IM
    CALL CMOVE(KEEP(1,J),KEEP(1,1),K)
    KS=KLIM
    GO TO 40
933 KS=0
    GO TO 40
C CYCLE LENGTH TOO SHORT OR TOO LONG OR TOO FEW SAMPLES AT BASE VALUE
940 WRITE(6,2940) CTIME,NSAMP,IM,NM,IB,NB,IM2,TM,TB,IM2
945 IF (NB.LE.2) NB = 3
    KLIM=200-NB
    K=32*KLIM
    J=NB-1
    CALL CMOVE(KEEP(1,J),KEEP(1,1),K)
    KS=KLIM
    GO TO 40
C TOO MANY PROBLEMS IN FINDING AN AVERAGE
950 WRITE(6,2950)
    NCODE=-1
    GO TO 999
C NO MORE DATA(NCODE=1)
990 WRITE(6,2990)
    NCODE = 1
2950 FORMAT(1X,'CYCLE 2950: STOP BECAUSE OF PROBLEMS IN AVERAGING')
2940 FORMAT(1X,'CYCLE 2940: CYCLE REJECTED. LENGTH WAS', F10.4,
    X 17,' SAMPLES', F10.4)
2990 FORMAT(1X,'CYCLE 2990: LESS THAN 100 SAMPLES REMAIN')
2941 FORMAT(1X,'CYCLE 2941: ', F10.4, F10.4)
2943 FORMAT(1X,'CYCLE 2943: ', F10.4, F10.4)
2946 FORMAT(1X,'CYCLE 2946: ', F10.4, F10.4, F10.4, F10.4)
2947 FORMAT(1X,'CYCLE 2947: ', F10.4, F10.4)
2948 FORMAT(1X,'CYCLE 2948: ', F10.4, F10.4, F10.4)
2949 FORMAT(1X,'CYCLE 2949: ', F10.4, F10.4, F10.4)
2951 FORMAT(1X,'CYCLE 2951: ', F10.4, F10.4, F10.4)
2952 FORMAT(1X,'CYCLE 2952: ', F10.4, F10.4, F10.4)
2953 FORMAT(1X,'CYCLE 2953: ', F10.4, F10.4, F10.4)
2954 FORMAT(1X,'CYCLE 2954: ', F10.4, F10.4, F10.4)
2955 FORMAT(1X,'CYCLE 2955: ', F10.4, F10.4, F10.4)
2956 FORMAT(1X,'CYCLE 2956: ', F10.4, F10.4, F10.4)
2957 FORMAT(1X,'CYCLE 2957: ', F10.4, F10.4, F10.4)
2958 FORMAT(1X,'CYCLE 2958: ', F10.4, F10.4, F10.4)
2944 FORMAT(1X,'BEFORE CMOVE ', F10.4, F10.4)
2945 FORMAT(1X,'AFTER CMOVE ', F10.4, F10.4, F10.4)
999 RETURN
END
C *****
C SUBROUTINE AVG(KEEP,N,IS,IN,SAVE)
C
C DATA IN KEEP, BETWEEN FRAMES IS AND IN. THE RESULT IS PLACED IN SAVE.
C
C REED/BATLUCK DECEMBER 1982

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C  ARGUMENTS:  KEEP  2-D ARRAY OF DATA
C              N    FIRST INDEX OF ARRAY
C              IS,IN START AND END VALUES OF SECOND INDEX
C              SAVE  AVERAGE VALUE
C              DIMENSION KEEP(8,200)
C              EQUIVALENCE(TIME,ITIM)
C              NPTS=IN-IS+1
C              IF(NPTS.GT.1) GO TO 20
C              SAVE=KEEP(N,IS)
C              GO TO 999
20  IF(NPTS.GT.2) GO TO 30
C              IF(ABS(KEEP(N,IS)-KEEP(N,IN)).GT.6) GO TO 300
C              SAVE = (KEEP(N,IS)+KEEP(N,IN)) *0.5
C              GO TO 999
30  MIN = 1 + NPTS/2
C              DO 200 IT=IS,IN
C              ITES=KEEP(N,IT)
C              ISUM=0
C              M=0

```

DEFENSES: PAGE 19
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```
C COMP FINDS THE VALUE OF THE COMPENSATION CHANNEL CORRESPONDING
C TO THE TIME OF EACH FILTER. IT CHOOSES THE FRAME NEAR THE STATED
C FRAME WITH THE MAXIMUM VALUE IN THE UNCOMP CHANNEL, AND USES THE
C CORRESPONDING VALUE FROM THE COMP CHANNEL. CMPAVE IS THE AVERAGE
C VALUE DURING THE CYCLE.
C REED/BATLUCK OCTOBER 1982
C S.COOKE 2/14/83 ADDED CMPAVE
C KEEP ARRAY OF DATA
C IM,IB,I2,I3 START POSITION FOR EACH OF THE FILTERS
C COMP ARRAY OF COMP CHANNEL VALUES CORRESPONDING TO EACH.
C
C DIMENSION KEEP(8,200),COMP(4),LMX(4)
C LMX(1)=IM
C LMX(2)=IB
C LMX(3)=I2
C LMX(4)=I3
C DO 100 L=1,4
C MAX=LMX(L)
```

26JUL84 08.52.34 - VOL=SACC09, DSN=Z8SAC.EDIT.CNTL

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```
J=MAX-2
IF(J.LT.1) J=1
K=MAX+2
NTEST=KEEP(7,MAX)
DO 50 I=J,K
  IF( KEEP(7,I).LT.NTEST) GO TO 50
  NTEST=KEEP(7,I)
MAX=I
50 CONTINUE
100 COMP(L)=KEEP(3,MAX)
N=0
ISUM=0
DO 200 I=IM,NB
  NTEST=KEEP(3,I)
  IF (NTEST .LE. 0) GO TO 200
  ISUM=ISUM+NTEST
  N=N+1
200 CONTINUE
IF (N .NE. 0) GO TO 220
CMPAVE=0.
GO TO 999
220 CMPAVE=FLOAT(ISUM)/N
999 RETURN
END
```

00007020
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00007090
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00007120
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*** END OF MEMBER *** 803 RECORDS PROCESSED

ORIGINAL FILE
OF POOR QUALITY

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*****
MERGE OZONE          6/10/80
EDITION: 1
LANGUAGE:  FORTRAN
COMPUTER:  IBM 360/75, 360/91
OPERATING SYSTEM: G. S. F. C.
PROGRAMMER:  EUGENE H. SHAFFER/SASC
LOW. DEG. E; 4 WORD RADAR RECORD; DD=DH      S. COOKE  11/83
*****

PURPOSE:
A PROGRAM TO MERGE THE DIGITIZED RADAR DATA AND THE
EDITED OZONE DATA. ALSO TO COMPUTE THE ZENITH ANGLE.

REED/BATLUCK 12-82 MINOR REVISIONS, CHANGED RECORD FORMATS
COOKE        03-83 MINOR REVISIONS, ADDED PEDIGREE, ETC
              04-83 MINOR REVISIONS
              11-83 REVISIONS FOR NEW RADAR TAPES
*****
VARIABLES:
NAME
-----
INTERNAL
MODE
-----
EDITED
ERD(20)
H1
HOUR
IBEG
IUNIT
IUNIT1
IUNIT2
LAT0
LOCA
LONG
MERGED(6)
NBAD
NF
NF1
NF2
RAD(13)
RAD2(4)
RADAR(6)
RESTR
S
STIME
T1
W
ZEN(60)
COMMON/2/
DD,DM,DS,DECOR R*4
I
EPHEMERIS DATA: DECLINATION(ANGLE)
I
*****
00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000210
00000220
00000230
00000240
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ORIGINAL
OF POOR QUALITY

IV-64

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ORIGINAL PAGE
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LOGICALM1 EDITED(6),RADAR(6),MERGED(6),LAUNCH(30)
LOGICALM4 SITE(4)
REALM4 LAT0,LON0
REALM8 RAD2(4),SUM
REALM8 TMTAP,'OZONE' //,RDTAP,'RADAR' //,MRTAP,'MERGE' //,
1 PLACE(6),'WALLOPS','CHURCHIL','NATAL','PRIMROSE',
2 'POKER FL','MARABIO',
EQUIVALENCE (RAD(10),SITE(1))
COMMON /Z/RH,RM,RS,RACOR,DD,DM,DS,DECOR,
KSH,SM,SS,GMT,REM,RMS,SOLARZ
COMMON/TEMPER/ NUM(100,3),SUM(100,3),TOP(100,3),BOT(100,3)
DATA RLOW/-75.48,-94.07,-35.25,-110.08,-147.48,-56.72/
DATA RLAT/37.85,58.75,-5.92,54.80,65.12,-64.24/

C
LINE = 0
LEN = 0
LEN1 = 0
LENF = 0

C
C
C READ IN TAPE INFORMATION, EPHEMERIS DATA, AND LOCATION

READ(5,1000) EDITED,MF,IUNIT
READ(5,1000)MERGED,MF1,IUNIT1
READ(5,1000) RADAR,MF2,IUNIT2,MODE
READ (5,1020) PED(2)
READ (5,1050) LOCA,RESTR,IBEG,NBAD,LAUNCH
IF (LOCA.EQ.0. OR. LOCA.GT.6.) GO TO 950
READ(5,1100)RH,RM,RS,RACOR
READ(5,1100)DD,DM,DS,DECOR
READ (5,1100) SH,SM,SS,HOURL
IF (MODE.EQ.2) GO TO 540
14 IF (NBAD.EQ.0) GO TO 15
IF (NBAD.GT.20) NBAD=20
DO 15 I=1,NBAD
READ (5,1150) BADI(I),BAD2(I)
15 CONTINUE

C
C PRINT OUT HEADER, TAPE INFORMATION, EPHEMERIS DATA, AND LOCATION

WRITE (6,2010)
WRITE (6,2020)
WRITE (6,2010)
WRITE (6,2030)
WRITE (6,2040) TMTAP,EDITED,IUNIT,NF
WRITE (6,2040) RDTAP,RADAR,IUNIT2,MF2
IF (MODE.NE.2) WRITE(6,2041)
IF (MODE.EQ.2) WRITE(6,2042)
2041 FORMAT ('+',83X,'MESUP')
2042 FORMAT ('+',83X,'PASS1')
WRITE (6,2040) MRTAP,MERGED,IUNIT1,MF1
WRITE (6,2050)
WRITE (6,2010)
IF (MODE.EQ.2) WRITE(6,2015) RAD,STIME
2015 FORMAT('0','RADAR PED: ',F5.0,2X,F4.0,2X,F4.0,2X,F7.0,2X,F8.1,2X,
X F7.3,2X,F8.3,2X,F7.0,2X,F7.0,2X,4A4,' LAUNCH TIME=',F7.0,
X ' SECONDS')
WRITE (6,2060)

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ORIGINAL PAGE
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WRITE(6,2070)PLACE(LOCA),RH,RH,RS,RACOR,DD,DM,DS,
1 DECOR,SH,SM,SS,HOUR,RESTR,LAUNCH
WRITE(6,2090)
WRITE(6,3000) IBEG,NBAD
IF(NBAD.GT.0) WRITE(6,2095)(BAD1(I),BAD2(I),I=1,NBAD)
WRITE(6,2050)
WRITE(6,2010)
WRITE(6,2050)

C MOUNT ALL INPUT/OUTPUT TAPES
C
C CALL MOUNT(1,IUNIT,EDITED,NF)
C CALL MOUNT(2,IUNIT1,MERGED,NF1)
C CALL MOUNT(1,IUNIT2,RADAR,NF2)
C LONG=RLON(LOCA)
C LAT0=RLAT(LOCA)

C VERIFY EQUIVALENCE OF RADAR AND EDIT FLIGHT NUMBERS.
C
IF (MODE .EQ. 2) GO TO 17
CALL FREAD(RAD(1),IUNIT2,LEN1,*560,*580)

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ORIGINAL PAGE 2
OF POOR QUALITY

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17 CALL FREAD(ERD(1),IUNIT,LEN,*570,*590)
   IF (RAD(2) .NE. ERD(2)) GO TO 550
C
C WRITE RADAR AND EDIT PEDIGREES ON MERGE TAPE.
CALL FWRITE(RAD(1),IUNIT1,LENF)
  LINE = LINE + 1
CALL FWRITE(ERD(1),IUNIT1,LENF)
  LINE = LINE + 1
C
C ESTABLISH PEDIGREE ARRAY AND WRITE ON MERGE TAPE.
PED(1) = -500.
CALL RPDAT0(1,IYMD)
PED(3) = IYMD(2)*10000 + IYMD(3)*100 + IYMD(1)
PED(4) = RH
PED(5) = RM
PED(6) = RS
PED(7) = RACOR
PED(8) = DD
PED(9) = DM
PED(10) = DS
PED(11) = DECOR
PED(12) = SM
PED(13) = SH
PED(14) = SS
DO 20 I = 15,20
  PED(I) = 0.0
20 CONTINUE
CALL FWRITE(PED(1),IUNIT1,LENF)
  LINE = LINE + 1
WRITE(6,3020) PED
3020 FORMAT ('0PEDIGREE:',/,/,1X,F5.0,2X,F5.1,1X,F7.0,3F6.2,8(1X,F8.2),
1 6(1X,F2.0))
  WRITE(6,2005)
C
C READ IN RADAR DATA UP TO 3000 RECORDS
C
N=0
IF (MODE .EQ. 2) GO TO 545
DO 100 I=1,3000
  CALL FREAD(RAD(1),IUNIT2,LEN1,*200,*910)
  IF(I.EQ.1) GO TO 90
  IF(ABS(RAD(1)-T1(N)) .GT.90. .OR. ABS(RAD(8)-H1(N)) .GT.
1 1 (H1(N)*0.5))GO TO 100
  N=N+1
90 N=N+1
  T1(N)=RAD(1)
  H1(N)=RAD(8)
  S(N)=RAD(6)
  W(N)=RAD(7)
100 CONTINUE
200 CONTINUE
C
C COMPUTE ZENITH ANGLE FOR EACH 60 SECONDS
C
210 K=0
DO 220 KK=1,N,60
  K=K+1
  TZ(K)=T1(KK)

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OF POOR QUALITY

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GMT=HOUR+(TZ(K)/3600.)
RNS=S(KK)
REN=H(KK)
CALL ZENITH(LONO,LATO,MODE)
ZEN(K)=SOLARZ
220 CONTINUE
C
C READ IN EDITED OZONE DATA
C
IBEG=IBEG-1
IF (IBEG.EQ. 0) GO TO 300
DO 290 IC=1,IBEG
CALL FREAD (ERD(1),IUNIT,LEN,*920,*930)
290 CONTINUE
300 CONTINUE
NI=1
CALL FREAD(ERD(1),IUNIT,LEN,*920,*930)
IF (NBAD.EQ. 0) GO TO 370
DO 350 IC=1,NBAD
350 IF (ERD(1).GT.BAD1(IC).AND.ERD(1).LT.BAD2(IC)) GO TO 300
370 CONTINUE
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226JUL84 08.52.34 - VOL=SACC10, DSN=Z8SAC.MERGE.CNTL

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00002220  CYC = ERD(15)
00002230  SAM = ERD(20)
00002240  TEM = ERD(19)
00002250  BAT = ERD(18)
00002260  CAV = ERD(17)
00002270  DO 450 JJ=1,4
00002280  IF (ERD(J) -LT. RESTR) ERD(J)=ERD(J)+3600.
00002290  IF (ERD(J) .GT. TI(N)) GO TO 940
00002300  C SEARCH FOR CORRESPONDING RADAR DATA
00002310  DO 400 JJ=N1,N
00002320  JS=JJ
00002330  IF(TI(JJ).GT.ERD(J))GO TO 420
00002340  400 CONTINUE
00002350  GO TO 450
00002360  420 CONTINUE
00002370  JS=JS-2
00002380  IF(JS.LE.0) JS=1
00002390  JE=JS+3
00002400  II=0
00002410  DO 430 I=JS,JE
00002420  II=II+1
00002430  TIME(II)=TI(I)
00002440  ALT(II)=H1(I)
00002450  430 CONTINUE
00002460  T2=ERD(J)
00002470
00002480  INTERPOLATE FOR ALTITUDE
00002490
00002500  ERD(J+15)=AITKEN(TIME,ALT,T2,4)
00002510  N1=JS+2
00002520  450 CONTINUE
00002530
00002540  INTERPOLATE FOR ZENITH ANGLE
00002550
00002560  DO 500 JJ=1,K
00002570  JS=JJ
00002580  IF(TZ(JJ).GT.ERD(1)) GO TO 520
00002590  500 CONTINUE
00002600  520 CONTINUE
00002610  JS=JS-2
00002620  IF(JS.LE.0) JS=1
00002630  JE=JS+3
00002640  IF (JE.GT.K) JE=K
00002650  II=0
00002660  DO 530 I=JS,JE
00002670  II=II+1
00002680  TIME(II)=TZ(I)
00002690  ALT(II)=ZEN(I)
00002700  530 CONTINUE
00002710  T2=ERD(1)
00002720  ERD(20)=AITKEN(TIME,ALT,T2,II)
00002730  ERD(2) = CYC
00002740  ERD(3) = SAM
00002750  ERD(4) = TEM
00002760  ERD(10) = BAT
00002770  ERD(15) = CAV
00002780  CALL FWRITE(ERD(1),IUNIT1,LENF)

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ORIGINAL PAGE
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550 WRITE (6,2550) RAD(2),ERD(2)
STOP
C
C RADAR PEDIGREE NOT IN RECORD 1.
560 WRITE (6,2560)
STOP
C
C EDIT PEDIGREE NOT IN RECORD 1.
570 WRITE (6,2570)
STOP
C
C ERROR IN RADAR PEDIGREE.
580 WRITE (6,2580)
STOP
C
C ERROR IN EDIT PEDIGREE.
590 WRITE (6,2590)
STOP
C
C ERROR IN RADAR TAPE
910 WRITE(6,2910) I
GO TO 100
C EOF ON TM TAPE
920 WRITE(6,2920)
GO TO 999
C ERROR ON TM TAPE
930 WRITE(6,2930)
GO TO 300
C NO RADAR DATA FOR TM TAPE
940 WRITE(6,2940) ERD(J),TI(N)
GO TO 999
950 WRITE (6,2950) LOCA
2950 FORMAT(' MAIN 2950: LOCA = ',I2,' OUT OF RANGE')
999 CONTINUE
IF (LINE.GT.10) CALL PRINTM
WRITE(6,2999)LINE
STOP
1000 FORMAT(1X,6A1,4X,2I5,3X,I2)
1020 FORMAT(F5.1)
1050 FORMAT (1I,26X,F6.1,2X,I3,2X,I2,30A1)
1100 FORMAT(10X,4F10.2)
1150 FORMAT(F6.1,2X,F6.1)
2000 FORMAT(1X,F9.3,F6.3,F4.0,F5.1,5F5.0,F5.2,4F5.0,F6.1,4F8.1,F8.2)
2005 FORMAT('1 S0 SEC CYCLE SAM TEMC S0 S1 S2',
X' S3 MARK BATV COM0 COM1 COM2 COM3 CMAVE S0 ALT S1 ALT',
X' S2 ALT S3 ALT SZA')
2010 FORMAT (1X,I3('*****'),'**')
2020 FORMAT (/,1X,42X,'PROGRAM: MERGE UPDATED NOV, 1983'//)
2030 FORMAT (/,1X,42X,'TAPE INFO: NAME UNIT FILE#')
2040 FORMAT (1X,46X,A8,2X,6A1,5X,I2,8X,I2)
2050 FORMAT (/)
2060 FORMAT (/,1X,2X,'LAUNCH SITE RH RM RS RACOR DD',
1 ' , DM DS DECOR SH SM SS HOUR RESTR',
2 ' , FLIGHT DATE AND TIME',/)
2070 FORMAT (1X,1X,A8,3X,2F7.2,F6.2,F7.2,F8.2,2F6.2,F8.2,F7.2,
1 2F6.2,F7.2,F9.2,30A1)
2090 FORMAT (/,1X,16X,'BEG. RECORD # BAD RECORDS START END',/)

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2095 FORMAT(50Y,2F10.1)/)
2550 FORMAT(1X,'MAIN 2550: CONFLICT IN FLIGHT NUMBERS',4X,'RADAR FLT ',F5.1)
2560 FORMAT(1X,'MAIN 2560: RADAR PEDIGREE MISSING FROM REC 1 OF RADAR',F5.1)
2570 FORMAT(1X,'MAIN 2570: EDIT PEDIGREE MISSING FROM REC 1 OF EDIT',F5.1)
2580 FORMAT(1X,'MAIN 2580: ERROR IN READING RADAR PEDIGREE')
2590 FORMAT(1X,'MAIN 2590: ERROR IN READING EDIT PEDIGREE')
2910 FORMAT(1X,'MAIN 2910: READ ERROR AFTER RADAR RECORD NO:',I5)
2920 FORMAT(1X,'MAIN 2920: END OF FILE ON EDIT OZONE TAPE.')
2930 FORMAT(1X,'MAIN 2930: READ ERROR ON EDIT OZONE TAPE.')
2940 FORMAT(1X,'MAIN 2940: TM TIME',F11.3,' IS GT LAST RADAR TIME',F11.3,10X,'STOP PROCESSING')
2999 FORMAT(1X,'MAIN 2999: NUMBER OF RECORDS ON MERGE TAPE IS',I7)
3000 FORMAT(1X,19X,I3,15X,I3)
      END
C
C
C *****
C SUBROUTINE ZENITH
C *****
C                                     6/10/80
C *****
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PROGRAMMER: EUGENE H. SHAFFER/SASC S. COOKE 11/83
LON = DEG. E; DD=DH

PURPOSE:
TO COMPUTE THE ZENITH ANGLE GIVEN ALL NECESSARY
EPHEMERIS DATA, LATITUDE, AND LONGITUDE.

CALLING SEQUENCE:
CALL ZENITH (LONO,LATO)

C REED/BATLUCK 11-82 :ADDED LAT DEPENDENT EARTH RADIUS
C COOKE 11-83 :ADDED MODE
C*****
C VARIABLES:
C NAME TYPE I/O DESCRIPTION
C ----
C INTERNAL
C DECU R*4 0 DECLINATION TIME
C DECORR R*4 0 DECLINATION CORRECTION
C LONO R*4 I LATITUDE OF LAUNCH SITE - DEG. E
C MODE Y*4 I LONGITUDE OF LAUNCH SITE - DEG. N
C RO R*4 I IF MODE = 2, RNS AND REM ARE DEG.
C R1 R*4 I RADIUS OF EARTH
C RAU R*4 I ANGLE CONVERSION
C RACORR R*4 0 RIGHT ASCENSION TIME - HOURS
C SIDI R*4 0 RIGHT ASCENSION CORRECTION -SECONDS
C COMMON/Z/
C DD,DM,DS,DECOR R*4 I EPHEMERIS DATA: DECLINATION, DEG.
C RH,RM,RS,RACOR R*4 I EPHEMERIS DATA: RIGHT ASCENSION, HR
C SH,SM,SS R*4 I EPHEMERIS DATA: SIDEREAL TIME, HR
C SOLARZ R*4 0 ZENITH ANGLE
C*****
C SUBROUTINE ZENITH (LONO,LATO,MODE)
C REAL LAT,LATO,LON,LONO,LATR
C DIMENSION RAD2(4)
C COMMON /Z/RH,RM,RS,RACOR,DD,DM,DS,DECOR,
C *SH,SM,SS,GMT,REM,RNS,SOLARZ
C
C RAU=RH+RM/60.+RS/3600.
C RACORR=RACOR/3600.
C DECU=DD+DM/60.+DS/3600.
C IF(DD.LT.0)DECU=DD-DM/60.-US/3600.
C DECORR=DECOR/3600.
C SIDI=SH+SM/60.+SS/3600.
C
C LATITUDE AND LONGITUDE OF LAUNCH SITE
C
C C =57.29578
C R1=1.0/C
C RO=6.371E6
C LATR=LATO*R1
C IF (MODE .EQ. 2) GO TO 200

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C FORMULA FROM BASIC PHYSICS OF THE SOLAR SYSTEM
C BLANCO & MCCUSKEY, 1961 PAGE 83
R0=6378388.*(1-3.367E-03*(SIN(LATR))**2+7.1E-06*(SIN(2.*LATR))**2)
C DEGREE-RAD CONVERSION, EARTH RADIUS (M)
C INSTANTANEOUS TIME AND RANGE EAST-WEST AND NORTH-SOUTH
C
    LAT=LAT0+C*RNS/R0
    LON=LON0+C*REW/(R0*COS(LAT0*R1))
    20 LON=LON/15.
C
C CONVERT DEGREES TO HOURS 360DEG/24HR
C
    DEC=DECU*(GMT*DECORR)/24.
    RA=RAU*(GMT*RACORR)/24.
    DL=0.5*R1*(LAT-DEC)
    SL=0.5*R1*(LAT+DEC)
    BD=7.5*R1*(1.00273*GMT+SIDT-RA+LON)
C
    1.0027379 = SOLAR DAY/SIDEREAL DAY
C
    F1=COS(BD)*SIN(DL)

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E1=SIN(BD)*COS(SL)
NM=ATAN2(F1,E1)
F2=COS(BD)*COS(DL)
E2=SIN(BD)*SIN(SL)
NP=ATAN2(F2,E2)
F3=SIN(HP)*TAN(DL)
E3=SIN(HM)
ZA=2.0*ATAN2(F3,E3)*C
IF(ZA LT 0.) ZA=ZA+360.0
SOLARZ=ZA
GO TO 999
200 LAT = RNS
LON = REM
GO TO 20
999 RETURN
END

*****
FUNCTION AITKEN
PROGRAMMER: EUGENE H. SHAFFER/SASC
6/10/80
PURPOSE:
A FOUR POINT INTERPOLATION SCHEME USING THE
AITKEN INTERPOLATION METHOD.
CALLING SEQUENCE:
AITKEN (X,Y,XHAT,N)
*****
VARIABLES:
NAME TYPE I/O DESCRIPTION
-----
INTERNAL
X(4) R*4 I X-VALUES FOR INTERPOLATION
XHAT R*4 I X-VALUE FOR WHICH Y IS TO BE COMPUTED
Y(4) R*4 I Y-VALUES FOR INTERPOLATION
YAIK(4) R*4 O COMPUTED Y-VALUE
*****
FUNCTION AITKEN(X,Y,XHAT,N)
DIMENSION YAIK(4),YAIK(4),X(4),Y(4)
DO 10 I=1,N
YAIK(I)=Y(I)
DO 20 J=1,N
IF ((XAIK(J) - XAIK(I-1)) .LE. 0.) WRITE(6,2010) J,I,N,
X
XAIK(I),XHAT,X(I),XAIK(J),XAIK(I-1)
2010 FORMAT(' TEST AITKEN 2010: J=',I2,' I=',I2,' N=',I2,' XAIK(I)=' ,
X F10.3, ' XHAT=' ,F10.3, ' X(I)=' ,F10.3, ' XAIK(J)=' ,F10.3,
X , XAIK(I-1)=' ,F10.3)
YAIK(J)=(XAIK(J)*YAIK(I-1)-XAIK(I-1)*YAIK(J))/(XAIK(J)-XAIK(I-1))
20 CONTINUE
AITKEN=YAIK(N)

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C C
C *****
C C
C SUBROUTINE RADAR2(RADZ,TI,H1,S,W,STIME,N,IUNIT2)
C COOKE          11/83
C C
C C RADAR2 READS IN THE INPUT DATA FROM 9 TRACK ECLIPSE PASS1 TAPES
C C (MODE 2). IN THIS CASE, THE RADAR TAPE SUPPLIED BY HALLOPS IS
C C USED DIRECTLY IN THE MERGE PROGRAM RATHER THAN USING A INTER-
C C MEDIATE REFORMATTED RADAR TAPE.
C C DIMENSION TI(3000),HI(3000),S(3000),W(3000)
C REAL*8 RADZ(4)
C C INITIALIZE VARIABLES AND ARRAYS
C C      TI(1) = 0.
C C      CALL CMOVE(TI(1),TI(2),11996)
C C      CALL CMOVE(TI(1),HI(1),12000)
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00005220 CALL CHOVE(TI(1),S(1),L2000)
00005222 CALL CHOVE(TI(1),W(1),L2000)
00005224 N = 0
00005226 C READ IN RADAR DATA UP TO 3000 RECORDS.
00005228 DO 100 I = 1,3000
00005230 CALL FREAD(RAD2(1),IUNIT2,32,*999,*200)
00005232 C TEST FOR INVALID ALTITUDE. IF ALTITUDE INVALID, SKIP RECORD.
00005234 IF (N.GE.1 .AND. (ABS(HI(N)-RAD2(2)).GT. 5000.)) GO TO 100
00005236 N = N + 1
00005238 TI(N) = RAD2(1) + STIME
00005240 C TEST FOR DUPLICATE TIMES FROM RADAR TAPE. IF SO, SKIP RECORD.
00005242 IF (N.GT.1 .AND.(TI(N).EQ.TI(N-1))) GO TO 90
00005244 HI(N) = RAD2(2)
00005246 S(N) = RAD2(3)
00005248 W(N) = RAD2(4)
00005250 GO TO 100
00005252 90 N = N - 1
00005254 100 CONTINUE
00005256 200 WRITE(6,2200) I
00005258 2200 FORMAT(/,IX,'RADAR2 2200: READ ERROR ON INPUT RADAR TAPE AFTER',
00005260 X' RECORD ',I5,2X,'PROCESSING CONTINUING')
00005262 GO TO 100
00005264 999 RETURN
00005266 END
00005268 C *****
00005270 SUBROUTINE TMPAVE(ERD)
00005272 C
00005274 C PROGRAMMERS: E. REED, S. COOKE NOV 1983
00005276 S. COOKE ADDED TO MERGE PGM FEB 1984
00005278 C
00005280 FOR ALTITUDES LESS THAN 45KM AND S3 LESS THAN 100 COUNTS, TMPAVE
00005282 OBTAINS THE AVERAGE COUNTS FOR S1, S2, AND S3 AS A FUNCTION OF
00005284 TEMPERATURE IN 0.5 DEGREE INCREMENTS, BETWEEN 40 AND -10 C.
00005286 REAL*8 SUM
00005288 DIMENSION ERD(20), TMP(100)
00005290 COMMON/TEMPER/ NUM(100,3),SUM(100,3),TOP(100,3),BOT(100,3)
00005292 DATA INIT/0/
00005294 C
00005296 TIM = ERD(4)
00005298 S3 = ERD(8)
00005300 ALT = ERD(16)
00005302 IF (INIT.NE. 0) GO TO 20
00005304 NUM(1,1) = 0
00005306 CALL CHOVE (NUM(1,1),NUM(2,1),5996)
00005308 DO 10 I = 1,100
00005310 TMP(I) = 40. - 0.5*I
00005312 BOT(1,1) = 1000.
00005314 BOT(1,2) = 1000.
00005316 10 BOT(1,3) = 1000.
00005318 INIT = 1
00005320 C INITIALIZATION COMPLETED
00005322 C
00005324 20 IF (S3.GT.100. .OR. ALT.GT.45000. .OR. TIM.GT.39.74 .OR.
00005326 00005328 00005330 00005332 00005334 00005336 00005338 00005340 00005342 00005344 00005346 00005348 00005350 00005352 00005354 00005356 00005358 00005360 00005362 00005364 00005366 00005368 00005370 00005372 00005374 00005376 00005378 00005380 00005382 00005384 00005386 00005388 00005390 00005392 00005394 00005396 00005398 00005400 00005402 00005404 00005406 00005408 00005410 00005412 00005414 00005416 00005418 00005420 00005422 00005424 00005426 00005428 00005430 00005432 00005434 00005436 00005438 00005440 00005442 00005444 00005446 00005448 00005450 00005452 00005454 00005456 00005458 00005460 00005462 00005464 00005466 00005468 00005470 00005472 00005474 00005476 00005478 00005480 00005482 00005484 00005486 00005488 00005490 00005492 00005494 00005496 00005498 00005500 00005502 00005504 00005506 00005508 00005510 00005512 00005514 00005516 00005518 00005520 00005522 00005524 00005526 00005528 00005530 00005532 00005534 00005536 00005538 00005540 00005542 00005544 00005546 00005548 00005550 00005552 00005554 00005556 00005558 00005560 00005562 00005564 00005566 00005568 00005570 00005572 00005574 00005576 00005578 00005580 00005582 00005584 00005586 00005588 00005590 00005592 00005594 00005596 00005598 00005600 00005602 00005604 00005606 00005608 00005610 00005612 00005614 00005616 00005618 00005620 00005622 00005624 00005626 00005628 00005630 00005632 00005634 00005636 00005638 00005640 00005642 00005644 00005646 00005648 00005650 00005652 00005654 00005656 00005658 00005660 00005662 00005664 00005666 00005668 00005670 00005672 00005674 00005676 00005678 00005680 00005682 00005684 00005686 00005688 00005690 00005692 00005694 00005696 00005698 00005700 00005702 00005704 00005706 00005708 00005710 00005712 00005714 00005716 00005718 00005720 00005722 00005724 00005726 00005728 00005730 00005732 00005734 00005736 00005738 00005740 00005742 00005744 00005746 00005748 00005750 00005752 00005754 00005756 00005758 00005760 00005762 00005764 00005766 00005768 00005770 00005772 00005774 00005776 00005778 00005780 00005782 00005784 00005786 00005788 00005790 00005792 00005794 00005796 00005798 00005800 00005802 00005804 00005806 00005808 00005810 00005812 00005814 00005816 00005818 00005820 00005822 00005824 00005826 00005828 00005830 00005832 00005834 00005836 00005838 00005840 00005842 00005844 00005846 00005848 00005850 00005852 00005854 00005856 00005858 00005860 00005862 00005864 00005866 00005868 00005870 00005872 00005874 00005876 00005878 00005880 00005882 00005884 00005886 00005888 00005890 00005892 00005894 00005896 00005898 00005900 00005902 00005904 00005906 00005908 00005910 00005912 00005914 00005916 00005918 00005920 00005922 00005924 00005926 00005928 00005930 00005932 00005934 00005936 00005938 00005940 00005942 00005944 00005946 00005948 00005950 00005952 00005954 00005956 00005958 00005960 00005962 00005964 00005966 00005968 00005970 00005972 000059
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```

X  TIN.LT.-10.24) GO TO 990
  IT = INT(80. - 2.MTIN)
  DO 50 J = 1,3
    CT = ERD(J+5)
    IF (CT.LT. 0.) GO TO 50
    NUM(IT,J) = SUM(IT,J) + 1
    SUM(IT,J) = SUM(IT,J) + CT
    IF (CT.GT. TOP(IT,J)) TOP(IT,J) = CT
    IF (CT.LT. BOT(IT,J)) BOT(IT,J) = CT
  50  CONTINUE
      GO TO 990

C  DISPLAY CONTENTS OF ARRAYS.
  ENTRY PRINTM
  WRITE (6,2050)
  2050 FORMAT(/,IX,'DEG C  SLAVE MAX  MIN  N  S2AVE  MAX  '
X 'MIN  N  S3AVE MAX MIN  N',/)
  DO 100 I = 1,100
    S1 = 0.
    S2 = 0.
    S3 = 0.

```

```

N1 = NUM(I,1)
N2 = NUM(I,2)
N3 = NUM(I,3)

C FIND AVG. COUNT FOR S1. IF MORE THAN 6 VALUES FOR S1, ELIMINATE
C HIGHEST AND LOWEST BEFORE FIGURING AVERAGE. IF NO VALUES EXIST FOR S2
C FOR THIS TEMP. LEVEL, GO ON TO CALCULATE S2 AVG.
IF (N1.EQ.0 .AND. N2.EQ.0 .AND. N3.EQ.0) GO TO 100
IF (N1 .EQ. 0) GO TO 60
IF (N1 .GT. 6) GO TO 55
S1 = SUM(I,1)/N1
GO TO 60
55 S1 = (SUM(I,1) - TOP(I,1) - BOT(I,1))/(N1 - 2)
C FIND AVG. COUNT FOR S2. IF MORE THAN 6 VALUES FOR S2 FOR THIS TEMP.
C LEVEL, ELIMINATE HIGHEST AND LOWEST BEFORE FINDING AVG. IF NO VALUES
C EXIST FOR THIS LEVEL, GO ON TO CALCULATE S3 AVG.
60 IF (N2 .EQ. 0) GO TO 70
IF (N2 .GT. 6) GO TO 65
S2 = SUM(I,2)/N2
GO TO 70
65 S2 = (SUM(I,2) - TOP(I,2) - BOT(I,2))/(N2 - 2)
C FIND AVG. COUNT FOR S3. IF MORE THAN 6 VALUES FOR S3 FOR THIS
C TEMPERATURE LEVEL, DISCARD HIGHEST AND LOWEST BEFORE CALCULATING
C AVG. IF NO VALUES EXIST, PRINT LINE AND GO ON TO NEXT TEMP. INCREMENT.
70 IF (N3 .EQ. 0) GO TO 80
IF (N3 .GT. 6) GO TO 75
S3 = SUM(I,3)/N3
GO TO 80
75 S3 = (SUM(I,3) - TOP(I,3) - BOT(I,3))/(N3 - 2)
C PRINT LINE
80 X WRITE(6,2080) TMP(I),S1,TOP(I,1),BOT(I,1),N1,S2,TOP(I,2),
2080 BOT(I,2),N2,S3,TOP(I,3),BOT(I,3),N3
2080 FORMAT(1X,F5.1,F8.3,2F6.1,15,F10.3,2F5.1,15)
100 CONTINUE
990 RETURN
END

```

*** END OF MEMBER ***

658 RECORDS PROCESSED

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OF POOR QUALITY

MEMBER=SMOOTH

26JUL84 08.53.47 - VOL=SACC09, DSN=Z8SAC.SMOO.CNTL

```

*****
SMOOTH SIGNAL PROGRAM          6/26/80
EDITION: 1
LANGUAGE:  FORTRAN
COMPUTER:  IBM 360/75, 360/91, 3081
OPERATING SYSTEM: G. S. F. C.
PROGRAMMER: EUGENE H. SHAFFER/SASC
REVISED: REED/BATLUCK
          COOKE      ADDED PEDIGREE          12/82
          "          ADDED TEMP DEPENDENT ZERO OFFSET,S2,S3 03/83
          "          ADDED MIN VALUE FOR COMPARD          06/83
          "          ADDED AVE COMP CHANNEL VALUE          "
          "          ADDED MINIMUM COUNT VALUE (2 CNTS)    11/83
          "          ADDED ISKIP TO SKIP BAD MERGE RECORDS 05/84

PURPOSE:
A PROGRAM TO READ THE MERGED SIGNAL AND RADAR DATA
AND TO SMOOTH THE DATA TO OBTAIN A SIGNAL VALUE FOR
EACH FILTER AT EVERY WHOLE KILOMETER LEVEL OVER THE
ENTIRE RANGE OF THE DATA.

THE INITIAL VERSION EVALUATED ERRORS AS DUE ONLY TO A
FIXED COUNT (E.G. DIGITIZATION ERROR), AND CARRIED THE
ESTIMATES IN "E AN" ER. THE 1982/3 VERSION ESTIMATES ERROR
AS DUE TO RANDOM NOISE AND OBTAINS ITS MAGNITUDE FROM THE
FIT OF POINTS TO THE LINE GENERATED IN LOGFIT.

*****
VARIABLES:
NAME
-----
INTERNAL
COMPMH
E(300)
HLOW
HTOP
ICODE
IRAT,L,RAT
ISKIP
IUNIT
IUNIT2
JK
LEN
MODE
NF
NF2
NR
OFF
PLOTX(50)
PLOTY(50)
RESULT(20)
TAPEIN(6)
TAPOUT(6)
X(800)

TYPE  I/O  DESCRIPTION
----  --  -
R*4   I    MIN ACCEPTABLE VALUE OF COMP WORD
R*4   I    ERROR FOR EACH PT. OF FIT
R*4   I    LOWEST HEIGHT OF DATA
R*4   I    HIGHEST HEIGHT OF DATA
I*4   I    END OF DATA INDICATOR
I*4   I    0: NO RATIOS; 1: S1/S0,S2/S0,S3/S0
I*4   I    0 OF BAD MERGE RECS TO BE SKIPPED
I*4   I    INPUT TAPE UNIT NUMBER
I*4   I    OUTPUT TAPE UNIT NUMBER
I*4   I    NUMBER OF HEIGHT INTERVALS
I*4   I    LRECL OF INPUT TAPE
I*4   I    =1 INSTRUM.=0 NONE,=-1 STAT
I*4   I    FILE NUMBER OF INPUT TAPE
I*4   I    FILE NUMBER OF OUTPUT TAPE
I*4   I    NUMBER OF INPUT RECORDS
I*4   I/O  OFFSETS FOR CHANS 0-3
R*4   I    ARRAY FOR X-VALUES OF PLOTS
R*4   I    ARRAY FOR Y-VALUES OF PLOTS
R*4   I/O  OUTPUT FOR I LEVEL FOR I FILTER
L*1   I    INPUT TAPE NAME
L*1   I    OUTPUT TAPE NAME
R*4   I/O  X-VALUES FOR FITTING INTERVAL(M)

```


26JUL84 08.53.47 - VOL=SACC09, DSN=Z8SAC.SMOO.CNTL

MEMBER=SMOOTH

```
C 9 BATTERY VOLTAGE
C 10 AVERAGE COMPENSATION WORD
C*****
C SUBROUTINES CALLED
C   GRAPH      DWRITE      CALSIZ      CMOVE
C   LOGFIT     FREAD      ENDPLT      RPDATA
C   OUTPUT     FWRITE     PLOTST
C   SELECT     MOUNT
C*****
C LOGICALX1 TAPEIN(6),TAPOUT(6)
C DIMENSION PLOTX(50),PLOTY(50),X(800),Y(800),E(800),
C X OFF(4),RESULT(20),R(20),PED(20),IYMD(3)
C COMMON/LABEL1/ N,S(4,800),H(4,800),ER(4,800)
C COMMON/LABEL2/SAVE(20,50,4)
C
C IMES = 6
C CALL CALSIZ(12.)
C CALL PLOTST(02001,4)
C
C READ INPUT INFORMATION.
C READ (5,1000) TAPEIN,NF,IUNIT
C READ (5,1000) TAPOUT,NF2,IUNIT2
C READ (5,1005) MODE,LRAT
C COMPNN IS GENERALLY SET TO 0.5*COMP WORD AFTER ATTITUDE IS STABLE.
C IN CASES WHERE SZA IS AROUND 60 DEGREES, COMPNN =
C COS(SZA) * MAX COMP WORD.
C READ (5,1010) HTOP,HLOW,COMPNN,ISKIP
C TA IS TEMP (DEG. C) FOR VALUES IN OFF; TB IS TEMP FOR S2 AND S3 ZERO
C OFFSETS GIVEN IN S2B AND S3B.
C READ (5,1030) OFF
C READ (5,1030) TA,TB,S2B,S3B
C
C MOUNT TAPES; READ AND WRITE RADAR,EDIT, AND MERGE PEDIGREES
C FROM MERGE TAPE ONTO OUTPUT TAPE.
C CALL MOUNT (1,IUNIT,TAPEIN,NF)
C CALL MOUNT (2,IUNIT2,TAPOUT,NF2)
C CALL FREAD(PED,IUNIT,LEN)
C CALL FWRITE(PED,IUNIT2,80)
C CALL FREAD(PED,IUNIT,LEN)
C CALL FWRITE(PED,IUNIT2,80)
C CALL FREAD(PED,IUNIT,LEN)
C CALL FWRITE(PED,IUNIT2,80)
C
C ESTABLISH SMOOTH PEDIGREE. PRINT OUT PEDIGREE AND INPUT INFORMATION;
C WRITE SMOOTH PEDIGREE ONTO OUTPUT TAPE.
C PED(1) = -400.
C READ (5,1040) PED(2)
C CALL RPDATA(1,IYMD)
C PED(3) = IYMD(2) * 10000 + IYMD(3) * 100 + IYMD(1)
C PED(4) = OFF(1)
C PED(5) = OFF(2)
C PED(6) = OFF(3)
C PED(7) = OFF(4)
C PED(8) = HTOP
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PED(9) = HLOW  
PED(10) = COMPMN  
PED(11) = TA  
PED(12) = TB  
PED(13) = S2B  
PED(14) = S3B  
DO 2 I = 15,20  
  PED(I) = 0.0  
  2 CONTINUE  
  WRITE (6,2035) PED(1),PED(2),P.D(3)  
  CALL FWRITE(PED,IUNIT2,80)  
  WRITE (6,2000) TAPEIN,NF,IUNIT  
  WRITE (6,2010) TAPOUT,NF2,IUNIT2  
  WRITE (6,2020) HTOP,HLOW,LRAI,MODE,COMPMN  
  WRITE(6,2025) OFF,TA,TB,S2B,S3B  
  HMAX = 100.*HTOP + 500.  
C  
C  
C MOVE INPUT DATA TO DISC  
NR=0
```

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      CALL GRAPH (PLOTX,PLOTY,JK,I,IRAT)
      800 CONTINUE
      IF(IRAT.EQ.1 .OR. LRAT.EQ.0) GO TO 900
      IRAT = 1
      GO TO 10
      900 CALL ENDPLT
      GO TO 999

C
C  ODDS AND ENDS
      910 WRITE (IMES,2910) NR
      2910 FORMAT ('OMAIN 2910: NUMBER OF MERGE RECORDS IS ONLY ',I4)
      1000 FORMAT (6A1,3(2X,I2))
      1005 FORMAT (I2,42X,I1)
      1010 FORMAT (2(2X,F4.1),2X,F4.0,2X,I4)
      1030 FORMAT (4(F6.1,2X))
      1040 FORMAT (F4.0)
      2000 FORMAT (////,1X,10X,'TAPE INFORMATION: NAME I/O',
      1      UNIT',/,1X,31X,6A1,3X,'INPUT',5X,I2,7X,I2)
      2010 FORMAT (1X,31X,6A1,3X,'OUTPUT',4X,I2,7X,I2)
      2020 FORMAT (////,1X,10X,'UPPER HEIGHT LIMIT:',F5.1,' KM',
      1      /,1X,10X,'LOWER HEIGHT LIMIT:',F5.1,' KM',10X,'RATIOS=',I2,

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X ' MODE=' ,I2,/,11X,'MINIMUM ACCEPTABLE COMPENSATION WORD = ',
X F6.1,/)
2025 FORMAT (1X,/,10X,' ZERO OFF-SETS: S0 S1 S2 S3',
1 10X,'TA TB S2B S3B',
1 1X,25X,F4.1,1X,F4.1,1X,F4.1,1X,F4.1,1X,F4.1,1X,F4.1)
2035 FORMAT (/,1X,20X,'FLT. NO.',5X,'RUN DATE')
2040 FORMAT (/,1X,10X,F5.0,6X,F4.0,8X,F7.0)
2075 FORMAT (/,1X,132('X'))
999 WRITE (IMES,2999)
2999 FORMAT ('OMAIN 2999: PROGRAM END')
STOP
END

```

```

C*****
C SUBROUTINE GRAPH 7/01/80
C PROGRAMMER: EUGENE H. SHAFFER/SASC
C REVISED: REED/BATLUCK DEC. 1982
C

```

```

C PURPOSE:
C TO PRODUCE A CAL-COMP PLOT OF THE SMOOTHED
C SIGNAL VALUES VERSUS HEIGHT.
C

```

```

C CALLING SEQUENCE:
C GRAPH (X,Y,N,I,IRAT)
C

```

```

C*****
C

```

VARIABLES:

NAME	TYPE	I/O	DESCRIPTION
------	------	-----	-------------

ARGUMENTS

I	I*4	I	FILTER NUMBER (1-4)
IRAT	I*4	I	INDICATOR FOR X COORDINATES
N	I*4	I	NUMBER OF POINTS TO BE PLOTTED
X(N)	R*4	I	X-AXIS DATA
Y(N)	R*4	I	Y-AXIS DATA

INTERNAL
(NONE)

SUBROUTINES CALLED

FRMADV
HORLIN
GRAPH
OGRID
SETGRD
VERLIN

```

SUBROUTINE GRAPH (X,Y,N,I,IRAT)
LOGICAL*1 LF(4)
DIMENSION X(N),Y(N)
DATA LF/'0','1','2','3'/

```

SET UP PLOT AND GRID

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C
CALL SETGRD (1.,1.,10.,8.,4)
IF(I.EQ.1)CALL OGRID (0.0,1000.,50,'F6.1'),'5,0.,75.,75,'I2'),'5,0)
IF(I.GT.1.AND. IRAT.EQ.1)CALL OGRID(-0.1,1.5,16,'F3.1'),'1,0.,75.,
* 75,'I2'),'5,0)
* IF(I.GT.1.AND.IRAT.EQ.0)CALL OGRID(-100.,1000.,55,'I4'),'5,0.,75.,
* 75,'I2'),'5,0)
C
WRITE GRAPH HEADINGS
C
CALL HORLIN ('UV SIGNAL S',11,5.5,0.5,0,0)
CALL HORLIN(LF(1),1,5.5,0.5,13,0)
IF(I.GT.1.AND.IRAT.EQ.1) CALL HORLIN('DIVIDED BY S0',
X 13,5.5,0.5,30,0)
CALL VERLIN ('HEIGHT (KM)',-11,0.5,4.5,0,0)
C
PLOT DATA
C
CALL PLOT (X,Y,N,'+')
CALL FPMADV
RETURN
C
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00002500
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*****
SUBROUTINE SELECT
PROGRAMMER: EUGENE H. SHAFFER/SASC
REVISED: REED/BATLUCK/COOKE DEC 82 - JUN 83

PURPOSE:
TO SELECT ALL DATA POINTS CENTERED AROUND A GIVEN
HEIGHT, AT LEAST A ONE KILOMETER INTERVAL OR 100
POINTS MUST MAKE UP THE SELECTED DATA.

AVERAGE VALUES OF CYCLE LENGTH AND COMPENSATION CHANNEL
ARE COMPUTED BASED ON 99 RECORDS CENTERED ON XCEN.
*****

VARIABLES:
NAME TYPE I/O DESCRIPTION
-----
ARGUMENTS
COMPMN R*4 I MIN ACCEPTABLE COMP WORD
HMAX R*4 I MAX ALTITUDE(M) FOR ACCEPTABLE DATA
ICODE I*4 I/O INDICATOR FOR END OF DATA
IRAT I*4 I INDICATOR FOR USING RATIOS
NREC I*4 I NUMBER OF RECORDS ON DISK
OFF R*4 I OFF-SETS FOR ALL CHANNELS
RESULT R*4 I/O OUTPUT ARRAY
S2B R*4 I S2 OFFSET AT TEMP B
S3B R*4 I S3 OFFSET AT TEMP B
TA R*4 I TEMP (C) FOR OFF
TB R*4 I TEMP (C) FOR S2B AND S3B
XCEN R*4 I CENTER OF INTERVAL, KM

COMMON/LABEL1/
ER(4,800) R*4 I ERRORS FOR ALL HEIGHT LEVELS
H(4,800) R*4 I HEIGHTS FOR ALL LEVELS (KM)
N I*4 I NUMBER OF PTS IN FITTING INTERVAL
S(4,800) R*4 I/O TELEMETRY SIGNAL VALUES

INTERNAL
HB R*4 0 LOWER HEIGHT OF INTERVAL (KM)
HT R*4 0 UPPER HEIGHT OF INTERVAL (KM)
NB I*4 0 LOW RECORD OF INTERVAL
NR I*4 0 LOW RECORD OF INTERVAL
NT I*4 0 HIGH RECORD OF INTERVAL
R(20) R*4 I SIGNAL VALUES FROM MERGE TAPE
*****

SUBROUTINES CALLED
DREAD, CMOVE
*****

SUBROUTINE SELECT(XCEN,NREC,ICODE,OFF,TA,TB,S2B,S3B,COMPMN,IRAT,
X RESULT,HMAX)
DIMENSION R(20),B(4),RESULT(20),OFF(4)
COMMON/LABEL1/ N,S(4,800),H(4,800),ER(4,800)

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00003180
00003190
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00003240
00003250

```

C INITIALIZE
C
C   IF (RESULT(2) .NE. 0.) GO TO 8
C   B(1) = 0.
C   CALL CMOVE(B(1),B(2),12)
C   IF (TA .EQ. TB) GO TO 8
C   B(3) = (S2B-OFF(3)) / (TB-TA)
C   B(4) = (S3B-OFF(4)) / (TB-TA)
C   SQRTH=SQRT(0.5)
C   8 NR=0
C   XC=XCENX)000.
C
C   FIND CENTER POINT OF DATA, ASSUMING A DESCENDING SONDE
C
C   10 CONTINUE
C   NR=NR+1
C   IF (NR .GT. NREC) GO TO 920
C   11 CALL DREAD (3,NR,R,810)
C   IF (R(16).LT.XC) GO TO 12
C   TMA=R(1)

```

ORIGINAL
OF POCB

```

HTA=R(16)
SZA=R(20)
GO TO 10
12 INB=R(1)
HTB=R(16)
SZB=R(20)
FRAC=(XC-HTB)/(HTA-HTB)
RESULT(5)=SZB+FRAC*(SZA-SZB)
RESULT(6)=TMB+FRAC*(TMA-TMB)
RESULT(7)=R(4)
RESULT(9)=R(10)
15 NT=NR-50
NB=NR+49
NX=NR
IF (NT.LE. 0) NB=100
IF (NT.LE. 0) NT=1
IF (NB.GT. NREC) NB=NREC
IF (NB.GE. NREC) NT=NREC-100
C FIND ALL DATA AROUND CENTER HEIGHT
C
16 CONTINUE
CALL DREAD (3,NT,R,816)
HT=R(16)/1000.
CALL DREAD (3,NB,R,816)
HB=R(16)/1000.
IF ((NT-HB).GE.2.0 .OR. (NB-NT).GT.800) GO TO 18
NT=NT-5
NB=NB+5
IF (NT.LE. 0) NT=1
IF (NB.GE. NREC) NB=NREC
GO TO 16
18 CONTINUE
N=0
J=0
COMP = 0.0
CYCLE = 0.0
C SELECT SIGNALS, AND HEIGHTS FOR THE INTERVAL. COMPUTE ERROR
C CALCULATE RATIOS IF REQUESTED (IRAT=1)
C
DO 200 I=NT,NB
CALL DREAD(3,I,R,8200)
IF (R(16).GT. HMAX) GO TO 200
N=N+1
IF(N.GT.800) GO TO 910
IF (IABS(I-NX).GT. 49) GO TO 50
J = J+1
COMP = COMP + R(15)
CYCLE = CYCLE + R(2)
50 DO 150 K=1,4
KF=K+4
S(K,N) = (R(KF)-OFF(K)-B(1) * (R(7))-TA)
IF (R(KF).LT. 2.0) S(K,N) = -99.
IF (R(K+10).LE.COMPMN) S(K,N) = -99.
C DEFINE ERROR AS Sqrt(.5/R)*2+(.5/R)**2 , I.E.=Sqrt(.5)/R
ER(K,N)=SQRTH

```

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IF(IRAT.EQ.1) GO TO 100
IF(R(KF).GT.1.0) ER(K,N) = SQRTH/R(KF)
GO TO 120
C IF RATIOS ARE REQUESTED DIVIDE S1,S2,S3 BY S0 AND COMPUTE ERROR
100 IF(K.EQ.1) GO TO 120
IF(R(5).LT.0.) GO TO 160
DENOM = S(1,N)
IF(ABS(DENOM).LT.0.5) GO TO 160
IF(R(KF).LT.2.0 .OR. S(K,N).LT.-90.) GO TO 110
S(K,N)=S(K,N)/DENOM
ER(K,N)=S(K,N)*0.5*SQRT(1/DENOM**2+1/DENOM**2)
GO TO 120
110 S(K,N) = -99.0
C CORRESPONDING ALTITUDES IN KILOMETERS
120 H(K,N)=R(K+15)/1000.
150 CONTINUE
GO TO 200
160 N=N-1
200 CONTINUE
IF(N.LT.5) GO TO 900
C OBTAIN AVERAGE CYCLE LENGTH AND COMP WORD

```

```

      RESULT(8) = CYCLE/J
      RESULT(10) = COMP/J
      GO TO 999
C   INSUFFICIENT NUMBER OF VALID VALUES
      900 WRITE(6,2900) N,H(1,1),H(1,M),XC
      2900 FORMAT(1X,'SELECT 2900: ONLY ',I3,' POINTS BETWEEN',F6.2,' AND',
        X F6.2,' KM, CENTERED AT',F6.2,' GO TO NEXT INTERVAL.')
      ICODE=-1
      GO TO 999
C   TOO MANY RECORDS IN HEIGHT INTERVAL
      910 WRITE(6,2910) H(1,1),H(1,800)
      2910 FORMAT(1X,'SELECT 2910: MORE THAN 800 CYCLES BETWEEN',
        X F7.2,' AND',F7.2,' KM.')
      GO TO 999
C   XC IS BELOW LOWEST ALT OF DATA
      920 WRITE(6,2920) XC,R(16)
      2920 FORMAT(1X,'SELECT 2920: REQUESTED CENTER ALTITUDE,',F8.2,
        X', IS LESS THAN LOWEST ALTITUDE IN DATA,',F8.2)
      ICODE=-2
      999 RETURN
      END
C *****
C   SUBROUTINE OUTPUT(N,IUNIT2)
C REED/BATLUCK/COOKE      DEC 82 - JUN 83
C ADDED COMP AND HTDIF COLUMNS      COOKE      NOV 1983
C ARGUMENTS
C   N      NUMBER OF HEIGHT LEVELS
C   IUNIT2 OUTPUT TAPE UNIT NUMBER
C *****
      DIMENSION ARR(7), BRR(17)
      COMMON/LABEL2/SAVE(20,50,4)
      DATA LEN2/80/
C PRINT COMMON PARAMETERS
      WRITE(6,2000)
      DO 20 J = 1,M
        ARR(1) = SAVE(2,J,1)
        ARR(2) = SAVE(6,J,1)
        ARR(3) = SAVE(5,J,1)
        ARR(4) = SAVE(7,J,1)
        ARR(5) = SAVE(8,J,1)
        ARR(6) = SAVE(9,J,1)
        ARR(7) = SAVE(10,J,1)
        WRITE(6,2010)ARR
      20 CONTINUE
C PRINT DATA FOR EACH FILTER: S3,S2,S1 AND S0
      DO 50 KF = 1,4
        K=5-KF
        NFIL = SAVE(1,1,K)
        WRITE(6,2050) NFIL
        IF(NFIL.GT.5) WRITE(6,2051)
        WRITE(6,2060)

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ORIGINAL
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OF FOUR

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DO 50 J = 1,N
  BRR(1) = SAVE (2,J,K)
  BRR(2) = SAVE (3,J,K)
  BRR(6) = SAVE (11,J,K)
  BRR(7) = SAVE (12,J,K)
  BRR(8) = BRR(6) - BRR(7)
  BRR(9) = SAVE (14,J,K)
  BRR(12) = SAVE (16,J,K)
  BRR(13) = SAVE (17,J,K)
  BRR(15) = SAVE (19,J,K)
  BRR(16) = SAVE (13,J,K)
  BRR(17) = SAVE (20,J,K)
  BRR(4) = (EXP(SAVE (4,J,K)) - 1.) * 100.
  BRR(3) = BRR(4) * BRR(2) * 0.01
  BRR(5) = BRR(12) * BRR(2)
  BRR(11) = (EXP(SAVE(15,J,K)) - 1.) * 100.
  BRR(10) = BRR(11) * BRR(9) * 0.01
  BRR(14) = (SAVE(18,J,K) - 1.) * 100.
50 WRITE(6,2070) BRR
C
C WRITE DATA ON TAPE
```

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DO 100 K = 1,4
DO 100 J = 1,M
100 CALL FWRITE(SAVE(1,J,K),IUNIT2,LEN2)
RETURN
2000 FORMAT('0','ALT-KM SECONDS      SZA  TMP C  CYCLE  BATTV  COMP')
2010 FORMAT(1X,F6.0,F8.1,F7.2,F7.1,F7.3,F6.2,F6.0)
2050 FORMAT('/',1X,'FILTER POSITION',I3)
2051 FORMAT('+',20X,' (DIVIDED BY S0)')
2060 FORMAT(1X,' KM CNT/RAT  STDCTS  STDx  SLOPE  START  END',
X ' COREL  DIFF  BASEIO  STDCTS  STDx  ABSORP  DABSORP  SETSDx',
X ' COREL  USD  PTS')
2070 FORMAT(1X,F3.0,F9.3,F9.4,F6.2,F9.4,F7.2,F7.2,F7.2,F9.3,
X F9.4,F6.2,F9.4,F7.2,F6.2,F5.0,F5.0)
END
C *****
C SUBROUTINE LOGFIT(M,S,E,RESULT,MODE)
C *****
C REED/BATLUCK/COOKE      DEC 82 - JUN 83
C LOGFIT FITS A CURVE OF THE FORM S=S0 EXP -(C(H-H0) ) TO THE SIGNAL
C VERSUS ALTITUDE DATA. THIS IS APPROXIMATED BY FITTING Y = A + BX
C WHERE Y = LN S, A=LN S0, B=-C, AND X =(H-H0). ( ALSO SEE P.R.BEVING-
C TON, DATA REDUCTION..., MCGRAW-HILL 1969, PP 180-185,104-105.)
C OUTLIERS (MORE THAN 2 S.D.) ARE DISCARDED.  PARAMETERS ARE PLACED
C IN RESULT. IF MOST VALUES ARE .LE. 0, THE DATA ARE AVERAGED.
C
C ARGUMENTS
C H      ALTITUDE
C S      CORRESPONDING COUNTS OR RATIO
C E      ERRORS DUE TO DIGITIZATION
C RESULT THE OUTPUT ARRAY
C
C MODE   =1 INSTRUM-1./ERR2 ; =2 NO MT; =-1 STAT. =1/Y(1)
C *****
C REALS SUM, SUMX, SUMY, SUMX2, SUMY2, SUMXY, SUMY2,
X XI, YI, WEIGHT, DELTA, VARNCE
C DIMENSION H(1), S(1), E(1), RESULT(20),CTS(5),CTL(5),Y(5),DF(5)
C
C MOLD = 0
NPTS = RESULT(13)
HBASE = H(NPTS)
110 N = 0
SUM=0.0
SUMX = 0.0
SUMY = 0.0
SUMX2 = 0.0
SUMXY = 0.0
SUMY2 = 0.0
210 DO 500 I = 1,NPTS
YI = S(I)
IF(YI.LE.0.0) GO TO 500
C ** TEST
C WRITE(6,2210) I,NPTS,S(I),YI
2210 FORMAT(1X,'LOGFIT 2210: I=',I3,1X,'NPTS=',I3,1X,'S(I)=' ,
X G11.4,1X,'Y(I)=' ,G11.4)

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YI = DLOG(YI)
XI = H(I)-HBASE
IF(MODE) 310,360,380
310 IF (YI) 340,360,320
320 WEIGHT = 1./YI
GO TO 410
340 WEIGHT = 1./(-YI)
GO TO 410
360 WEIGHT = 1.
GO TO 410
380 WEIGHT = 1./E(I)**2
410 N = N+1
SUM = SUM + WEIGHT
SUMX = SUMX + WEIGHT*XI
SUMY = SUMY + WEIGHT*YI
SUMX2 = SUMX2 + WEIGHT*XI*XI
SUMXY = SUMXY + WEIGHT*XI*YI
SUMY2 = SUMY2 + WEIGHT*YI*YI
500 CONTINUE
C CALCULATE COEFFICIENTS AND STANDARD DEVIATIONS
C

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C-3

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510 DELTA = SUMXSUMX2-SUMX*SUMX
    IF(DABS(DELTA) .LT. 1.0D-16) GO TO 700
A = (SUMX2*SUMY-SUMX*SUMXY)/DELTA
530 B = (SUMXY*SUM-SUMX*SUMY)/DELTA
610 IF(MODE.EQ.0 .AND. N.GT.2) GO TO 640
    VARNCE = 1.
    GO TO 670
640 C = N - 2
    VARNCE = (SUMY2+A*SUM+B*SUMX2-2.*(A*SUMY+B*SUMXY-A*B*SUMX))/C
    IF (VARNCE .LE. 1.0D-16) GO TO 700
670 SIGMAA = DSQRT(VARNCE*SUMX2/DELTA)
680 SIGMAB = DSQRT(VARNCE*SUM/DELTA)
R = (SUMX*SUMY - SUMX*SUMY)/DSQRT(DELTA*(SUMX*SUMY2-SUMY*SUMY))
C SHAPE CHECKS RESIDUALS
C IF(NOLD.NE.0.AND.A.GT.3.) CALL SHAPE(A,B,NPTS,H,S)
C IF(NOLD.NE.0) GO TO 800
C DISCARD POINTS WHICH ARE MORE THAN 2 STD DEV AWAY.

SD = DSQRT(VARNCE)
SD2 = 2. * SD
DO 690 I = 1,NPTS
    SI = S(I)
    IF (SI .LE. 0.) GO TO 690
C ** TEST
C WRITE(6,2690) I,NPTS,S(I),SI
2690 FORMAT(1X,'LOGFIT 2690: I=',I3,1X,'NPTS=',I3,1X,'S(I)=' ,G11.4,
X 1X,'SI=',G11.4)
TMP = A + B * (H(I)-HBASE)
ERCT = ABS(SI - EXP(TMP))
    IF (SI.GT.2.0 .AND. ERCT.LT.2.0 + (SI/100.)) GO TO 690
ERRR = ABS(ALOG(SI) - TMP)
    IF(ERRR .GT. SD2) S(I) = -99.
690 CONTINUE
NOLD = N
    IF(N.GT.(0.4*NPTS)) GO TO 110
C TOO MANY NEGATIVE VALUES OR DELTA IS TOO SMALL; DO SIMPLE AVERAGES
700 NOLD=0
705 N = 0
SUMY = 0.0
SUMY2 = 0.0
RMEAN = 0.0
ND=0
DO 720 I = 1,NPTS
    YI = S(I)
    IF(YI.LT.-50.0) GO TO 720
    IF (RESULT(1).GT.106. .AND. YI.LT.-0.2) GO TO 720
    N = N+1
SUMY = SUMY+YI
SUMY2 = SUMY2+YI*YI
720 CONTINUE
    IF(N.EQ.0) GO TO 760
RMEAN = SUMY/N
    IF(N.EQ.1) ND=1
VARNCE = (SUMY2-(SUMY**2)/N)/(N-1+ND)
    IF(VARNCE.LE.0.0) GO TO 764
SD = DSQRT(VARNCE)
SD2 = 2. * SD

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```

IF(NOLD.NE.0) GO TO 770
DO 740 I = 1,NPTS
IF(ABS(S(I)-RMEAN).LT.SD2) GO TO 740
S(I) = -99.0
740 CONTINUE
NOLD = N
GO TO 705
C  FILL OUTPUT ARRAY
760 RESULT(3) = 0.
764 GO TO 766
764 RESULT(3) = RMEAN
766 RESULT(18) = 0.
GO TO 780
770 RESULT(3) = RMEAN
780 RESULT(18) = SD
RESULT(4) = 0.
RESULT(14)=0.0
RESULT(15)=0.0
RESULT(16)=0.0
RESULT(17)=0.0
RESULT(19)=0.0

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      GO TO 820
      IF (N .GE. 0.5*NPTS) GO TO 815
      WRITE (6,2800) NPTS,NOLD,N,RESULT(1),RESULT(2),A,B,SD2
2800  FORMAT (1X,'LOGFIT 2800: NPTS =',I4,' NOLD =',I4,' N =',I4,
X' FP =',F4.0,' ALT =',F4.0,' A =',F8.4,' B =',F7.4,' TWO S.D. =',
X F7.3,' SI(CTS) LNSI DIF')
      CALL DISPLA (NPTS,S,M,A,B,HBASE,SD2)
      815 RESULT(3) = EXP(A+B*(RESULT(2)-HBASE))
C ** TEST
C
      WRITE(6,2815) SIGMAA,SIGMAB,RESULT(2),HBASE,A,B
2815  FORMAT(1X,'LOGFIT 2815: SIGMAA=',G10.3,1X,'SIGMAB=',G10.3,1X,
X 'RESULT(2) =',G10.3,1X,'HBASE=',G10.3,1X,'A =',G10.3,1X,'B =',G10.3)
      RESULT(4) = (SIGMAA*SIGMAA + SIGMAB*SIGMAB *
X (RESULT(2)-HBASE)**2)**0.5
      RESULT(14) = EXP(A)
      RESULT(15) = SIGMAA
      RESULT(16) = -B
      RESULT(17) = SIGMAB
      RESULT(18) = EXP(SD)
      RESULT(19) = R
      820 RESULT(11) = H(1)
      RESULT(12) = HBASE
      RESULT(20) = RESULT(13)
      RESULT(13) = N
      RETURN
      END
C *****
C SUBROUTINE MOLFRC
C THIS REPLACES THE UNUSED ROUTINES OF MULTIPLY FOR THE GERBER SC4020,
C AND THE SD4060 PLOTTERS, REDUCING LENGTH BY 15.4K. REED/BATLUCK 12/82
      ENTRY GERBER
      GO TO 999
      ENTRY SC4020
      GO TO 999
      ENTRY SD4060
      GO TO 999
999  RETURN
      END
      SUBROUTINE SHAPE(A,B,NPTS,H,S)
      REED/BATLUCK JAN 1983
C
C SHAPE EXAMINES THE RESIDUALS RESULTING FROM THE FITTED CURVE TO LOOK
C FOR A NON-RANDOM DISTRIBUTION. THE AVERAGE DEVIATION IS COMPUTED AND
C LISTED FOR 10 POINT GROUPS.
C
      DIMENSION H(1),S(1),AVE(80)
      N=0
      SUM=0
      K=0
      HBASE=H(NPTS)
      DO 200 I = 1,NPTS
      SI=S(I)
      IF(SI.LE.0.) GO TO 200
      E = SI-EXP(A+B*(H(I)-HBASE))
      SUM = SUM+E
      N = N+1
      IF(N.LT.10) GO TO 200

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C C C C C
      K = K+1
      AVE(K) = SUM/N
      N = 0
      SUM = 0
200  CONTINUE
      I = NPTS/2+1
      WRITE(6,2200) H(I),S(I), (AVE(N),N=1,K)
2200  FORMAT(2X,(1X,26F5.0))
      RETURN
      END
C C C C C
      SUBROUTINE DISPLA (NPTS,S,H,A,B,HBASE,SD2)
C REED/DATLUCK/COOKE
C JUNE 1983
C DISPLA PRINTS OUT THE OBSERVED AND COMPUTED VALUES FO A GIVEN LEVEL.
C DIMENSION H(1),S(1),CTS(5),CTL(5),Y(5),DF(5)
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26JUL84 08.53.47 - VOL=SACC09, DSN=Z8SAC.SMOO.CNTL

MEMBER=SMOOTH

C

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DO 810 I = 1,NPTS
  K = I-1
  J = MOD(K,5) + 1
  CTS(J) = S(I)
  IF (S(I) .LE. .00001) GO TO 800
  CTL(J) = ALOG(S(I))
  Y(J) = A + B * (H(I) - HBASE)
  DF(J) = CTL(J) - Y(J)
  GO TO 805
800 CTL(J) = 0.0
  Y(J) = 0.0
  DF(J) = 0.0
805 IF (J.NE.5) GO TO 810
  WRITE (6,2810) (CTS(K),CTL(K),Y(K),DF(K),K=1,5)
2810 FORMAT (1X,5(F7.1,F6.1,F6.1,F6.2))
810 CONTINUE
  RETURN
END
```

*** END OF MEMBER *** 798 RECORDS PROCESSED

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SUBROUTINE ALFEFF(IF,ALT,SLTOZ,SLTAR,ALPHA,BETAF,NCODE,IMES,ITBL)00000010
C REED, BATLUCK, ZANNER, COOKE      JUN 1983  FORTRAN-IV IBM 360/370 00000020
C ALFEFF COMPUTES THE EFFECTIVE OZONE ABSORPTION AND SCATTERING COEFFI- 00000030
C CIENTS FOR A FILTER, ADJUSTING FOR OZONE AND AIR OVERBURDENS AND AIR 00000040
C TEMPERATURE. AEROSOL SCATTERING IS IGNORED. METHOD IS DERIVED FROM 00000050
C THAT USED BY MCBRIDE AT NAVAL WEAPONS CENTER, CHINA LAKE, CA. 00000060
C 00000070
C 00000080
C 00000090
C 00000100
C 00000110
C 00000120
C 00000130
C 00000140
C 00000150
C 00000160
C 00000162
C 00000164
C 00000166
C 00000170
C 00000180
C 00000190
C 00000200
C 00000210
C 00000220
C 00000230
C 00000240
C 00000250
C 00000252
C 00000260
C 00000270
C 00000280
C 00000290
C 00000310
C 00000320
C 00000330
C 00000360
C 00000370
C 00000380
C 00000382
C 00000384
C 00000390
C 00000392
C 00000400
C 00000401
C 00000402
C 00000404
C 00000406
C 00000410
C 00000420
C 00000430
C 00000440
C 00000450
C 00000460
C 00000470
C 00000480

C ARGUMENTS:
C IF = FILTER NUMBER: 1-7 CORRESPONDING TO S3,S2,S1,S0,S3,S2,S1
C ALT = ALTITUDE - TO BE USED TO ACCESS AIR TEMP PROFILE IN SONDE.
C SLTOZ = OZONE SLANT OVERBURDEN (ATM-CM)
C SLTAR = AIR MASS - SLANT PATH (ATM)
C ALPHA = EFFECTIVE OZONE ABSORPTION COEFFICIENT
C BETAF = EFFECTIVE COEFFICIENT FOR RAYLEIGH SCATTERING
C NCODE = -16 NO AIR TEMP FOR THIS ALT.
C " = -17 FILTER WAVELENGTH NOT IN 2401-3400A
C " = -18,-19 FILTER TRANS .LE. 0.

C OTHER SIGNIFICANT VARIABLES
C GAMM(1000) PRODUCT OF SOLAR FLUX, DIFFUSER TRANSMISSION, AND
C DETECTOR RESPONSIVITY. 240.1 TO 340.0 NM
C BETA(1000) RAYLEIGH SCATTERING COEFFICIENT
C ABSZ(1000) OZONE ABSORPTION COEFFICIENT, NEAR ROOM TEMPERATURE
C ABST(800.2) OZONE ABS. COEFF. AT TWO LOWER TEMP. 260.1-340.0 NM.
C TEMPK(3) TEMPERATURES FOR ABSZ AND ABST
C FILTER(1000) FILTER TRANSMISSION AS A FUNCTION OF WAVELENGTH

C DIMENSION TEMPK(3), STR(1000,3), FILTER(1000)
C COMMON/COEFTS/GAMM(1000),BETA(1000),ABSZ(1000),ABST(800.2)
C COMMON/PROFLS/DSB(3),MXSND,NECC(2),ECCLM(3,2),SONDE(5,70),
C X ECC(4,19,2),STD(3,60)
C COMMON/FSHAPE/CH(7),BH(7),CMCBRD(4,7)
C EQUIVALENCE (GAMM(1),STR(1,1))
C DATA INIT/0/,LSTNF/0/,

C RATINGA = 0.0
C RATINGB = 0.0
C NCODE = 0
C NF = IF
C IF (INIT .EQ. 1) GO TO 100
C ALPHAG = 0.0
C CALL INARRY(NCODE,TEMPK,IMES)
C CALL PRTPED(IMES)
C CALL TAPMRT(1,IMES)
C IF (NCODE .LT. 0) GO TO 999
C INIT = 1
C C INITIALIZATION OF ARRAYS IS COMPLETE.
C C INITIALIZE FOR THE FIRST ENTRY FOR EACH FILTER
C 100 IF (NF.EQ.LSTNF) GO TO 140
C LSTNF = NF
C C FILTER SHAPE : GAUSSIAN OR MEASURED?

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A0 = CMCRD(1,IF)
IF (A0 .NE. 0.) GO TO 130
IF (IF.GT.4) GO TO 950
C READ MEASURED SHAPE - WRITE WHEN DETAILS OF HFF ARRAY ARE AVAILABLE.
CALL SHAPE(NF,FILTER,LMA,LMB,IMES,NCODE)
IF (NCODE.NE.0) GO TO 999
GO TO 150
C OR ASSUME GAUSSIAN SHAPE BASED ON CENTER WAVELENGTH AND BANDWIDTH.
130 IF (IF.GT.4) GO TO 140
IF (CH(NF) .GT. 1000.) GO TO 131
C CONVERT MM TO A
CH(NF) = CH(NF) * 10.
BH(NF) = BH(NF) * 10.
131 SIGMA = BH(NF)/2.355
FSIGMA = 5. * SIGMA
C COMPUTE ARRAY INDEXES CORRESPONDING TO WAVELENGTHS IN FILTER
LC = (CH(NF)-2481.)
IF (LC.LT.1 .OR. LC.GT.1000) GO TO 930
LMA = LC - FSIGMA
LMB = LC + FSIGMA
IF (LMA.LT.1) LMA = 1

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IF (LMB.GT.1000) LMB = 1000
C CALCULATE SHAPE
C
DO 135 I = LMA,LMB
  WL = LC - I
  FILTER(I) = EXP(-(WL*WL)/(2*SIGMA*SIGMA))
135 CONTINUE
C WRITE (IMES,2135) LMA,LC,LMB,(I,FILTER(I),I=LMA,LMB)
2135 FORMAT (1X,'ALFEFF 2135: LMA,LC,LMB = ',3I4,'/1X,13(I4,F6.3))
C
C HEIGHT FILTER SHAPE WITH GAMM
150 DO 155 I = LMA,LMB
155 FILTER(I) = GAMM(I)
C
C USE MCBRIDE COEFFICIENTS
140 IF (A0.EQ.0.) GO TO 200
  ALPHFM = CMCBRD(1,IF) + (CMCBRD(2,IF) * SLTOZ) +
    X (CMCBRD(3,IF) * SLTOZ*SLTOZ)
  BETAFM = CMCBRD(4,IF)
C WRITE (IMES,2140) ALPHFM,BETAFM,IF
2140 FORMAT('0ALFEFF 2140: MCBRIDES EFFECTIVE ALPHA AND BETA = ',
  X 2F10.6,' IF = ',I2)
  GO TO 850
C
C COMPUTE AVERAGE TEMPERATURE WEIGHTED FOR DENSITY
C FROM SONDE PROFILE:
200 ALTM = ALT + 10.
  SUMA = 0.
  SUMB = 0.
C LOOK IN SONDE
DO 220 I = 1, MXSND
  T = SONDE(1,I)
  IF (T.GT. ALTM) GO TO 220
  SUMA = SUMA + (SONDE(4,I) * SONDE(2,I))
  SUMB = SUMB + SONDE(4,I)
  IF (T.LE.ALT) GO TO 250
220 CONTINUE
C LOOK IN ECC PROFILE FOR TEMPERATURE DOWN TO ALT
DO 240 J = 1,2
  L = MECC(J)
  DO 235 I = 1,L
    T = ECC(1,I,J)
    IF (T.GT. ALTM) GO TO 235
    IF (T.LT. ALT) GO TO 235
  C DENSITY IS PROPORTIONAL TO PRESS/TEMP
    SUMA = SUMA + ECC(3,I,J)
    SUMB = SUMB + ECC(3,I,J)/ECC(2,I,J)
  235 CONTINUE
240 CONTINUE
250 IF (SUMB.LE. 0.) GO TO 925
  TMT = SUMA/SUMB
C *** TEST STATEMENT
C WRITE(IMES,2250) SUMA,SUMB,TMT
2250 FORMAT(1X,'ALFEFF 2250: SUMA = ',G12.6,2X,
  X 'TMT = ',G12.6)
C
C CALCULATE EFFECTIVE ABSORPTION COEFF FOR THE WEIGHTED TEMPERATURE.

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SUMA = 0.
SUMB = 0.
SUMC = 0.
IF (TMT .LT. TEMPK(2)) GO TO 263
ITA = 1
ITB = 2
GO TO 265
263 ITA = 2
    ITB = 3
    FRAC1 = (TMT-TEMPK(2))/(TEMPK(1)-TEMPK(2))
    265 FRAC2 = (TMT - TEMPK(3))/(TEMPK(2) - TEMPK(3))
    C USE LIMITING FORMULA FOR ZERO OPTICAL DEPTHS.
    DO 280 I = LMA, LMB
        T = FILTER(I)
        IF (T .LE. 0.) GO TO 278
        SUMB = SUMB + T
        SUMC = SUMC + T * BETA(I)
        K = I - 200
        IF (I.GT.200 .AND. ABST(K,1).GT.0.) GO TO 270
    C INDEPENDENT OF TEMPERATURE
    SUMA = SUMA + T * ABSZ(I)

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      GO TO 278
C DEPENDENT ON TEMP.
270 IF (ITA.EQ.2 .AND. ABST(K,2) NE.0.) GO TO 275
      SUMA = SUMA + T * (ABST(K,1) + FRAC1 * (ABSZ(I)-ABST(K,1)))
      GO TO 278
275 SUMA = SUMA + T * (ABST(K,2) + FRAC2 * (ABST(K,1)-ABST(K,2)))
278 CONTINUE
C *** TEST STATEMENT
C IF (I.EQ.LC) WRITE(IMES,2278) SUMA,SUMB,FRAC1,FRAC2,I,
C X K,ABSZ(I),ABST(K,1),ABST(K,2)
2278 FORMAT(1X,'ALFEFF 2278: SUMA =',G12.6,2X,'SUMB =',G12.6,2X,
C X 'FRAC1 =',G12.6,2X,'FRAC2 =',G12.6,2X,'I,K =',215,/,
C X 14X,'ABSZ(I) =',G12.6,2X,'ABST(K,1) =',G12.6,2X,'ABST(K,2) =',
C X G12.6)
280 CONTINUE
      IF (SUMB .LE. 0.) GO TO 935
      ALPHAF = SUMA/SUMB
      BETAF = SUMC/SUMB
      FLUXIN = SUMB
      ATAU = 0.0
C
C WRITE (IMES,2280) NF,A0,ALPHAF,CMCBRD(4,IF),BETAF,FLUXIN
2280 FORMAT ('ALFEFF 2280: FILTER',I3,'; MCBRIDE A0=',F9.4,' GAUSSIAN
C X ',F9.4,' MCBETA =',F9.5,' GAUSS BETA =',
C X F9.5,'/11X,FLUXIN =',F9.5)
300 IF (SLTOZ .LT. 1.E-5 .AND. SLTAR .LT. 1.E-2) GO TO 850
C CALCULATE SUMS FOR ALPHAF FOR GIVEN SLANT BURDENS
C
302 SUMA = 0.
      SUMB = 0.
      DO 320 I = LMA,LMB
        T = FILTER(I)
        IF (T .LE. 0.) GO TO 320
        B = BETAF(I) * SLTAR
        Z = ABSZ(I) * SLTOZ
        IF (ABS(Z+B) .GT. 174.) GO TO 320
        K = I - 200
        IF (I.LT.201 .OR. ABST(K,1) .LE. 0.) GO TO 310
C DEPTD ON TEMPERATURE, I.E. LONGER THAN ABOUT 260.0 MM.
        IF (ITA.EQ.2 .AND. ABST(K,2) .GT. 0.) GO TO 305
        Z = SLTOZ * (ABST(K,1) + FRAC1 * (ABSZ(I)-ABST(K,1)))
        GO TO 310
305 Z = SLTOZ * (ABST(K,2) + FRAC2 * (ABST(K,1)-ABST(K,2)))
310 SUMA = SUMA + T * EXP(-Z-B)
        SUMB = SUMB + T * EXP(-B)
      320 CONTINUE
C
C ALPHA EFFECTIVE AND BETAF
C
      IF (SUMA .LE. 0.) GO TO 940
      ATAU = ALOG(SUMB/SUMA)
      ALPHFG = ATAU/SLTOZ
      TAU = ALOG(FLUXIN/SUMA)
      BTAU = TAU - ATAU
      BETAFG= BTAU/SLTAR
C *** TEST STATEMENT

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C      WRITE (IMES,2320) SUMA,SUMB,ATAU,TAU,BTAU,BETAFO
2320 FORMAT(1X,'ALFFFF 2320: SUMA =',G11.5,2X,'SUMB =',G11.5,2X,
X 'ATAU =',G11.5,2X,'TAU =',2X,G11.5,2X,'BTAU =',G11.5,2X,
X 'BETAFO =',G11.5)
C
C CHOOSE COEFF. BASED ON MCBRIDE, GAUSSIAN, OR MEASURED SHAPE.
C
C SELECT ALPHAF AND BETAF
850 AOMG = 0.0
    AFMG = 0.0
    BMG = 0.0
    IF (A0.EQ. 0.) GO TO 860
C USE MCBRIDE VALUES
    ALPHAF = ALPHFM
    BETAF = BETAFM
    IF (ALPHAG.LE. 0.) GO TO 990
    AOMG = A0/ALPHAG
    BMG = BETAFM/BETAG
    IF (ATAU.NE.0.) AFMG = ALPHFM/ALPHAG
    GO TO 990
C USE VALUES FROM MEASURED FILTER SHAPE

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860 IF (ATAU.NE.0.0) GO TO 865
  ALPHAF = ALPHAG
  BETAF = 1.9
  GO TO 990
865 ALPHAF = ALPHFG
  BETAF = BETAFG
  GO TO 990
C
C ODDS AND ENDS
C
C IN WEIGHTED AVE OF TEMPERATURE, NO DATA FOUND
925 WRITE (IMES,2925) ALT
2925 FORMAT ('0ALFEFF 2925: NO TEMPERATURE AVAILABLE FOR ALT=',F9.2)
  MCODE = -16
  GO TO 999
C FILTER RANGE OUTSIDE OF AVAILABLE ARRAYS
930 WRITE (IMES,2930) CH(NF)
2930 FORMAT ('0ALFEFF 2930: CENTER WAVELENGTH',F7.1,' IS NOT BETWEEN '
  X'240.1 AND 340.0 NM')
  MCODE = -17
  GO TO 999
C
C SUMB LE 0, TEMP DEPT CALC.
935 WRITE (IMES,2935) SUMB
2935 FORMAT ('0ALFEFF 2935: IN TEMPR. DEPT. CALC. OF ALPHA-EFF,'
  X' SUMB =',E10.2)
  MCODE = -18
  GO TO 999
C
C SUMA LE ZERO
940 WRITE (IMES,2940) SUMA
2940 FORMAT ('0ALFEFF 2940: IN COMP OF ALPHAF , SUMA =',E10.2)
  MCODE = -19
  GO TO 999
C RATIOS REQUESTED, BUT MCDRIDE A0 = 0
950 WRITE (IMES,2950) IF,A0
2950 FORMAT(IX,'ALFEFF 2950: RATIOS REQUESTED (IF=',I2,') BUT A0=',
  X'E9.2)
  MCODE = -20
  GO TO 999
C
C NORMAL END
990 MCODE = 0
999 CONTINUE
C *** TEST STATEMENT
C *** WRITE(IMES,2999) TMT,IF,ALT,SLTOZ,SLTAR,ALPHAF,BETAF,A0MG,AFMG,BMG
2999 FORMAT(IX,'ALFEFF 2999: TMT=',F6.2,' F8=',I2,' ALT=',F3.0,
  X' SLTOZ=',F8.5,' SLTAR=',F8.5,' ALPHAF=',F9.5,' BETAF=',F6.4,
  X' A0MG=',F6.4,' AFMG=',F6.4,' BMG=',F5.3)
  RETURN
  END

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*** END OF MEMBER *** 284 RECORDS PROCESSED *****

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C SETUP INFORMATION: FLIGHT NUMBER, TAPE IN & OUT, FILTER CAL DATE,
C MANUFACTURER, DAY AND YEAR OF ASSEMBLY(1), FUTURE I.D.
  NCRD=1
  READ(5,1005,END=980,ERR=990)FLT(1),TAPEIN,NFIN,TAPOUT,NFOT,MDY,
  X MFG,ICAL,ICLID
  1005 FORMAT (1X,F6.1,2X,A8,I3.4X,A8,I3.4X,3(I2,1X),A4,1X,I5,1X,I6)
  WRITE(IECHO,1005) FLT(1),TAPEIN,NFIN,TAPOUT,NFOT,MDY,MFG,ICAL,
  X ICLID
C START PEDIGREE RECORDS
  PED(1,5) = -500.
  PED(2,5) = FLT(1)
  CALL RPDAT0 (1,IYMD)
  PED(3,5) = IYMD(1) + 100.*IYMD(3) + 10000.*IYMD(2)
  PED(5,5) = MFG
  PED(6,5) = ICAL
  PED(7,5) = ICLID
  PED(8,5) = MDY(3) + 100.*MDY(2) + 10000.*MDY(1)
C FILTER CALIBRATION DATA: OPTION; S3.SHORTEST WAVELENGTH FIRST; NM
  WRITE (IECHO,2030)
  2030 FORMAT ('00PT TOP BASE CTR NM BW NM A0',10X,'A1',11X,'A2',6X,00000570
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SUBROUTINE CARDS (NCODE,IMES,IECHO)

REED/BATLUCK/COOKE FEB 1983

CARDS READS FROM DATAS TO OBTAIN INPUT AND OUTPUT DATA LOCATIONS,
FILTER CALIBRATIONS, AND DATA FROM DOBSONS, DATASONDE AND ECC.
PROVISION IS MADE FOR TWO ECC SONDES.

INCLD(1) = 3,2,1,0,30,20,10 PROCESS THIS FILTER
= ANY NEGATIVE NUMBER OMIT
TOP(1) = HIGHEST ALTITUDE TO BE PROCESSED FOR THIS FILTER - KM
BASE(1) = LOWEST ALTITUDE TO BE PROCESSED FOR THIS FILTER - KM

NCODE = 1 NO PROBLEMS
= -1 UNEXPECTED EOF
= -2 READ ERROR
= -3 DATASONDE IS NOT DESCENDING, AS EXPECTED.
= -4 ECC IS NOT ASCENDING, AS EXPECTED.

SONDE(1,) = ALTITUDE (KM), STARTING AT TOP, FOR DATASONDE, EVERY KM
(2,) = TEMPERATURE (KELVIN)
(3,) = AIR PRESSURE (MBAR), COMPUTED HYPSONOMETRICALLY.
(4,) = AIR DENSITY (KG/M3), COMPUTED FROM P AND T.
(5,) = ERROR (ONE SIGMA) IN AIR TEMPERATURE - KELVIN

DSB(1) = BASE ALTITUDE (KM) FOR USE WITH DATASONDE
DSB(2) = AIR TEMPERATURE (K) AT BASE ALT
DSB(3) = AIR PRESSURE (MBAR) AT BASE ALT

ECC(1,) = ALTITUDE (KM) FOR ECC SONDE, AT STD PRESSURE LEVELS
(2,) = TEMPERATURE (KELVIN)
(3,) = AIR PRESSURE (MBAR), STARTING AT ABOUT 1000 MBAR
(4,) = OZONE PARTIAL PRESSURE (NANOBAR)

ECCLM(1) = OZONE COLUMN (ATM-CM) AT 250 MBAR AIR PRESSURE
ECCLM(2) = " " " 125 " " "
ECCLM(3) = " " " 62.5 " " "

STD(1,) = ALTITUDE (KM) MODEL, TO BE FILLED BY SUBROUTINE MODEL
(2,) = OZONE NUMBER DENSITY (MOLECULES/M3)
(3,) = OZONE OVERBURDEN (ATM-CM)

CMCBRD(1,) = A0, AS GIVEN BY NMC, CHINA LAKE MEAS. AND COMPUTATIONS.
(2,) = A1
(3,) = A2
(4,) = BETA

REAL*8 TAPEIN,TAPOUT, FLTID
DIMENSION IYMD(3), MDY(3), FLT(2)
COMMON/SETUP/ TAPEIN,TAPOUT, NFIN, NFOT, INCLD(7),TOP(7),BASE(7)
COMMON/PROFL/ DSB(3),MXSND, NECC(2),ECCLM(3,2),
X SONDE(5,70),ECC(4,19,2),STD(3,60)
COMMON/FSHAPE/ CM(7),BM(7),CMCBRD(4,7)
COMMON/DATOUT/ NSAV, PED(20,30), SAVE(20,60)
EQUIVALENCE (FLTID,FLT(1))

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X'BETA')
DO 30 I=1,7
NCRD=NCRD+1
READ (5,1040,END=980,ERR=990)INCLD(I),TOP(I),BASE(I),CH(I),BH(I),
X (CMCBRD(J,I),J=1,4)
1040 FORMAT (2X,I2,2F5.1,2X,F6.2,1X,F5.2,2X,F8.4,F12.5,F13.5,1X,F7.5)
C BE SURE CH & BH ARE IN NM
IF (CH(I) .LT. 1000.) GO TO 28
CH(I) = CH(I) / 10.
BH(I) = BH(I) / 10.
28 WRITE (6,1040) INCLD(I),TOP(I),BASE(I),CH(I),BH(I),
X (CMCBRD(J,I),J=1,4)
C WRITE(IMES,2150) NCRD
30 CONTINUE
DO 40 I=1,2
IS=(I-1)*6
PED((9+IS),5) = CH(I)
PED((10+IS),5) = BH(I)
DO 40 J=1,4
PED((10+J+IS),5) = CMCBRD(J,I)
40 CONTINUE
DO 45 I=3,4
IS=(I-3)*6
PED((9+IS),6) = CH(I)
PED((10+IS),6) = BH(I)
DO 45 J=1,4
PED((10+J+IS),6) = CMCBRD(J,I)
45 CONTINUE
PED(1,6) = -501.
NCRD = NCRD+1

C READ DOBSON DATA: DATE, AM, PM,IN DOBSON UNITS
READ(5,1050,END=980,ERR=990) MDY,PED(3,6),PED(4,6)
1050 FORMAT (2X,I2,1X,I2,1X,I2,2X,F5.1,2X,F5.1)
WRITE (IECHO,2050)
2050 FORMAT ('0 DATE AM PM DOBSON UNITS')
WRITE (IECHO,1050) MDY, PED(3,6), PED(4,6)
C WRITE(IMES,2150) NCRD
PED(2,6) = MDY(3) + 100.*MDY(2) + 1000.*MDY(1)

C READ DATASONDE FOR TEMP VS ALT.; BASE PRES & ALT FROM ECC SONDE OR STD00000900
C FLIGHT ID, DATE, TIME, BASE ALT & PRES.; MAX ALTITUDE FIRST.
NCRD=NCRD+1
READ (5,1060,END=980,ERR=990) FLTID, MDY, IH, IM, MDEL, DSB
1060 FORMAT (2X,A8,2X,I2,1X,I2,1X,I2,2X,I2,2X,I3,2X,F7.1,2X,F6.2,2X,
X F6.2)
IF (DSB(1).GT.1000.) DSB(1) = DSB(1)/1000.
IF (DSB(2).LT.100.) DSB(2) = DSB(2) + 273.15
WRITE (IECHO,2060)
2060 FORMAT ('0 FLT ID MM/DD/YY HHMM DMN BALT BTMP BMBAR',
X DATASONDE')
WRITE (IECHO,1060) FLTID, MDY, IH, IM, MDEL, DSB
C WRITE(IMES,2150) NCRD
IF (DSB(1) .GT. 1000.) DSB(1) = DSB(1)/1000.
DO 70 I=1,70
NCRD=NCRD+1
READ (5,1070,END=980,ERR=990) ALT, TEMP, TERR

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IF (ALT .LE. 0.) GO TO 75
MXSND = I
IF (ALT .GT. 1000.) ALT = ALT/1000.
SONDE(1,1) = ALT
IF (TEMP .LT. 100.) TEMP = TEMP + 273.15
SONDE(2,1) = TEMP
C OBTAIN ONE SIGMA ERROR; ADD ERROR DUE ATMOSPHERIC VARIABILITY
C (MINUTES BETWEEN DATASONDE AND ROCOZ).
IF (MDEL.GT.100) MDEL = 100
B = 0.32
IF (SONDE(1,1) .LT. 52.5) B = 0.19
SONDE(5,1) = SQRT(0.5*TEMP*TERR + B*MDEL)
70 CONTINUE
75 IF (SONDE(1,1) .LT. SONDE(1,MXSND)) GO TO 970
1070 FORMAT (2X,F6.0,2X,F6.2,2X,F4.1)
C PRESSURES AND DENSITIES ARE COMPUTED IN DATSND, AFTER LAUNCH LAT IS
C READ IN FROM THE PEDIGREE RECORDS.
PED(1,7) = -502
PED(2,7) = SONDE(1,1)
PED(3,7) = SONDE(1,MXSND)
PED(4,7) = MXSND

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PED(5,7) = FLT(1)
PED(6,7) = FLT(2)
PED(7,7) = MDY(3) + 100.*MDY(2) + 10000.*MDY(1)
PED(8,7) = 100.*IM + IM
PED(9,7) = DSB(1)
PED(10,7) = DSB(3)
C PED(11,7) AND (12,7) ARE FILLED AFTER VALUES ARE COMPUTED IN DATSND.
C
DO 76 I = 1,8
J = I + 12
76 PED(J,7) = SONDE(2,I)
C
DO 79 K = 8,10
PED(1,K) = -503.
DO 78 J = 2,20
I = 7 + J + 19*(K-8)
78 PED(J,K) = SONDE(2,I)
79 CONTINUE
PED(4,5) = 0.0
C
C READ ECC DATA
DO 200 J = 1,2
K = 15 + 5*(J-1)
NCRD = NCRD+1
READ (5,1080,END=990,ERR=990) FLTID,MDY,IM,IM,TIEALT,TIECOL
1080 FORMAT(2X,A8,2X,I2,1X,I2,2X,I2,1X,I2,2X,F6.0,2X,F7.5)
C THE NEXT THREE PED RECORDS (11,12,13) ARE RESERVED FOR MID-LAT OZONE
C MODEL
IF (MDY(1).LE.0) GO TO 200
PED(1,K) = -506.
PED(2,K) = TIEALT
PED(3,K) = TIECOL
PED(5,K) = FLT(1)
PED(6,K) = FLT(2)
PED(7,K) = MDY(3) + 100.*MDY(2) + 10000.*MDY(1)
PED(8,K) = 100.*IM + IM
WRITE (IECHO,2080)
2080 FORMAT ('0 FLT ID MM/DD/YY HHMM ALT ATM-CM ECC SONDE')
WRITE (IMES,2150) NCRD
C
PED(2,K) = PED(2,K)/1000.
NECC(J) = 0
DO 120 I = 1,19
READ (5,1120,END=125,ERR=990) KH,ECC(4,I,J),ECC(3,I,J),ECC(2,I,J)
1120 FORMAT (2X,15,2X,F5.1,2X,F6.1,2X,F5.1)
IF (ECC(4,I,J).LE.0.) GO TO 120
NECC(J) = NECC(J) + 1
IF (ECC(2,I,J).LT.100.) ECC(2,I,J) = ECC(2,I,J) + 273.15
ECC(1,I,J) = KH/1000.
120 CONTINUE
125 IF (ECC(1,NECC(J)),J) .LT. ECC(1,1,J)) GO TO 960
PED(4,5) = PED(4,5) + 1
PED(4,K) = NECC(J)
C PUT ECC DATA IN PED RECORDS 15 - 18 AND 19 - 22
CALL CMOVE(ECC(1,1,J),PED(9,K),48)
DO 160 L = 1,4
K = K + 1

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PED(1,K) = -507.
PED(2,K) = J
PED(3,K) = FLT(1)
PED(4,K) = FLT(2)
LT = 4 * L
160 CALL CMOVE(ECC(1,LT,J),PED(5,K),64)
    IF (J.EQ.2) GO TO 200
205 READ (5,1205) (ECCLM(I,J),I=1,3)
1205 FORMAT (3(6X,F7.5))
200 CONTINUE
NSAV = 24
NCRD = NCRD + NECC(1) + NECC(2) + 1
WRITE (IMES,2150) NCRD
2150 FORMAT ('0CARDS 2150: NUMBER OF DATA5 RECORDS READ IS',I5)
NCRD = 1
GO TO 999
C ODDS AND ENDS
C ECC ALT IS NOT ASCENDING AS EXPECTED
960 WRITE (IMES,2960)
2960 FORMAT ('0CARDS 2960: ECC ALTITUDES SHOULD BE INCREASING')
NCRD = -4

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00001452
00001460
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00001480
00001490
00001500
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26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=CARDS

```
GO TO 999
C DATASOPE ALTITUDE IS NOT DESCENDING, AS EXPECTED.
970 WRITE (IMES,2970)
2970 FORMAT ('OCARDS 2970: DATASOPE ALTITUDES SHOULD BE DECREASING')
NCODE = -3
GO TO 999
C UNEXPECTED EOF
980 WRITE (IMES,2980) NCRD
2980 FORMAT ('CARDS 2980: UNEXPECTED EOF ON DATAS. RECORD NO',I4)
NCODE = -1
GO TO 999
C READ ERROR
990 WRITE (IMES,2990) NCRD
2990 FORMAT ('CARDS 2990: READ ERROR ON DATAS RECORD NO',I4)
NCODE = -2
999 RETURN
END
```

00001560
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00001600
00001610
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*** END OF MEMBER *** 252 RECORDS PROCESSED *****

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```

SUBROUTINE CFTWRT(TEMPK,IRNG,IMES)
      COOKE          JULY 1983
      C
      C CFTWRT PRINTS OUT THE VALUES FOR TEMPK AND IRNG AS WELL AS THE
      C VALUES OF THE CONTENTS OF COMMON/COEFTS (ARRAYS GAMM,BETA,ABSZ,
      C AND ABST).
      C
      DIMENSION IRNG(2,7),TEMPK(3)
      COMMON/COEFTS/GAMM(1000),BETA(1000),ABSZ(1000),ABST(800,2)
      C
      C PRINT OUT TEMPK AND IRNG
      WRITE(IMES,2020) TEMPK
      WRITE(IMES,2030) ((IRNG(I,J),J=1,7),I=1,2)
      C
      C PRINT OUT GAMM ARRAY
      WRITE(IMES,2040)
      WRITE(IMES,2000) (L,L=1,10)
      J = 0
      K = 0
      DO 100 M = 1,100
        WRITE(IMES,2080) J,(GAMM(I+K),I=1,10)
        K = K + 10
        J = J + 1
      100 CONTINUE
      C
      C PRINT OUT BETA ARRAY
      WRITE(IMES,2050)
      WRITE(IMES,2000) (L,L=1,10)
      J = 0
      K = 0
      DO 200 M = 1,100
        WRITE(IMES,2080) J,(BETA(I+K),I=1,10)
        K = K + 10
        J = J + 1
      200 CONTINUE
      C
      C PRINT OUT ABSZ ARRAY
      WRITE(IMES,2060)
      WRITE(IMES,2000) (L,L=1,10)
      J = 0
      K = 0
      DO 300 M = 1,100
        WRITE(IMES,2080) J,(ABSZ(I+K),I=1,10)
        K = K + 10
        J = J + 1
      300 CONTINUE
      C
      C PRINT OUT ABST ARRAY
      WRITE(IMES,2100)
      L = 1
      N = 2
      WRITE(IMES,2110) L,N,L,N,L,N,L,N
      DO 400 K = 1,100
        K1 = K + 100

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OF POOR QUALITY

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K2 = K + 200
K3 = K + 300
WRITE(UNIT,2150) K,(ABST(K,I),I=1,2),K1,(ABST(K1,I),I=1,2),
X K2,(ABST(K2,I),I=1,2),K3,(ABST(K3,I),I=1,2)
400 CONTINUE
WRITE(UNIT,2110) L,N,L,N,L,N,L,N
DO 500 K = 1,100
K4 = K + 400
K5 = K + 500
K6 = K + 600
K7 = K + 700
WRITE(UNIT,2150) K4,(ABST(K4,I),I=1,2),K5,
X (ABST(K5,I),I=1,2),K6,(ABST(K6,I),I=1,2),K7,
X (ABST(K7,I),I=1,2)
500 CONTINUE
C
2000 FORMAT(/,2X,10(1X,I2),/)
2020 FORMAT(1X,' TEMPK = ',3G12.3)
2030 FORMAT(/,1X,' IRNG = ',/,2(1X,7I7,/))
2040 FORMAT(/,1X,' GAMM = ')
2050 FORMAT(/,1X,' BETA = ')

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00300560
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00000650

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=CFTMRT

2060 FORMAT(//,1X,' ABSZ =')
2080 FORMAT(1X,12,5X,10(G10.3,2X))
2100 FORMAT(//,1X,' ABST =')
2110 FORMAT(//,13X,3(11,11X,11,18X),11,11X,11)
2150 FORMAT(3X,4(13,2X,G10.3,2X,G10.3,4X))

C
RETURN
END

00000660
00000670
00000680
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00000700
00000710
00000720
00000730

*** END OF MEMBER *** 85 RECORDS PROCESSED

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SUBROUTINE CHECKS(NCODE,IMES,ICLK)

```

C REED, BATLUCK, COOKE
C
C CHECKS EVALUATES THE SET OF OBSERVATIONS AS FOLLOWS:
C 1. CONSISTENCY AMONG THE FILTERS AND FILTER-RATIOS.
C 2. COMPUTE OVERBURDEN AS A FUNCTION OF ALTITUDE.
C 3. COMPARE DENSITIES WITH MODEL USED IN THIS PROGRAM.
C 4. COMPARE ROCOZ + ECC COLUMN WITH DOBSON DATA.
C 5. ADD AIR T AND P TO COMPOSITE PROFILE
C 6. COMPARE VARIOUS ESTIMATES OF RATE OF CHANGE OF LM I.
C 7. LOOK AT VARIATION OF COMP CHANNELS VS THAT EXPECTED DUE TO SZA AND
C SCATTERING.
C 8. LOOK AT CONSTANCY OF APPARENT DRAG CROSS SECTION.
C
C ARGUMENTS
C NCODE = 0 NORMAL RETURN
C
C IMES = PRINTER UNIT FOR PROBLEM MESSAGES
C ICLK = PRINTER UNIT FOR COMPUTATIONAL RESULTS
C
C ARRANGEMENT OF DATA IN WORK: INITIALLY, WORDS 1-20 ARE FILLED IN
C COMPT. BEFORE RETURNING, THE CONTENTS BECOME:
C 1 NO OF VALUES/ 300. TO 0.
C 2 ALTITUDE - KM, 70. TO 0.
C 3 OZONE DENSITY - ATM-CM/KM
C 4 OZONE DENSITY NUMBER/M3
C 5 OZONE DENSITY ERROR X
C 6 OZONE VERTICAL COLUMN- ATM-CM
C 7 OZONE VERTICAL COLUMN- ERROR X
C 8 AIR TEMPERATURE-KELVIN
C 9 AIR TEMPERATURE X
C10 AIR PRESSURE MBAR
C
C ARRANGEMENT OF DATA IN TABLE:
C(1)OVERLAPS (3)COMP SITE-MDL (6)SLOPES (7)COMP-CH.
C 1 FILTER 1 1 ALTITUDE-KM 1 ALTITUDE KM 1A ALTITUDE 1B ALTITUDE
C 2 FILTER 2 2 CMP DENS/M3 2 D(LMI)/DH 2 OBS COMP 2 COS SZA
C 3 MAX ALT 3 CMP ERROR X 3 " NOISE 3 COS SZA 3 1- SLAT
C 4 MIN ALT 4 MDL DENS/M3 4 B 4 MDL DENS/M3 4 CORRECT
C 5 NUM PAIRS 5 CMP - MDL X 5 B STD DEV 5 5 PRED CM
C 6 A SIGMA A 6 CMP COL ATM-CM 6 DIFF RMS 6 OBS CM
C 7 B SIGMA B 7 CMP COL ATM-CM 7 ERR RMS 7 X DIFF
C 8 C SIGMA C 8 MDL COL 8 DIFF X 8
C 9 D SIGMA D 9 CMP-MDL ATM-CM 9 - 9
C10 R2 10 " 10 10
C
C(8)DRAG (TAB)
C 1 ALTITUDE
C 2 VELOCITY
C 3 ACCELER.
C 4 AIR DENS
C 5 APP DRAG C

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REAL*8 X2

ORIGINAL FILE
OF POOR QUALITY

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00000730
00000740
00000750
00000760

C      DIMENSION TAB(6,60),HEADS(7)
C      COMMON/SETUP/DUM(4),INCLD(7),TOP(7),BASE(7)
COMMON/PROFLS/DSB(3),HXSND,NECC(2),ECCLM(3,2),SONDE(5,70),
X      ECC(4,19,2),STD(3,60)
C      COMMON/DATAIN/MLAYS,SECSZA(60),SAVE(20,60,7)
C      NOTE THAT ARRAYS IN DATOUT ARE REDEFINED.
COMMON/DATOUT/NSAV,NDXTOP,NDXBAS,MLVLS,DH(10),DOBTM,DOBAM,DOBPM,
X      PMDL(2),ECTIE,ECCOL,MORK(20,71),TABLE(10,36)
COMMON/CONSTT/AVOGAD,VOLSTP,RSTAR,DOTORD,GRV45,AIRM,GRV,RZRO

C      EQUIVALENCE (TAB(1,1),TABLE(1,1))
DATA HEADS/' S3 ',' S2 ',' S1 ',' S0 ',' S3/0 ',' S2/0 ',' S1/0 '/

C      NCODE = 0
C(1) CHECK CONSISTENCY IN THE OVERLAP REGIONS.
CALL OVERLP(IMES,ICNK)

C (2) COMPUTE OZONE COLUMN AND ERROR AT EACH LEVEL
C OBTAIN INITIAL OVERBURDEN FROM MODEL AND ADJUST TO COMPOSITE PROFILE.00000760

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OF POOR QUALITY

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ISTD = (71.1-WORK(2,NDXTOP))
WORK(6,NDXTOP) = STD(3,ISTD) * WORK(4,NDXTOP) / STD(2,ISTD)
C *** TEST STATEMENT
C X WRITE(INES,2010) ISTD,WORK(6,NDXTOP),STD(3,ISTD),WORK(4,NDXTOP),
C X STD(2,ISTD)
2010 FORMAT(IX,'CHECKS 2010: ISTD =',I4,' WORK(6,NDXTOP) =',G10.3,
X' STD(3,ISTD) =',G10.3,' WORK(4,NDXTOP) =',G10.3,' STD(2,ISTD) =',
X' G10.3)
C ASSUME INITIAL COLUMN ERROR IS DUE TO DENSITY ERROR PLUS 15% ERROR IN
C SCALE HEIGHT. AT LOWER LEVELS, ERROR IS DUE TO ERRORS IN DENSITIES.
WORK(7,NDXTOP) = Sqrt(WORK(5,NDXTOP)*WORK(5,NDXTOP)+225.)
IA = NDXTOP + 1
DO 50 I = 1A,NDXBAS
  A = 0.5 * WORK(3,I-1)
  B = 0.5 * WORK(3,I)
  WORK(6,I) = WORK(6,I-1) + A + B
  ERRTOP = WORK(7,I-1) * WORK(6,I-1)
  A = A * WORK(5,I-1)
  B = B * WORK(5,I)
  WORK(7,I) = Sqrt(ERRTOP*ERRTOP + AXA + B*B)/WORK(6,I)
50 CONTINUE
C (3) COMPARE COMPOSITE PROFILE TO MODEL.
WRITE (ICM,2050) PMDL(1),PMDL(2)
2050 FORMAT ('COMPARISON OF COMPOSITE PROFILE WITH ',2A4,' MODEL',
X'0 ALT-KM COMP 03 /M3 COMP ERR X MODEL 03 /M3 COMP-MODL X',
X' COMP COL ATM-CM COMP ERR X MODEL COL COMP-MODL ATM-CM
X' X',/)
C
DO 100 I = NDXTOP,NDXBAS
  TABLE(1,1) = WORK(2,I)
  TABLE(2,1) = WORK(4,I)
  TABLE(3,1) = WORK(5,I)
  TABLE(4,1) = STD (2,I)
  TABLE(5,1) = (TABLE(2,1)-TABLE(4,1)) * 100./TABLE(2,1)
  TABLE(6,1) = WORK(6,I)
  TABLE(7,1) = WORK(7,I)
  TABLE(8,1) = STD (3,I)
  TABLE(9,1) = WORK(6,I) - STD(3,I)
  TABLE(10,1) = 100. * TABLE(9,1)/TABLE(6,1)
  WRITE (ICM,2100) (TABLE(J,1),J=1,10)
  FORMAT (IX,F7.0,E13.4,F11.1,E13.4,F12.2,F17.7,F11.2,F15.7,F16.7,
2100 X F10.2)
  100 CONTINUE
C (4) COMPARE TOTAL COLUMN VALUES
C
IF (DOBAM .LE. 0) DOBAM = DOBPM
IF (DOBPM .LE. 0) DOBPM = DOBAM
NLV = (71. - ECTIE)
RCOL = WORK(6,NLV)
COL = RCOL + ECCOL
C ASSUME ERROR IN ECC COLUMN VALUE IS 10% , IN DOBSON, 7%,
C CONVERT DOBSON MILLI ATM-CM TO ATM-CM
DBAVE = 5.0E-4 * (DOBAM+DOBPM)
ERDOB = 0.07 * DBAVE
ERROC = WORK(6,NLV) * WORK(7,NLV) * 0.01

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ERECC = 0.1 * ECCOL
ERCOL = SORT(ERROCHERROC + ERECCHERECC)
DIF = COL - DBAVE
DFERR = SORT(ERCOL*ERCOL + ERDOB*ERDOB)
DIFPC = 200. * DIF/(DBAVE+COL)
WRITE(ICKK,2110) ECTIE, RCOL, ERROC, ECTIE, ECCOL, ERECC, COL,
X ERCOL, DBAVE, ERDOB, DIF, DFERR, DIFPC
2110 FORMAT(// 'COMPARE ROCOZ + ECC COLUMN CONTENT WITH DOBSON TOTAL'//,
X 20X, 'ATM-CM ERROR', ' ROCOZ ', F3.0, '+ KM', 3X, 2F9.5, ' ECC 0-',
X F3.0, ' KM', 4X, 2F9.5, ' TOTAL', 11X, 2F9.5, ' DOBSON', 10X, 2F9.5,
X ' ROCOZ+ECC-DOBSON', 2F9.5, ' OR', F7.2, ' PERCENT'//)
C (5) ADD AIR T AND P TO COMPOSITE PROFILE.
C COPY NEEDED DATA FROM SONDE AND ROCOZ PROFILES.
C
ALT = WORK(2,NDXTOP)
DO 118 I = 1, MXSND
  J = I-1
  IF (ALT .EQ. SONDE(1,I)) GO TO 120
118 CONTINUE
120 DO 130 I = NDXTOP, NDXBAS

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      J = J+1
      WORK(8,I) = SONDE(2,J)
      WORK(9,I) = 100.*SONDE(5,J)/SONDE(2,J)
      WORK(10,I) = SONDE(3,J)
      WORK(11,I) = 100./DSB(3) + WORK(9,I)
130  CONTINUE
C (6) COMPARE ESTIMATES OF RATE OF CHANGE OF LM I.
      WRITE(ICHK,2130)
2130 FORMAT('I')
C *****
C *** BECAUSE OF THE MALFUNCTIONING OF THE 0 FILTER FOR FLT 329,
C *** THE FOLLOWING 'DO 160' LOOP IS PERFORMED ONLY THREE TIMES.
C *** (FOR FILTERS 3,2,1) INSTEAD OF THE USUAL 7 TIMES.
C *****
      DO 160 I=1,3
      DO 160 I=1,7
C FIND LEVEL IN COMPOSITE (WORK) FOR SAVE(2,1,I)
      DO 135 L = NDXTOP,NDXBAS
      N = L
      IF (SAVE(2,1,I) .EQ. WORK(2,N)) GO TO 138
135  CONTINUE
138  NA = N
C MOVE DATA FOR I FILTER INTO WORK
      DO 145 J = 1,59,2
      WORK(12,N) = SAVE(18,J,I)
      WORK(13,N) = SAVE(19,J,I)
      WORK(14,N) = 0.0
      WORK(16,N) = SAVE(4,J+1,I)
      WORK(17,N) = SAVE(19,J+1,I)
      WORK(19,N) = SAVE(5,J+1,I)
      WORK(20,N) = SAVE(3,J,I)
      WORK(15,N) = SAVE(10,J,I)
      WORK(18,N) = SAVE(16,J,I)
      IF (SAVE(20,J+1,I) .LE. 0.) GO TO 150
      N = N+1
145  CONTINUE
150  NB = N
C *** TEST STATEMENT - DISPLAY FOR I FILTER
C 155 WRITE(IMES,2155) ((WORK(K,M),K=1,20),M=NA,NB)
2155 FORMAT('I',CHECKS 2155: COMPOSITE ARRAY')
      X = NO ALT ATTMCH /KM O3NUM/M3 ERX ATM-CM ERX ATMP ERX AMBAR',
      X , ERX BSMOOTH STD DEV 0 DLNIH HNMSS.S SECND NOSDIF SZA COMP',
      X(1X,F2.0,F4.0,1X,E8.3,1X,E8.3,F4.1,1X,F6.5,1X,F4.1,F5.0,F4.1,F6.2,
      X 1X,F4.1,1X,F6.5,2X,11,1X,F5.4,F9.1,F6.0,1X,F6.5,F5.1,F6.1))
      WRITE (IMES,2157) HEADS(1)
2157 FORMAT('I',COMPARISON OF D(LN I)/DH WITH B FROM SMOOTH FOR ',
      X'FILTER ',A4,' ALT-KM D(LN I)/DH NOISE B(SMOOTH) SDEV ',
      X'DIFFERENCE+,- ERROR DIFFX')
      M = 1
      DO 156 J = NA, NB
      TABLE(1,M) = WORK(2,J)
      TABLE(2,M) = WORK(15,J)
      TABLE(3,M) = WORK(18,J)
      TABLE(4,M) = WORK(12,J)
      TABLE(5,M) = WORK(13,J)
      TABLE(6,M) = TABLE(2,M)-TABLE(4,M)
      TABLE(7,M) = SQRT(TABLE(3,M)*TABLE(3,M)+TABLE(5,M)*TABLE(5,M))

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TABLE(8,M) = 200. * TABLE(6,M) / (TABLE(2,M)+TABLE(4,M))
M = M + 1
IF (M.GT. 36) GO TO 158
CONTINUE
156 J = M - 1
158 WRITE (IMES,2160) ((TABLE(L,M),L=1,8),M=1,J)
2160 FORMAT (1X,F6.0,F11.4,F7.4,F11.4,F7.4,F11.4,F7.4,F8.2)
160 CONTINUE
C (7) VARIATION OF COMPENSATION CHANNEL.
C 7-A DETERMINE EXPECTED VALUE OF COMP CHANNEL FOR SZA=0.
C TRY TO USE DATA BETWEEN 50 AND 35 KM.
IF (NDXTOP.GT. 36) GO TO 175
N = 0
NA = 0
X = 0.0
X2 = 0.0
J = 21
IF (J.LI.NDXTOP) J = NDXTOP
DO 170 I= J,36
N = N+1
TABLE(1,N) = WORK(2,I)

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00001802
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TABLE(2,N) = WORK(20,I)
IF (TABLE(2,N).GE.1015.) GO TO 170
TABLE(3,N) = COS(WORK(19,I)*DGTORD)
TABLE(4,N) = TABLE(2,N)/TABLE(3,N)
X2 = X2 + TABLE(4,N)*TABLE(4,N)
X = X + TABLE(4,N)
NA = NA + 1
170 CONTINUE
C OBTAIN AVERAGE AND STD. DEV.
AVEC = X/NA
STDV = DSORT((X2 - N*AVEC*AVEC)/(N-1)*N))
WRITE (ICLK,2170) AVEC,STDV, ((TABLE(I,J),I=1,4),J=1,N)
2170 FORMAT ('CHECKS 2170: ',
X' COMPENSATION CHANNEL FOR SZA=0, BASED ON DATA 50 - 35',
X' KM, IS, F8.1, '+', F7.1, ' COUNTS, '//, ALTITUDE OBS.COMP',
X' COS SZA COMP(SZA=0) //(1X,F8.0,F10.2,F9.5,F13.2))
GO TO 180
C SINCE DATA ABOVE 40 KM IS NOT AVAILABLE, CALC COMP(SZA=0) FROM TOP ALT
175 SECANT = 1./COS(WORK(19,NDXTOP)*DGTORD)
AVEC = WORK(20,NDXTOP)*SECANT/(1.-0.376*(SECANT**0.874))*10. **
X (WORK(2,NDXTOP)/16.))
WRITE (ICLK,2175) AVEC, WORK(2,NDXTOP)
2175 FORMAT ('CHECKS 2175: ',
X' COMPENSATION CHANNEL FOR SZA=0 IS, F7.0, ' COUNTS, ',
X' BASED ON DATA AT, F5.0, ' KM.')
C 7-B COMPARE OBS COMP VALUES WITH ESTIMATES BASED ON SZA AND SCATTER-
ING. THE R.FRASER FORMULA IS USED TO ESTIMATE SCATTERING.(THOMAS
ET.AL, APPL.OPT.,21,2436,JULY 1,1982)
180 IA = 31
N = 0
DO 190 I= NDXTOP,NDXBAS
N = N+1
TABLE(1,N) = WORK(2,I)
TABLE(2,N) = COS(WORK(19,I)*DGTORD)
TABLE(3,N) = (1. - 0.376 * ( 1./TABLE(2,N))*0.874)/10.**
X (TABLE(1,N)/16.)
TABLE(4,N) = TABLE(2,N) * (1.-TABLE(3,N))
TABLE(5,N) = TABLE(4,N) * AVEC
TABLE(6,N) = WORK(20,I)
TABLE(7,N) = 100. * (TABLE(5,N)-TABLE(6,N)) / TABLE(5,N)
190 WRITE (ICLK,2190) ((TABLE(I,J),I=1,7),J=1,N)
2190 FORMAT ('CHECKS 2190: ',
X' ALTITUDE COS SZA 1-SCATTRD CORR FACTR PRED COMP',
X' OBS COMP PR-OB/PR X'/(1X,F8.0,F9.3,F11.5,F12.4,F11.0,F10.0,
X F12.2))
C (8) LOOK AT CONSTANCY OF DRAG COEFFICIENT
= 2*DRAG / (DENSITY * VEL**2 * AREA)
C REYNOLDS NUMBER = VELOCITY * SIZE * DENSITY / DYNAMIC VISCOSITY
C DYNAMIC VISCOSITY
= (1.458E-6 * TEMP**1.5) / (TEMP + 110.4)
C U.S. STD ATMOSPHERES, 1976, P.19; STARUTE IS 7 FEET DIAMETER.
200 IA = NDXTOP + 1
IB = NDXBAS - 1
N = 0

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DIA = 7. * 0.3048
AREA = 3.14159 * DIA * DIA * DIA * 0.25
CON = 100. * AIRM/RSTAR
DO 205 I = 1A, 1B
  N = N+1
  TAB(1,N) = WORK(2,I)
  TAB(3,N) = WORK(17,I+1) - WORK(17,I-1)
  TAB(2,N) = 2000. / TAB(3,N)
  DVIS = (1.458E-6 * WORK(8,I) * 1.5) / (WORK(8,I) + 110.4)
  TAB(4,N) = WORK(10,I) * CON / WORK(8,I)
  TAB(6,N) = DIA * TAB(2,N) * TAB(4,N) / DVIS
205  IB = N-1
DO 210 I = 2, 1B
  TAB(3,I) = (TAB(2,I+1) - TAB(2,I-1)) / TAB(3,I)
  TAB(5,I) = 2. * (GRV + TAB(3,I)) / (TAB(4,I) * TAB(2,I) * TAB(2,I))
  X
  WRITE (ICLK,2210) ((TAB(I,J), I=1,6), J=2, 1B)
2210 FORMAT ('CHECKS 2210: ',
X' CHECK OF DRAG COEFFICIENT VS ALTITUDE',
X' ALTITUDE VELOCITY ACCELER AIR DENS DRAG C REYNOLDS',
X' NO. ' / (IX, F8.0, F10.2, F9.4, E11.3, F10.3, F12.0))

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00002464
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26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=CHECKS

C COMPLETE COMPOSITE TABLE IN WORK

COMP = 0.1 * RSTAR/VOLSTP

DO 300 I = NDXTOP, NDXBAS

WORK(12,I) = COMP * WORK(8,I) * WORK(3,I)

WORK(13,I) = SQR(WORK(5,I)*WORK(5,I) + WORK(9,I)*WORK(9,I))

WORK(14,I) = WORK(12,I)/WORK(10,I)

WORK(15,I) = SQR(WORK(11,I)*WORK(11,I)+WORK(13,I)*WORK(13,I))

WORK(18,I) = WORK(1,I)

WORK(1,I) = 300.

WORK(20,I) = I

300 WORK(20,NDXBAS) = -1.

NCOP = 0

999 RETURN

END

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*** END OF MEMBER *** 326 RECORDS PROCESSED *****

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```

SUBROUTINE COMPST(NCODE,IMES)
C REED, BATLUCK, COOKE
C
C COMPST EXAMINES UP TO SEVEN DATASETS (S3,S2,S1,S0,S3/S0,S2/S0,S1/S0)
C AND DERIVES A "COMPOSITE" PROFILE. EACH ALTITUDE LEVEL IS AN
C AVERAGE OF AVAILABLE DATA, WEIGHTED BY THE INVERSE OF THE ASSOCIATED
C ERROR. ERROR INCLUDES THAT DUE TO ERROR IN ALTITUDE.
C
C THE AREA IN COMMON/DATOUT/ IS REASSIGNED TO PROVIDE A WORKSPACE FOR
C THE MANIPULATION OF THE VARIOUS AVAILABLE PROFILES. CONTENTS OF WORK
C IN THIS SUBROUTINE BECOME:
C 1 NUMBER OF VALUES AT THIS LEVEL 11 S1 03 DENSITY ATM-CM/KM
C 2 ALTITUDE - KM 70. - 0 12 S1 " " ERROR X
C 3 OZONE DENSITY ATM-CM/KM 13 S0 " " ATM-CM/KM
C 4 " " NUMBER/M3 14 S0 " " ERROR X
C 5 " " X ERROR 15 S3/S0 " " ATM-CM/KM
C 6 ALT. ERROR, Z1 RESULTING 03 ERR% 16 S3/S0 " " ERROR X
C 7 S3 03 DENSITY -ATM-CM/KM 17 S2/S0 " " ATM-CM/KM
C 8 S3 " " -ERROR X 18 S2/S0 " " ERROR X
C 9 S2 " " -ATM-CM/KM 19 S1/S0 " " ATM-CM/KM
C10 S2 " " -ERROR X 20 S1/S0 " " ERROR X
C
C NOTE THAT THE TYPE 1XX AND 2XX PROFILE TAPE RECORDS ARE NOW LOCATED
C IN SMOOTH.
C
COMMON/DATIN/NLAYRS,SECSZA(60),SMOOTH(20,60,7)
COMMON/DATOUT/N_AV,NDXTOP,NDXBAS,NLVLS,DM(17),WORK(20,89)
COMMON/CONSTT/AVOGAD,VOLSTP,DUM(6)
C
C DM IS FILLED AS FOLLOWS:
C 1 HMDY. ROCOZ LAUNCH
C 2 HMDY. S
C 3 LATITUDE
C 4 LONGITUDE
C 5 ROCOZ FLIGHT MO
C 6 DATE REF RADAR TAPE
C 7 LAUNCH SITE
C 8 "
C 9 "
C10 "
C
CONR = 1.E-5 * AVOGAD/VOLSTP
CALL CMOVE(NDXBAS,DM(5),4)
DM(11) = WORK(2,5)
DM(12) = WORK(3,5)
DM(13) = WORK(5,5)
DM(14) = WORK(5,10)
DM(15) = WORK(6,10)
DO 5 I = 11,15
IF (WORK(1,I).NE.-506.) GO TO 5
DM(16) = WORK(2,I)
DM(17) = WORK(3,I)
GO TO 6

```



```

5  CONTINUE
6  WORK(1,1) = 0.
   CALL CHOVE(WORK(1,1),WORK(2,1),7116)
   NDXTOP = 0
   NDXBAS = 0
C  ASSIGN ALTITUDES TO WORK, FROM 70 TO 0 KM, 1 KM INTERVALS.
   DO 20 I = 1,71
C
C    20 WORK(2,I) = 71. - I
C
C  TRANSFER OZONE DENSITIES AND ERRORS FROM SMOOTH. (1XX AND 2XX RECORDS)
C
C  ***** BECAUSE THE 0 FILTER IN FLT. 329 WAS MALFUNCTIONING, THE
C  ***** FOLLOWING 'DO 50' LOOP IS ONLY DONE THROUGH FILTER 1. THE
C  ***** RATIO DATA FROM SMOOTH IS NOT BEING USED IN DETERMINING
C  ***** NDXTOP AND NDXBAS. NORMALLY THIS LOOP IS DONE 7 TIMES, BUT
C  ***** IT IS ONLY DONE THREE TIMES FOR FLT. 329.
C
C    DO 50 ISM = 1,3
C    DO 50 ISM = 1,7
C      IT = (SMOOTH(2,1,ISM) + 0.01)
C      IF (IT .LE. 0) GO TO 50

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IT = (SMOOTH(1,1,ISM) - 99.9)
IF (IT.GE.10) IT = (IT/10) - 4
IM1 = 13 - 2*IT
C *** TEST
C WRITE(6,2050) ISM,SMOOTH(2,1,ISM),SMOOTH(1,1,ISM),IT,IM1
2050 FORMAT(' COMPST 2050 TEST: ISM=',13,2X,'SMOOTH(2,1,ISM)=',
X G8.3,' SMOOTH(1,1,ISM)=',G8.3,' IT=',13,' IM1=',13)
C
DO 40 I = 2,60,2
IM2 = 71 - (SMOOTH(2,1,ISM)-0.01)
WORK(IM1,IM2) = SMOOTH(7,1,ISM)
WORK(IM1+1,IM2) = SMOOTH(6,1,ISM)
WORK( 6, IM2) = SMOOTH(3,1,ISM)
IF (NDXTOP.EQ. 0) NDXTOP = IM2
IF (IM2.GT. NDXBAS) NDXBAS = IM2
IF (SMOOTH(20,1,ISM).LE. -0.5) GO TO 42
C *** TEST
C WRITE(6,2040) IM2,NDXTOP,NDXBAS
2040 FORMAT(' COMPST 2040 TEST: IM2=',13,' NDXTOP=',13,
X ' NDXBAS=',13)
40 CONTINUE
42 CONTINUE
50 CONTINUE
NLVLS = NDXBAS - NDXTOP + 1
IF (NLVLS.LE. 1) GO TO 900
C *** TEST STATEMENTS
C WRITE (IMES,2060) NDXTOP,NDXBAS,NLVLS,
X ((WORK(I,J),I=1,20),J=NDXTOP,NDXBAS)
2060 FORMAT('1COMPST 2060: WORK NDXTOP,NDXBAS,NLVLS',314,'(1X,F3.0,
X F4.0,1X,G8.3,1X,G8.3,F5.1,
X F5.1,1X,G7.2,F5.1,1X,G7.2,F5.1,1X,G7.2,F5.1,1X,G7.2,
X F5.1,1X,G7.2,F5.1,1X,G7.2,F5.1)')
C
C CALCULATE COMPOSITE OZONE DENSITY PROFILE AND ERRORS (1 STD. DEV.)
C USING S3, S2, S1, AND S0 BUT NOT THE RATIOS.
C
DO 100 I = NDXTOP,NDXBAS,1
60 DMX = 0.0
DMN = 1000.
SUMD = 0.0
SUMR = 0.0
WORK(1,I) = 0.0
DO 70 J = 8,14,2
R = WORK(J,I)
IF (R.LE. 0.0) GO TO 70
D = WORK(J-1,I)
SUMD = SUMD + D/R
SUMR = SUMR + 1./R
IF (D.GT. DMX) DMX = D
IF (D.LT. DMN) DMN = D
WORK(1,I) = WORK(1,I) + 1.
CONTINUE
70 IF (SUMD.LE. 0.0) GO TO 100
WORK(3,I) = SUMD/SUMR
WORK(5,I) = 1./SUMR
WORK(4,I) = CONR * WORK(3,I)

```

```

100 CONTINUE
C
C GO TO 999
C
C ODDS AND ENDS - ONLY ONE ALTITUDE LEVEL
900 WRITE(INES,2900) NLVLS,NDXTOP,NDXBAS,WORK(2,NDXTOP),WORK(2,NDXBAS)
2900 FORMAT('OCOMPST 2900: ONLY',I7,' AVAILABLE, BETWEEN INDICES',I218,
X,' ALTITUDES:',I2F6.1,'. COMPOSITE PROFILE NOT COMPUTED.')
NCODE = -22
C 999 RETURN
END

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*** END OF MEMBER *** 146 RECORDS PROCESSED *****

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SUBROUTINE DATSND(DLAT,NCODE,IMES)
  REED/BATLUCK/COOKE    FEB. 1983
  SONDE COMPUTES PRESSURES AND DENSITIES AS A FUNCTION OF ALTIUDE,
  GIVEN TEMPERATURES VS ALTITUDE, A PRESSURE AT A BASE ALTITUDE, AND
  LATITUDE, USING  $P = P_0 \exp(-GM/(H-H_0)/(R \times T))$ 
  R=8314.32; M=28.964 AS GIVEN IN U.S. STD. ATM, 1976
  G = 9.80665 M/S2 AT 0. ALT AND 45. LAT
  AT LAT=PHI, G(PHI)=G*(1-2.6373E-3 * COS(2*PHI))+5.9E-6 *
  (COS(2*PHI))**2)
  VALUE OF G AND LAT. CORR. FROM LIST,R.J., SMITHSONIAN
  METEOROLOGICAL TABLES, 6 ED., 1968, P 488.
  AT ALT (H), G=G(PHI) * (RO/(RO+H))**2, WHERE
  RO = 6378388. * (1-3.367E-03)*(SIN(LAT))**2+7.1E-6*(SIN(2*LAT))**2
  (BASIC PHYSICS OF THE SOLAR SYSTEM, BLANCO & MCCUSKEY, 1961, P 83)
  DENSITY(KG/M3) = P/(MBAR)*M/(R*T*100.)
  IF A DATASONDE FLIGHT IS NOT AVAILABLE, THEN TEMPERATURE PROFILE
  AND A BASE PRESSURE SHOULD BE TAKEN FROM U.S. STD ATMOSPHERE
  SUPPLEMENTS, 1966, OR OTHER LAT - SEASONAL MODEL

  SONDE (1,X) = ALTITUDE (KM)
  SONDE (2,X) = AIR TEMPERATURE (KELVIN)
  SONDE (3,X) = AIR PRESSURE (MBAR)
  SONDE (4,X) = AIR DENSITY (KG/M3)
  SONDE (5,X) = ERROR IN AIR TEMP (KELVIN)

  NCODE = -5 FAILED TO COMPUTE PRESSURES AND DENSITIES

  DSB(1) = BASE ALTITUDE (KM)
  DSB(2) = BASE TEMPERATURE (K)
  DSB(3) = BASE PRESSURE (MBAR)

  COMMON/PROFLS/DSB(3),MXSND,NECC(2),ECCLM(3,2),SONDE(5,70),
  X ECC(4,19,2),STD(3,60)
  COMMON/CONST/AVOGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,RZRO
  NCODE = 0
  C * 2 TO OBTAIN AVERAGE TEMP AND * 1000. TO CONVERT DELTA H TO M.
  CON = 2000.*AIRM/RSTAR
  C COMPUTE GRAVITY AND EARTH RADIUS AT LATITUDE OF LAUNCH SITE
  RLAT = DLAT/DGTORD
  TM = COS(2*RLAT)
  GRV = GRV45*(1.-2.6373E-3*TM+5.9E-6*TM*TM)
  TM = SIN(RLAT)
  TMA = SIN(2*RLAT)
  RZRO = 6378.388*(1.-3.367E-3*TM*TM+7.1E-6*TM*TM*TM)
  C FIND INDEX CORRESPONDING TO BASE ALTITUDE
  DO 50 I = 1,MXSND
  INDB = I
  IF(ABS(SONDE(1,I) - DSB(1)).LT.0.01) GO TO 60
  50 CONTINUE
  INDB = MXSND + 1
  DO 52 I = 1,MXSND
  INDB = INDB - 1
  IF (DSB(1).LT. SONDE(1,INDB)) GO TO 54
  52 CONTINUE

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GO TO 990
C COMPUTE VALUES AT LEVEL ABOVE DSB. ALT
54 R = RZRO/(RZRO+SONDE(1,INDB))
   SONDE(3,INDB) = DSB(3) * EXP(-GRV *R*R*CON*(SONDE(1,INDB)-DSB(1)))
   X /(SONDE(2,INDB)+DSB(2))
GO TO 65
C COMPUTE PRESSURE AS A FUNCTION OF ALTITUDE, ABOVE AND BELOW BASE.
60 SONDE(3,INDB) = DSB(3)
C *** TEST STATEMENT
C *** WRITE(IMES,2000) AVOGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,
C X
C2000 FORMAT(/,1X,'AVOGAD = ',E10.3,' VOLSTP = ',F8.3,' RSTAR = ',
C X F8.3,' DGTORD = ',F8.3,' GRV45 = ',F8.3,' AIRM = ',F8.3,'
C X ' GRV = ',F8.3,' 1X,RZRO = ',F8.3,' R = ',F8.3,' CON = ',
C X F8.3,' DLAT = ',F8.3)
65 J = INDB
DO 70 I = 2,INDB
   K = J-1
   R = RZRO/(RZRO+SONDE(1,K))
   SONDE(3,K)=SONDE(3,J)*EXP(-GRV*R*R*CON*(SONDE(1,K)-SONDE(1,J)))
   X /(SONDE(2,K)+SONDE(2,J))

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26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=DATSND

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70 J = J-1
   LIM = MXSND-1
   J = INDB
   IF (LIM.LE.INDB) GO TO 85
   DO 80 I = INDB,LIM
     K = J+1
     R = RZRO/(RZRO+SONDE(1,K))
     SONDE(3,K)=SONDE(3,J)*EXP(-GRV*RR*CON*(SONDE(1,K)-SONDE(1,J))
       X/(SONDE(2,K) + SONDE(2,J)))
     80 J = J+1
   C COMPUTE DENSITY(KG/M3)
     85 CON = 100. * AIRM / RSTAR
     DO 90 I = 1,MXSND
       90 SONDE(4,I) = CON*SONDE(3,I)/SONDE(2,I)
       GO TO 999
   C ODDS AND ENDS
     990 WRITE(1,2990) DSB(1),SONDE(1,1),SONDE(1,1),MXSND)
     2990 FORMAT('SONDE 2990: BASE ALTITUDE,',F7.1,' , NOT WITHIN RANGE ',
       X,'OF DATASONDE:',2F7.1)
     NCODE = -5
     999 RETURN
   END
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*** END OF MEMBER *** 99 RECORDS PROCESSED *****

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MEMBER=DINARRY

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

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SUBROUTINE INARRY(MCODE,TEMPX,IMES)
C REED, COOKE
C DEC. 1983
C INARRY (UNDER PROF.CNTL(DINARRY)) IS A SUBROUTINE USED IN BYPASSING
C THE SUBROUTINE BY THE SAME NAME IN PROF.CNTL(INARRY). IN THIS CASE,
C MCBRIDE COEFFICIENTS ARE SUPPLIED IN DATA5 CARDS INSTEAD OF USING
C FIGURES EXISTING IN V. ZAMNERS DISK FILES.
C
C WRITE(IMES,2000)
C 2000 FORMAT('DINARRY 2000: ARRAYS ARE NOT FILLED')
C RETURN
C END
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END OF MEMBER *** 13 RECORDS PROCESSED *****

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MEMBER-INMARRY

26JUL84 08.53.47 - VOL=SACC10, DSM=L3EIR.PROF.CMTL

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SUBROUTINE INMARRY(INCODE,TEMPK,IMES)
C REED, BATLUCK, COOKE      MARCH 1983
C SOLAR FLUX, DIFFUSER, DETECTOR, OZONE ABS AND SCATTERING DATA ARRAYS
C ARE FROM 240.1 TO 340.0 NM. OZONE ABS. AT OTHER TEMP ARE 260.1 TO
C 340.0 NM. ALL ARE PRECEDED BY A 28-WORD HEADER.
C THE INITIAL RECORD OF EACH HAS 64 CHARACTERS FOLLOWED BY 4 R*4 WORDS
C 31-SOLAR FLUX 32-DIFFUSER TR. 33-DETECTOR RESP 34-BETA,RAYLEIGH
C 35-OZ ABS 18C 36-OZ ABS - C 37-OZ ABS - C
C
C DIMENSION IRMG(2,7), TEMPK(3), STR(1000,3), HDR(20),ZEROS(100)
C COMMON/COEFTS/GAMM(1000),BETA(1000),ABSZ(1000),ABST(300,2)
C COMMON/DATOUT/NSAV,PED(20,30),SAVE(20,60)
C EQUIVALENCE (GAMM(1),STR(1,1))
C
C INITIALIZE ARRAYS TO ZERO
C 5 GAMM(1) = 0
C CALL CHOVE(GAMM(1),GAMM(2),18396)
C FILL ARRAYS WITH DATA TO BE USED FOR EFFECTIVE OZONE ABSORPTION.
C GAMM WILL CONTAIN THE PRODUCT OF SOLAR FLUX, DIFFUSER TRANSMISSION,
C AND DETECTOR RESPONSIVITY.
C
C DO 20 M = 1,3
C N = M + 30
C READ (N,ERR=905,END=910) HDR,ZEROS,(STR(J,M),J=1,1000)
C WRITE(IMES,2005) M, HDR
C 2005 FORMAT ('01NARRY 2005: UNIT',I3,X,16A4,4F7.1)
C
C DETERMINE WAVELENGTH/INDEX RANGE; CONVERT, IF NECESSARY, NM TO A.
C 15 IF (HDR(17) .LT. 1000.) HDR(17) = 10. * HDR(17)
C IF (HDR(18) .LT. 1000.) HDR(18) = 10. * HDR(18)
C IRMG(1,M) = (HDR(17) + .001)
C IRMG(2,M) = (HDR(18) + .001)
C PLACE HDR INFO IN PED
C NSAV = NSAV + 1
C PED(1,NSAV) = -507. - M
C CALL CHOVE(HDR(1),PED(2,NSAV),76)
C 20 CONTINUE
C
C CALCULATE PRODUCT OF SOLAR FLUX, DIFF TRANSM, AND DETECTOR RESP.
C
C DO 25 I = 1,1000
C 25 GAMM(I) = GAMM(I) * BETA(I) * ABSZ(I)
C
C DETERMINE RANGE OF USEFUL DATA IN GAMM
C IA = 1
C IB = 10000
C DO 30 I = 1,3
C IF (IRMG(1,I) .GT. IA) IA = IRMG(1,I)
C IF (IRMG(2,I) .LT. IB) IB = IRMG(2,I)
C 30 IF ((IB-IA) .LT. 100) GO TO 915
C
C BRING IN RAYLEIGH SCATTERING COEFF. AND OZONE ABS. COEFF AT ROOM TEMP.
C

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DO 50 M = 2,3
N = M + 32
READ (N,ERR=905,END=910) HDR,ZEROS,(STR(J,M),J=1,1000)
WRITE (IMES,2005) N, HDR
C
45 IF (HDR(17) .LT. 1000.) HDR(17) = 10. * HDR(17)
IF (HDR(18) .LT. 1000.) HDR(18) = 10. * HDR(18)
K = M + 2
IRNG(1,K) = HDR(17)
IRNG(2,K) = HDR(18)
C
NSAV = NSAV + 1
PED(1,NSAV) = -509. - M
CALL CHOVE(HDR(1),PED(2,NSAV),76)
50 CONTINUE
C
C RANGE LIMITS ; STORE TEMPERATURE
C
DO 55 I = 4,5
IF (IRNG(1,I) .GT. IA) IA = IRNG(1,I)
55 IF (IRNG(2,I) .LT. IB) IB = IRNG(2,I)

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IF ((IB-IA) .LT. 100) GO TO 915
TEMPK(1) = HDR(19)
IF (TEMPK(1) .EQ. 0.0) TEMPK(1) = 300.
C BRING IN OZONE ABS COEFFICIENTS AT LOW TEMPERATURES
C
DO 70 M = 1,2
N = M + 35
READ (N,ERR=905,END=910) HDR,ZEROS,ZEROS,(ABST(J,M),J=1,800)
WRITE (IMES,2005) N, HDR
C
C
65 IF (HDR(17) .LT. 1000.) HDR(17) = HDR(17) * 10.
IF (HDR(18) .LT. 1000.) HDR(18) = HDR(18) * 10.
K = M + 4
IRNG(1,K) = HDR(17)
IRNG(2,K) = HDR(18)
TEMPK(M+1) = HDR(19)
NSAV = NSAV + 1
PED(1,NSAV) = -512. - M
CALL CMOVE(HDR(1), PED(2,NSAV),76)
70 CONTINUE
C PUT TEMPERATURE INTO KELVIN UNITS
C
DO 80 I = 1,3
80 IF (TEMPK(I) .LT. 70.) TEMPK(I) = TEMPK(I) + 273.15
C *** TEST STATEMENTS
C CALL CFTNRT(TEMPK,IRNG,IMES)
GO TO 999
C
C
C ODDS AND ENDS
C
C READ ERROR IN DATASET
905 WRITE (IMES,2905) N
2905 FORMAT ('INARYY 2905: READ ERROR ON UNIT',I4)
NCODE = -12
GO TO 999
C
C EOF AFTER HEADER
910 WRITE (IMES,2910) N
2910 FORMAT ('INARYY 2910: UNEXPECTED EOF AFTER HEADER RECORD ON UNIT',
X14)
NCODE = -13
GO TO 999
C
C
C USEFUL RANGE OF TABULAR DATA IS INADEQUATE
915 WRITE (IMES,2915) IA,IB,IRNG
2915 FORMAT ('INARYY 2915: SOLAR FLUX, DIFF TRANSM, AND DETECTOR RESP',
X' IS AVAILABLE ONLY FOR INDICES',215,' IRNG:',3(2X,215))
NCODE = -14
GO TO 999
C
C 999 RETURN
END

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*** END OF MEMBER *** 132 RECORDS PROCESSED *****

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C SUBROUTINE LINFIT
C BOVINGTON, P.R., DATA REDUCTION..., MCGRAW-HILL, 1969, P. 104-5.
C
C PURPOSE
C MAKE A LEAST-SQUARES FIT TO DATA WITH A STRAIGHT LINE
C   Y = A + B*X
C
C USAGE
C CALL LINFIT(X, Y, SIGMAY, NPTS, MODE, A, SIGMAA, B, SIGMAB, R)
C
C DESCRIPTION OF PARAMETERS
C   X - ARRAY OF DATA POINTS FOR INDEPENDENT VARIABLE
C   Y - ARRAY OF DATA POINTS FOR DEPENDENT VARIABLE
C   SIGMAY - ARRAY OF STANDARD DEVIATIONS FOR Y DATA POINTS
C   NPTS - NUMBER OF PAIRS OF DATA POINTS
C   MODE - DETERMINES METHOD OF WEIGHTING LEAST-SQUARES FIT
C     +1 (INSTRUMENTAL) WEIGHT(I) = 1./SIGMAY(I)**2
C     0 (NO WEIGHTING) WEIGHT(I) = 1.
C     -1 (STATISTICAL) WEIGHT(I) = 1./Y(I)
C   A - Y INTERCEPT OF FITTED STRAIGHT LINE
C   SIGMAA - STANDARD DEVIATION OF A
C   B - SLOPE OF FITTED STRAIGHT LINE
C   SIGMAB - STANDARD DEVIATION OF B
C   R - LINEAR CORRELATION COEFFICIENT
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C *****
C SUBROUTINE LINFIT(X,Y,SIGMAY,NPTS,MODE,A,SIGMAA,B,SIGMAB,R)
C
C DOUBLE PRECISION SUM, SUMX, SUMY, SUMX2, SUMXY, SUMY2
C DOUBLE PRECISION XI, YI, WEIGHT, DELTA, VARNCE, A, B
C DIMENSION X(1), Y(1), SIGMAY(1)
C
C ACCUMULATE WEIGHTED SUMS
C
C11 SUM = 0.
C   SUMX = 0.
C   SUMY = 0.
C   SUMX2 = 0.
C   SUMXY = 0.
C   SUMY2 = 0.
C21 DO 50 I = 1,NPTS
C   XI = X(I)
C   YI = Y(I)
C   IF (MODE) 31, 36, 38
C31 IF (YI) 34, 36, 32
C32 WEIGHT = 1. / YI
C   GO TO 41
C34 WEIGHT = 1. / (-YI)
C   GO TO 41
C36 WEIGHT = 1.

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38  GO TO 41
41  HEIGHT = 1. / SIGM(YI)X2
    SUM = SUM + HEIGHT * XI
    SUMX = SUMX + HEIGHT * XI
    SUMY = SUMY + HEIGHT * XI
    SUMX2 = SUMX2 + HEIGHT * XI * XI
    SUMXY = SUMXY + HEIGHT * XI * YI
    SUMY2 = SUMY2 + HEIGHT * YI * YI
50  CONTINUE

    C      CALCULATE COEFFICIENTS AND STANDARD DEVIATIONS
    C
51  DELTA = SUMXSUMX2 - SUMX*SUMX
53  A = (SUMX2*SUMY - SUMX*SUMXY) / DELTA
61  B = (SUMXY*SUM - SUMX*SUMY) / DELTA
62  IF (MODE) 62, 64, 62
62  VANCE = 1.
64  GO TO 67
64  C = NPTS - 2
    VANCE = (SUMY2 + A*SUM + B*SUMX2
X -2.0000*(A*SUMY + B*SUMXY - A*B*SUMX)) / C

```

C C C

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=LINFIT

```
IF (VARNCE.LT.0.0) VARNCE = 0.0D0
67 SIGNAA = DSQRT(VARNCE*SUNX2 / DELTA)
68 SIGNAB = DSQRT(VARNCE*SUN / DELTA)
71 R = (SUN*SUNXY - SUMX*SUNY) /
  X DSQRT(DELTA*(SUM*SUNY2 - SUMY*SUNY))
  RETURN
  END
```

00000812
00000820
00000830
00000840
00000850
00000860
00000870

*** END OF MEMBER *** 84 RECORDS PROCESSED

ORIGINAL PAGE
OF POOR QUALITY

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SUBROUTINE MODEL(NCODE)
C REED, BATLUCK, AND COOKE      MAR 1983
C BATLUCK, COOKE                MAY 1984      MODIFIED CODE TO CORRECTLY
C                                     FILL PED ARRAY
C
C MODEL FILLS THE ARRAY, STD., WITH VALUES BASED ON THE KRUEGER-MINZNER
C MODEL. IT WOULD BE DESIRABLE TO ADJUST THE MODEL PROFILE FOR
C TOTAL OZONE (FROM DOBSON OBSERVATIONS), AND LATITUDE, BASED,
C FOR EXAMPLE, ON THE FIRST GUESS TABLES USED IN SBUV DATA
C REDUCTION.
C
C NCODE = 1 NO PROBLEMS
C STD(1)= ALTITUDE (KM)
C (2)= OZONE NUMBER DENSITY (MOLECULES/M3)
C (3)= OZONE OVERBURDEN (ATM-CM)
C
C DIMENSION DKM (31), DKMID(2)
C COMMON/PROFLS/DUMA(12),DUMB(502),STD(3,60)
C COMMON/CONST/AVOGAD,VOLSTP,DUMC(6)
C COMMON/DATOUT/NSAV,PED(20,30),SAVE(20,60)
C
C VALUES IN DKM CORRESPOND TO OZONE NUMBER DENSITY AT 10,12,14,..70 KM
C FROM US STD ATMOS., 1976, ALL TO BE MULTIPLIED BY 1.E17
C BUR = OZONE OVERBURDEN ABOVE 70 KM, EST. FROM US STD, 1976.
C
C DATA DKMID/'KRUG','MINZ'/
C DATA DKM /11.3,20.2,23.5,29.5,40.4,47.7,48.6,45.4,40.3,32.4,25.2,
C X 20.3,15.8,12.2,8.73,6.07,3.98,2.74,1.69,1.03,.664,.384,.255,.161,
C X .112,.0733,.0481,.0317,.0172,.0075,.0054/
C CON = 1.E05 * VOLSTP/AVOGAD
C BUR = 5.35E-6
C
C FILL STD ARRAY, USING 1 KM INTERVALS, DESCENDING FROM 70 AT STD(1,1)
C KM = 71
C K = 31
C DO 100 I=1,60
C STD(1,I) = KM - I
C OZONE NUMBER DENSITIES
C IF ( (KM-I) .EQ. (2*K+8) ) GO TO 20
C IT = K-1
C STD(2,I) = (DKM(K) + DKM(IT)) * 0.5E17
C K = IT
C GO TO 25
C 20 STD(2,I) = DKM(K) * 1.E17
C OZONE OVERBURDENS
C 25 IF (I .GT. 1) GO TO 30
C STD(3,I) = BUR
C GO TO 100
C 30 IT = I-1
C STD(3,I) = (STD(2,IT) + STD(2,I)) * 0.5 * CON + STD(3,IT)
C 100 CONTINUE
C
C PLACE IN PEDIGREE (11,12,13) OZONE DENSITIES FROM STD.
C
C PED(1,11) = -504.
C PED(2,11) = 70.

```

00000550
 00000560
 00000570
 00000580
 00000590
 00000600
 00000610
 00000620
 00000630
 00000635
 00000640
 00000650
 00000660
 00000670
 00000680
 00000690
 00000700
 00000710
 00000720
 00000730
 00000740

```

PED(3,11) = -1.
PED(4,11) = 50.
PED(5,11) = DKMID(1)
PED(6,11) = DKMID(2)
PED(7,11) = KM - 1
PED(8,11) = BUR
DO 150 I= 9,20
  J = I-8
150 PED (I,11)= STD(2,J)
C
C PED (1,12) = -505.
DO 160 I=2,20
  J = I + 11
160 PED (I,12) = STD (2,J)
C
C PED (1,13) = -505.
DO 170 I=2,20
  J = I + 30
170 PED (I,13) = STD (2,J)
  
```

GROUP
 OF FOUR

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=MODEL

PED (1,14) = -505.

DO 180 I = 2,11

J = I + 49

180 PED (I,14) = STD (2,J)

C

NCODE = 1

RETURN

END

*** END OF MEMBER ***

85 RECORDS PROCESSED

00000742
00000744
00000746
00000748
00000750
00000760
00000770
00000780

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SUBROUTINE OVERLP (IMES,ICLK)
C REED, BATLUCK, AND COOKE
C APRIL 1983
C OVERLP CHECKS THE OZONE DENSITIES FOR CONSISTENCY AMONG THE VARIOUS
C PROFILES WHERE THEY OVERLAP IN ALTITUDE, FITTING THE POINTS TO A
C LINEAR REGRESSION; Y = A + BX, WHERE Y IS DENSITY FROM THE LONGER
C WAVELENGTH FILTER.
C NPRS = NUMBER OF PAIRS OF OVERLAPS
C DIMENSION HEADS(7),X(30),Y(30),SIGMAY(30)
C COMMON/DATOUT/NSAV,NDXTOP,NDXBAS,NLVLS,DM(17),
C X WORK(20,71), TABLE(10,36)
C DATA HEADS/' S3 ',' S2 ',' S1 ',' S0 ',' S3/0','S2/0','S1/0'/,
C X 'MODE'/,
C
C NPRS = 0
DO 200 IX = 7,17,2
IT = IX + 2
DO 100 IY = IT,19,2
NP = 0
ALTMX = 0.
ALTMN = 0.
IHX = (IX-5)/2
IHY = (IY-5)/2
DO 50 L = NDXTOP, NDXBAS
C FIND SET OF OVERLAPPING DATA -
IF (WORK(1,L) .LE. 1.001 .OR. WORK(IX,L) .LE. 0. .OR. WORK(IY,L)
X .LE. 0.) GO TO 50
IF (ABS(WORK(IY,L) - WORK(IX,L))/WORK(IY,L)).GT.0.30) GO TO 5000000320
NP = NP + 1
IF (NP.LE.30) GO TO 40
WRITE(IMES,2040) HEADS(IHX),HEADS(IHY),WORK(2,L)
2040 FORMAT(' OVERLP 2040: IN ANALYSIS OF',A4,' AND',A4,
X ' ALTITUDES BELOW',F4.0,' ARE IGNORED')
NP = 30
GO TO 60
40 IF (NP .EQ. 1) ALTMX = WORK(2,L)
X(NP) = WORK (IX,L)
Y(NP) = WORK (IY,L)
SIGMAX = WORK(IX+1,L)*X(NP)*0.01
SIGMAY(NP) = WORK (IY+1,L)*Y(NP)*0.01
ALTMN = WORK(2,L)
50 CONTINUE
IF (NP .EQ. 0) GO TO 100
IF (NP .GT. 1) GO TO 60
B = Y(1)/X(1)
A = 0.
SIGMAA = 0.
R = 0.
SIGMAB=50.*SQRT(SIGMAY(1)*SIGMAY(1)+SIGMAX*SIGMAX)/(X(1)+Y(1))
GO TO 70

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00000490
00000500
00000510
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```

C LINEAR REGRESSION
60 CALL LINFIT(X,Y,SIGMAY,NP,MODE,A,SIGMAA,B,SIGMAB,R)
C FILL OUTPUT TABLE
70 NPRS = NPRS + 1
TABLE (1,NPRS) = HEADS(IHX)
TABLE (2,NPRS) = HEADS(IHY)
TABLE (3,NPRS) = A/TMX
TABLE (4,NPRS) = ALTMN
TABLE (5,NPRS) = NP
TABLE (6,NPRS) = A
TABLE (7,NPRS) = SIGMAA
TABLE (8,NPRS) = B
TABLE (9,NPRS) = SIGMAB
TABLE(10,NPRS) = R
IF (NPRS .EQ. 36) GO TO 210
100 CONTINUE
200 IF (NPRS .EQ. 0) GO TO 990
C WRITE OUTPUT TABLE
210 WRITE (ICNK,2210) MODE,((TABLE(I,J),I=1,10),J=1,NPRS)

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26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=OVERLP

```
2210 FORMAT ('NO OVERLAP ANALYSIS , WITH WEIGHTING MODE =',I2,  
X', FILT Y = A + B * FILT X' ,//', FILT X FILT Y MX ALT MM ALT PAIRS',  
X', A STD DEV A B STD DEV B CORREL',//  
X(3X,A4,2X,A4,2F7.0,F6.0,2X,E11.4,1X,E9.2,2X,F11.4,1X,F9.5,1X,  
X F7.4))  
IF (MODE.EQ.1) WRITE(ICHK,2215)  
2215 FORMAT('MODE 1 IS INSTRUMENTAL WEIGHTING, THAT IS, 1/SIGMAY**2')  
GO TO 999  
990 WRITE (TIMES,2990)  
2990 FORMAT ('NO OVERLAP 2990; NO PROFILES OVERLAPPED IN ALTITUDE.')  
999 RETURN  
END
```

*** END OF MEMBER *** 89 RECORDS PROCESSED *****

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SUBROUTINE OVRBRDKALT, SECANT, SLTOZ, SLTAR, MCODE)
C REED, BATLUCK, COOKE      MAR 1983
C OVRBRD ESTIMATES THE SLANT PATH OZONE AND AIR MASS BETWEEN THE OBSER-
C VATION AT ALTITUDE AND THE SUN, USING THE STD OZONE PROFILE AND
C DATSND AIR PROFILE.
C
C ALT = ALTITUDE OF OBSERVATION - KM
C SECANT = SECANT OF THE SOLAR ZENITH ANGLE, AS GIVEN BY SUBR. SECANG
C SLTOZ = SLANT COLUMN OF OZONE - ATM-CM
C SLTAR = SLANT AIR MASS - ATMOSPHERES
C MCODE = 0 NO PROBLEM
C      = -9 FAILED TO PROVIDE OZONE OVERBURDEN
C      = -10 FAILED TO PROVIDE AIR OVERBURDEN
C      = -11 FAILED TO PROVIDE BOTH
C
C COMMON/PROFLS/DSBALT,DSBPRS,MXSND,NECC(2),SONDE(5,70),ECC(4,21,2),
C X STD(3,60)
C COMMON/CONSTT/AVOGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,RZRO,IMES
C
C MCODE = 0
C
C FIND GIVEN ALTITUDE IN STD OZONE PROFILE
C DO 10 I=1,60
C   J = I
C   IF (ALT - STD(1,I)) 10,20,30
C 10 CONTINUE
C GO TO 900
C
C USE OVERBURDEN AT GIVEN ALTITUDE
C 20 COLOZ = STD(3,J)
C GO TO 40
C
C INTERPOLATE TO OBTAIN OVERBURDEN
C 30 FRAC = (ALT - STD(1,J))/(STD(1,J-1) - STD(1,J))
C COLOZ = STD(3,J) + FRAC * (STD(3,J-1) - STD(3,J))
C
C SLANT OZONE
C 40 SLTOZ = COLOZ * SECANT
C
C FIND ALTITUDE IN DATASONDE PROFILE
C 100 DO 110 I=1,MXSND
C   J = I
C   IF (ALT - SONDE(1,I)) 110, 120, 130
C 110 CONTINUE
C GO TO 910
C
C FIND DENSITY AT ALT
C 120 DENS = SONDE(4,J)
C GO TO 140
C 130 FRAC = (ALT - SONDE(1,J))/(SONDE(1,J-1) - SONDE(1,J))
C DENS = EXP(ALOG(SONDE(4,J)) + FRAC*(ALOG(SONDE(4,J-1)) - LOG(SONDE(4,J))))
C

```

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C COMPUTE DENSITY SCALE HEIGHT (OPTICS OF THE ATMOS., MCCARTNEY, 1976,
C J. WILEY, P.81)  RG IS ABOUT 29; FOR KM; 29E-3
C
140 RG = 1.E-3*HSTAR / (AIRHGRV)
    IF (J.EQ. 1) GO TO 150
    K = J - 5
    IF (K.LE. 0) K = 1
    GAMMA = -(SONDE(2,J) - SONDE(2,K))/(SONDE(1,J) - SONDE(1,K))
    HRMO = RG * SONDE(2,J) / (1 - RG * GAMMA)
    GO TO 160
150 HRMO = RG * SONDE(2,J)
C
C COMPUTE SLANT AIR MASS; DIVIDE BY STD AIR MASS IN KG/M2, CHVRT
C HRMO TO M
C 160 SLTAR = SECANT * HRMO * DENS / 101.325
    GO TO 990
C ODDS AND ENDS
C NO SLOTS
C 900 WRITE (IMES,2900) ALT, STD(1,1), STD(1,J)

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MEMBER=OVERORD

26JUL84 08.53.47 - VOL=SACC10, BSN=L3EIR.PROF.CNTL

```
2900 FORMAT('00VRBRD 2900: ALTITUDE(',F6.0,') NOT IN RANGE OF PROFILE ',00000770
X,' IN STD:', 2F7.0)
      NCODE = -9
      GO TO 100
C NO SLTAR
910 WRITE (IMES,2910) ALT, SONDE(1,1), SONDE(1,MXSND)
2910 FORMAT ('00VRBRD 2910: ALTITUDE(',F6.0,') NOT IN RANGE OF PROFILE ',00000780
X,' IN SONDE:', 2F7.0)
      NCODE = NCODE - 10
      IF (NCODE .LT. -11) NCODE = -11
995 RETURN
      END
```

*** END OF MEMBER *** 90 RECORDS PROCESSED *****

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SUBROUTINE OZDENS(NCODE,IMES,ITBL)
  REED, BATLUCK, AND COOKE   APR 1983

  OZDENS COMPUTES OZONE DENSITY AND COLUMN CONTENT FOR EACH ALTITUDE
  LEVEL FOR EACH FILTER, BASED EITHER ON OBSERVED INTENSITIES OR ON
  THEIR RATIOS TO SO INTENSITY. AFTER THE PROFILE FOR A FILTER IS
  COMPLETE, THE RESULTS (2 RECORDS PER ALTITUDE LEVEL) ARE WRITTEN
  ON THE OUTPUT TAPE, AND ALSO MOVED TO THE SMOOTH ARRAY, REPLACING
  THE INPUT DATA FOR THAT FILTER, THUS KEEPING THE PROFILES AVAILABLE
  FOR USE BY LATER SUBROUTINES.

  THE OZONE DENSITY IS BASED ON THIS FORMULA, EVALUATED WITH DN = 2 KM:
  DU/DH = -(LN(IT)-LN(IB))/2 + BEFF(DH/DH)/(AEFF + U * D(AEFF)/DU),
  ITERATED AS NECESSARY. AN ADJUSTMENT IS MADE TO BETA FOR SCATTERED
  LIGHT IN THE COMPENSATION CHANNEL, UNLESS RATIO TO SO IS BEING USED.

  ARGUMENTS
  NCODE = 1 NO PROBLEMS
          =20 DESIRED ALTITUDE NOT FOUND IN SONDE OR ECC PROFILE.
          =21 DESIRED ALTITUDE NOT FOUND IN STD - FOR OZONE COLUMN.

  SELECTED VARIABLES
  IF      = INDEX FOR FILTER SELECTION CARD BEING PROCESSED      1-7
  ISM     = LOCATION OF DATA IN SMOOTH - 3RD SUBSCRIPT          1-7
  LT      = INDEX OF TOP ALTITUDE LEVEL UNDER CONSIDERATION; 2ND SUB-
           SCRIPT IN SMOOTH 1-57
  LC      = INDEX FOR CENTER ALTITUDE 2-59
  LB      = INDEX FOR BOTTOM ALTITUDE 3-60
  ALTT,ALTC,ALTB = ALTITUDES UNDER CONSIDERATION - KM
  ASLTT,ASLTC,ASLTB = SLANT AIR MASS - ATMOSPHERES
  DMHDC   = RATE OF CHANGE OF SLANT AIR MASS
  UT,UC,UB = SLANT PATH OZONE BETWEEN OBS AND SUN - ATM-CM
  ALFAC,ALFAC,ALFAB = EFFECTIVE OZONE ABSORPTION
  BETAT,BETAC,BETAB = EFFECTIVE SCATTERING COEFFICIENT
  DELU    = OZONE SLANT COLUMN BETWEEN T AND B
  ODENC   = OZONE DENSITY AT C ATM-CM /KM
  NS      = NUMBER OF RECORDS IN SAVE

  LOGICAL  FIRST, RATIO

  COMMON/SETUP/DUM(6),INCLD(7),TOP(7),BASE(7)
  COMMON/PROFLS/DSB(3),MXSND,NECC(2),ECCLM(3,2),SONDE(5,70),
  X      ECC(4,19,2),STD(3,60)
  COMMON/DATAIN/NLAYRS,SECSZA(60),SMOOTH(20,60,7)
  COMMON/DATOUT/NSAV,PED(20,30),SAVE(20,60)
  COMMON/CONSTT/AVOGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,RZRO
  DATA BETCHMP/0.472/

  NSETS = 0

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C LAUNCH HOUR
  HOUR = (INT(PED(5,1)/10000.)) * 10000.
  CONR = 1.E-5 * AVOGAD / VOLSTP
  CONP = 0.1 * RSTAR / VOLSTP
  COND = 100. * AVOGAD / RSTAR
  CONS = 2000. * AIRM / RSTAR

C DO LOOP FOR S3, S2, S1, S0, S3/S0, S2/S0, S1/S0.
  DO 800 IF = 1,7
    RATIO = .FALSE.
    C WHAT FILTER IS TO BE PROCESSED?
    IF (INCLD(IF).GT.30 .OR. INCLD(IF).LT.0) GO TO 800
    IF (INCLD(IF).GT.5) RATIO = .TRUE.
    FLTRID = INCLD(IF)
    NS = 0
    C FIND START OF THIS FILTER IN SMOOTH
    DO 50 I=1,7
      ISM = I
      IF (ABS(SMOOTH(1,1,I)-FLTRID) .LT. 0.01) GO TO 55
    50 CONTINUE
    WRITE (IMES,1950) INCLD(IF),(SMOOTH(1,1,J)),J=1,7)

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1950 FORMAT('OZDENS 1950: FILTER ID',I3,' NOT FOUND IN SMOOTH',7F10.0)00000770
GO TO 8000000780
C FIND INITIAL ALTITUDE LEVEL FOR THIS FILTER
55 FIRST = .TRUE.00000790
DO 70 I=1,600000800
  LT = I0000810
  IF (SMOOTH(2,LT,ISM) .LE. TOP(IF)) GO TO 800000820
  CONTINUE0000830
70 WRITE (IMES,1970) TOP(IF), INCLD(IF)0000840
1970 FORMAT ('OZDENS 1970: TOP ALTITUDE',F7.0,' FOR',I3,' NOT FOUND',0000850
X' IN SMOOTH')0000860
GO TO 800000870
0000880
0000890
0000900
0000910
0000920
0000930
0000940
0000950
0000960
0000970
0000980
0000990
0001000
0001010
0001020
0001030
0001040
0001050
0001060
0001070
0001080
0001090
0001100
0001110
0001120
0001130
0001140
0001150
0001160
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0001190
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0001210
0001220
0001230
0001240
0001250
0001260
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0001280
0001290
0001300
0001310
0001320
0001330

C DEFINE TOP, CENTER, AND BOTTOM ALTITUDE LEVEL;
C REENTRY FOR SUCCEEDING LEVELS.
75 LT = LT + 1
80 LC = LT + 1
  LB = LT + 2
  IF (LB.GT.NLAYRS .OR. SMOOTH(2,LB,ISM).LT.BASE(IF)) GO TO 800
C
  ALTT = SMOOTH (2,LT,ISM)
  ALTC = SMOOTH (2,LC,ISM)
  ALTB = SMOOTH (2,LB,ISM)
C OBTAIN SLANT AIR MASS AND ITS RATE OF CHANGE
  CALL SLANTA(LT,LC,LB,ALTT,ALTC,ALTB,ASLTC,ASLTT,ASLTB,DMDHC,ISNDC,
X NCODE,IMES)
C *** TEST STATEMENTS
C WRITE (IMES,2000) LT,LC,LB,ALTT,ALTC,ALTB,ASLTT,
X ASLTC,ASLTB,DMDHC,ISNDC,NCODE
2000 FORMAT(/,1X,'OZDENS 2000: LT =',I2,' LC =',I2,' LB =',I2,
X ' ALTT =',F6.3,' ALTC =',F6.3,' ALTB =',F6.3,' ASLTT =',
X G10.3,' ASLTC =',G10.3,' ASLTB =',G10.3,'/1X,'DMDHC =',G10.3,
X ' ISNDC =',I3,' NCODE =',I3)
  IF (NCODE .LT. 0) GO TO 900
C
C OBTAIN D(LN(I))/DH FOR TWO KM CENTERED AT C
C
  DLIDH=(ALOG(SMOOTH(3,LT,ISM)) - ALOG(SMOOTH(3,LB,ISM))) * (-0.5)
C
C OBTAIN ESTIMATES OF SLANT PATH OZONE.
  IF (.NOT. FIRST) GO TO 95
C OBTAIN FROM MODEL OZONE PROFILE - GIVEN AT 1 KM INTERVALS.
  DO 90 IX=1,60
    IF (STD(1,IX) .NE. ALTT) GO TO 90
    UT = STD(3,IX) * SECSZA(LT)
    UC = STD(3,IX+1) * SECSZA(LC)
    UB = STD(3,IX+2) * SECSZA(LB)
    GO TO 100
  90 CONTINUE
    GO TO 910
C UPDATE SLANT OVERBURDENS
  95 UT = UC
    UC = UB
    DELCT = UC/SECSZA(LC) - UT/SECSZA(LT)
    UB = (UC/SECSZA(LC) + DELCT) * SECSZA(LB)

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```

C OBTAIN VALUES FOR EFFECTIVE OZONE ABS. COEFF. AND SCATTERING COEFF.
C
C 100 CONTINUE
C *** TEST STATEMENT
C WRITE (IMES,2050) DLIDH,UT,UC,UB,DELCT
C 2050 FORMAT(/,IX,OZDENS 2050: DLIDH = ',G11.3,' UT = ',G11.3,' UC = ',
X G11.3,' UB = ',G11.3,' DELCT = ',G11.3)
IF (.NOT. FIRST) GO TO 104
C
CALL ALFEFF(IF,ALTT,UT,ASLTT,ALFAT,BETAT,NCODE,IMES,ITBL)
IF (ALTT.EQ. TOP(IF)) ALFTOP = ALFAT
IF (NCODE.LT. 0) GO TO 999
IF (.NOT.RATIO) BETAT = BETAT - BETCMP
CALL ALFEFF(IF,ALTC,UC,ASLTC,ALFAC,BETAC,NCODE,IMES,ITBL)
IF (NCODE.LT. 0) GO TO 999
IF (.NOT.RATIO) BETAC = BETAC - BETCMP
GO TO 105
C
C UPDATE
C 104 ALFAT = ALFAC

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00001340
00001350
00001360
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00001400
00001410
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00001500
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00001540

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      ALFAC = ALFAB
      BETAT = BETAC
      BETAC = BETAB
      PDELU = 0.0
105 CALL ALFEFF(IF,ALTB,UB,ASLTB,ALFAB,BETAB,NCODE,IMES,ITBL)
      IF (.NOT.RATIO) BETAB = BETAT - BETCMP
      IF (NCODE .LT. 0) GO TO 999

C CALCULATE SLANT OZONE BETWEEN T AND B LEVELS
C
      NI = 0
106 CONTINUE
      WRITE (IMES,2106) ALFAT,ALFAC,ALFAB,BETAT,BETAC,BETAB
2106 FORMAT ('00ZDENS 2106: ALFAT,C,B =',F13.6,' BETAT,C,B = ',
X 3F10.6)
      NI = NI + 1
      DELU = (ALTT - ALTB) *
X (DLIDH+BETAC*DMDHC)/(ALFAC+(ALFAT-ALFAB)*UC*0.5)
      DELU = ABS(DELU)

C ITERATE?
C
      WRITE(IMES,2108) DELU,PDELU
2108 FORMAT('00ZDENS 2108: DELU =',G12.4,2X,'PDELU =',G12.4)
      IF (ABS(DELU-PDELU)/DELU) .LT. 0.001) GO TO 110
      IF (NI .LT. 4) GO TO 109
      WRITE(IMES,2109) IF,ALTC
2109 FORMAT('0ZDENS 2109: NUMBER OF ITERATIONS FOR FILTER',I3,
X ' AT',F4.0,' KM IS 4. GO TO NEXT FILTER.')
      GO TO 150
109 PDELU = DELU
C RECOMPUTE UB, ALFAC, BETAC
      UB = UT + DELU
      CALL ALFEFF(IF,ALTB,UB,ASLTB,ALFAB,BETAB,NCODE,IMES,ITBL)
      IF (.NOT.RATIO) BETAB = BETAT - BETCMP
      IF (NCODE .LT. 0) GO TO 999
      ALFAC = 0.5 * (ALFAT + ALFAB)
      BETAC = 0.5 * (BETAT + BETAB)
      GO TO 106

C ITERATION COMPLETE
110 UC = UT + 0.5 * DELU
C OZONE DENSITY AT C IN ATM-CM
      ODENC = 0.5 * DELU / SECSZA(LC)

C
C
C PLACE DATA IN OUTPUT ARRAY SAVE. UPON COMPLETION OF A FILTER, THESE
C ARE TO BE WRITTEN ON TAPE AND ALSO SAVED IN SMOOTH, OVERWRITING
C SMOOTH DATA FOR THAT FILTER, FOR USE BY OTHER SUBROUTINES IN
C PROFILE.
C
      NS = NS + 1
      SAVE (1,NS) = 100. + SMOOTH(1,1,ISM)
      SAVE (2,NS) = ALTC
      SAVE (3,NS) = SMOOTH (10,LC,ISM)
      SAVE (4,NS) = SECSZA (LC)
      SAVE (5,NS) = SMOOTH (3,LC,ISM)

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ORIGINAL PAGE
OF POOR QUALITY

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SAVE (6,NS) = UC
SAVE (7,NS) = ASLTC
SAVE (8,NS) = ALFAC
SAVE (9,NS) = BETAC
SAVE(10,NS) = DLIDH
SAVE(11,NS) = (ALFAT-ALFAB) * 0.5 / UC
SAVE(12,NS) = DMDHC
SAVE(13,NS) = ALFAC * UC
SAVE(14,NS) = BETAC * ASLTC

C
C FRASER CORRECTION IS AN ESTIMATE OF THE LIGHT SCATTERED OUT OF PATH
C TO THE SUN: I(NO LOSS)(1-F) = I(OBSERVED) FROM R.S. FRASER, GSFC.
C SEE THOMAS ET AL., APPL. OPT. 21,2436, JULY 1,1982.
C
C SAVE (15,NS) = 0.376 * ((SECSZA(LC))*0.874)/10.*(ALTC/16.)
C
C ESTIMATE NOISE (1 SD) IN D(LN(I)
C
C ERRTT= SMOOTH(15,LT,ISM)**2+(SMOOTH(17,LT,ISM)*(ALTT-SMOOTH(12,LT,
XISM))**2
```

```

C      ERRBB= SMOOTH(15,LB,ISM)**2+(SMOOTH(17,LB,ISM)*(ALTB-SMOOTH(12,LB,
XISM))**2
C
C      SAVE (16,NS) = SQRT(ERRTT+ERRBB)
C      SAVE (17,NS) = SMOOTH(11,LT,ISM) - SMOOTH(12,LB,ISM)
C      SEC = SMOOTH(6,LC,ISM)
C      SAVE (18,NS) = SMOOTH (16,LC,ISM)
C      SAVE (19,NS) = SMOOTH (17,LC,ISM)
C      SAVE (20,NS) = SMOOTH ( 7,LC,ISM)
C *** TEST STATEMENTS
C      WRITE(16,2110) (L,L=1,20)
2110  FORMAT(/,1X,' SAVE = (IN COLUMN,ROW ORDER)',/,4X,'NS',9X,
X 9(12,10X),12,/,5X,10(10X,12))
C      WRITE(16,2112) NS,(SAVE(L,NS),L=1,20)
2112  FORMAT(1X,15,2X,10(G10.4,2X),/,11X,10(G10.3,2X))
C
C C FILL SECOND RECORD FOR THIS LEVEL
C      LNS = NS
C      NS = NS + 1
C      SAVE (1,NS) = SAVE (1,LNS) + 100.
C      SAVE (2,NS) = ALTIC
C      C ASSUME RADAR ERROR IS 20 M. +/- 10 M. (A. HOLLAND 4-19-83)
C      SAVE (3,NS) = 2./ ALTIC
C      SAVE (4,NS) = HOUR + 100*(AINT(SEC/60.)) + AMOD(SEC,60.)
C      SAVE (5,NS) = SMOOTH (5,LC,ISM)
C      SAVE (6,NS) = 100.* ((SAVE(16,LNS)/SAVE(10,LNS))*2 + 0.5E-4)**0.5
C      SAVE (7,NS) = ODENC
C      SAVE (8,NS) = ODENC * CONR
C      SAVE (9,NS) = UC / SECSZA(LC)
C      SAVE(10,NS) = CONR * SAVE(9,NS) * 1000.
C
C      IF (ISNDC.EQ. 0) GO TO 120
C      LISNDC = ISNDC
C      PALT = ALTIC
C      SAVE (11,NS) = SONDE(2,ISNDC)
C      SAVE (12,NS) = 100. * SONDE(5,ISNDC)/SONDE(2,ISNDC)
C      SAVE (13,NS) = SONDE(3,ISNDC)
C      C ASSUME 1.0 MBAR ERROR IN BASE PRESSURE.
C      SAVE (14,NS) = ((100./DSB(3))**2 + SAVE(12,NS)**2)**0.5
C      GO TO 140
C
C      IF (ISNDC.EQ. 0) GO TO 120
C      LISNDC = ISNDC
C      PALT = ALTIC
C      SAVE (11,NS) = SONDE(2,ISNDC)
C      SAVE (12,NS) = 100. * SONDE(5,ISNDC)/SONDE(2,ISNDC)
C      SAVE (13,NS) = SONDE(3,ISNDC)
C      C ASSUME 1.0 MBAR ERROR IN BASE PRESSURE.
C      SAVE (14,NS) = ((100./DSB(3))**2 + SAVE(12,NS)**2)**0.5
C      GO TO 140
C
C      C FIND AIR TEMPERATURE AND PRESSURE IN ECC NO. 1.
C
C      120 N = NECC(1)
C      DO 130 K = 1,N
C      I = NECC(1) - K + 1
C      Z1 = ECC (1,I,1)
C      IF (ALTIC.GT. Z1) GO TO 130
C      J = I - 1
C      Z2 = ECC (1,J,1)
C      GO TO 135
C      130 CONTINUE
C      135 RAT = (Z1-ALTIC) / (Z1-Z2)
C
C      C TEMPERATURE; ASSUME ERROR IS TWO DEGREES
C      SAVE(11,NS) = ECC(2,1,1) - (ECC(2,1,1)-ECC(2,J,1)) * RAT

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ORIGINAL 1-1-61
OF POOR QUALITY

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SAVE(12,NS) = 200./SAVE(11,NS)
C PRESSURE ; ERROR IS ASSUMED TO BE 0.7 MBAR
SAVE(13,NS) = EXP(ALOG(ECC(3,I,1)) -
X (ALOG(ECC(3,I,1)) - ALOG(ECC(3,J,1))) * RAT)
SAVE(14,NS) = 70. /SAVE(13,NS)
C STORE T,P,D IN SONDE FOR LATER USE
ISNDC = LISNDC + PALT - ALTC
SONDE(1,ISNDC) = ALTC
SONDE(2,ISNDC) = SAVE(11,NS)
SONDE(3,ISNDC) = SAVE(13,NS)
SONDE(4,ISNDC) = CONS*SONDE(3,ISNDC)/SONDE(2,ISNDC)
SONDE(5,ISNDC) = 2.0
C DERIVED UNITS
C
C 140 SAVE (15,NS) = COND * SAVE(13,NS)/SAVE(11,NS)
SAVE (16,NS) = ASLTC/SECSZA(LC)
SAVE (17,NS) = COMP * SAVE(11,NS) * SAVE(7,NS)
SAVE (18,NS) = SAVE(17,NS) / SAVE(13,NS)
SAVE (19,NS) = SEC
SAVE (20,NS) = NS

```

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=OZDENS

```
C *** TEST STATEMENTS
C WRITE(IMES,2110) (L,L=1,20)
C WRITE(IMES,2112) NS,(SAVE(L,NS),L=1,20)
C
C NEXT ALTITUDE LEVEL OR PLACE THIS FILTER'S PROFILE IN SMOOTH & ON
C TAPE.
  IF (ALFAC.LT. 0.3HALFTOP) BASE(IF) = ALTB
  IF (NS.EQ. 60) GO TO 150
  IF (ALTB.GT. BASE(IF)) GO TO 75
150 SAVE (20,NS) = -1.
  NSETS = NSETS + 1
  NBYTES = NS*20*4
  CALL CMOVE(SAVE(1,1),SMOOTH(1,1,ISM),NBYTES)
  NSAV = NS
  CALL TAPMRT(2,IMES)
C *** TEST STATEMENT
C CALL PRISAV(NS,IMES)
C
C READY TO LOOK FOR NEXT FILTER'S DATA
800 CONTINUE
  MCODE = 1
  GO TO 999
C
C ODDS AND ENDS
C
C PRESSURE DATA NOT AVAILABLE FOR COMPUTATION OF AIR MASS
C EXPLANATIONS GIVEN BY SLANTA WHERE MCODE IS SET TO -20
900 GO TO 999
C OZONE OVERBURDEN NOT FOUND IN MODEL (STD)
910 WRITE(IMES,2910) ALTT
2910 FORMAT ('OZDENS 2910: OZONE COLUMN NOT FOUND IN STD FOR ALT=',
XF6.0)
  MCODE = -21
C 999 RETURN
  END
```

*** END OF MEMBER *** 347 RECORDS PROCESSED *****

ORIGINAL PAGE 18
OF POOR QUALITY

ORIGINAL FILED
OF POOR QUALITY

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C MAIN - PROFILE
C REED/BATLUCK MARCH 1983
C PROFILE (1) ASSEMBLES THE ROCOZ OBSERVATIONS,CALIBRATIONS,CORREL-OBS.
C (SUBROUTINES CARDS, TAPE, INARRY)
C (2) COMPUTES DERIVED DATA
C (SUBROUTINES MODEL, DATSND, SECANG, OVRBRD, ALFEFF, SLANTA)
C (3) COMPUTES OZONE DENSITIES FROM THE ROCOZ ; EVALUATES ROCOZ RESULTS
C (SUBROUTINES OZDENS, COMPCH)
C (4) COMBINES ROCOZ 03 WITH CORREL OBS; PUTS RESULTS ON TAPE, PRINT,
C AND PLOT
C (SUBROUTINES RELATD, TAPHRT, PRTWRT, PLTWRT)
C
C REAL*8 TAPEIN, TAPOUT
C TAPE LOCATIONS, TAPE FILES, ALT. RANGE FOR EACH OF THE 4 FILTERS.
C COMMON/SETUP/ TAPEIN,TAPOUT,MFIN,MFOT,INCLD(7),TOP(7),BASE(7)
C
C DATA SONDE,ECC,AND MODEL PROFILES; DESCRIBED IN CARDS.
C COMMON/PROFLS/DSB(3),MXSND,NECC(2),ECCLM(3,2),SONDE(5,70),
C X ECC(4,19,2),STD(3,60)
C
C FILTER SHAPES AS GIVEN BY MCBRIDE, NWC, CHINA LAKE, CA.
C COMMON/FSHAPE/CH(7),BW(7),CMCBRD(4,7)
C
C MISCELLANEOUS CONSTANTS -
C COMMON/CONSTT/AVOGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,RZRO
C
C INPUT DATA FROM ROCOZ
C COMMON/DATIN/NLAYRS,SECSZA(60),SMOOTH(20,60,7)
C
C OUTPUT ARRAYS
C COMMON/DATOUT/ NSAV,PED(20,30),SAVE(20,60)
C DATA IMES/9/,IECHO/6/,ICHR/6/,ITBL/6/
C
C INITIALIZATION
C AVOGAD = 6.022169E26
C VOLSTP = 22.4136
C RSTAR = 8314.32
C DGTORD = 1.745329E-2
C GRV45 = 9.806160
C AIRM = 28.9644
C NCODE = 0
C NSAV = 0
C CALL CHOVE(NSAV,PED(1,1),7200)
C DSB(1) = 0.
C CALL CHOVE(DSB(1),DSB(2),2772)
C NLAYRS = 8
C CALL CHOVE(NLAYRS,SECSZA(1),33840)
C
C READ AND SETUP INPUT DATA
C CALL CARDS(NCODE,IMES,IECHO)
C 9 IF (NCODE) 905,10,10
C 10 CALL TAPE(NCODE,IMES)

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OF POOR QUALITY

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      IF (NCODE) 910,20,20
20  CALL MODEL(NCODE)
      C*** TEST STATEMENTS
      C      CALL PRTPRF(IMES)
      IF (NCODE) 915,30,30
30  CALL DATSND(PED(6,1),NCODE,IMES)
      C*** TEST STATEMENTS
      C      CALL PRTPRF(ITBL)
      IF (NCODE) 920,35,35
35  PED(11,7) = GRV
      PED(12,7) = RZRO
      C
      C      COMPUTE SECANT/CHAPMAN-FUNCTION FOR SOLAR ZENITH ANGLES
      CALL SECANG(IMES)
      C
      C
      C      COMPUTE AN OZONE PROFILE FOR EACH FILTER AND/OR FILTER RATIO.
      CALL OZDENS(NCODE,IMES,ITBL)
      IF (NCODE .LT. 0) GO TO 990
      CALL DATWRT(ITBL)
      C

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26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=PROFILE

COMPUTE COMPOSITE OZONE PROFILE BASED ON ROCOZ DATA.

CALL COMPT(NCODE,IMES)

IF (NCODE .LT. 0) GO TO 996

C

CHECK ROCOZ DATA FOR INTERNAL CONSISTENCY, COMPLETE COMPOSITE TABLE.

CALL CHECKS(NCODE,IMES,ICLK)

CALL CMPMRT(ITBL)

CALL RELATD(IMES)

CALL TP4MRT(ITBL)

CALL TP5MRT(ITBL)

CALL TAPMRT(3,IMES)

GO TO 990

C

ODDS AND ENDS

905 WRITE (6,2905)

2905 FORMAT ('OMAIN 2905: PROBLEM IN DATAS INPUT')

GO TO 990

910 WRITE (6,2910)

2910 FORMAT ('OMAIN 2910: PROBLEM WITH SMOOTH TAPE')

GO TO 990

915 WRITE (6,2915)

2915 FORMAT ('OMAIN 2915: PROBLEM IN MODEL')

GO TO 990

920 WRITE (6,2920)

2920 FORMAT ('OMAIN 2920: PROBLEM IN DATSND')

GO TO 990

990 WRITE (IMES,2990)

2990 FORMAT ('OMAIN 2990: PROGRAM END')

STOP

END

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*** END OF MEMBER ***

108 RECORDS PROCESSED

ORIGINAL
OF POOR Q

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=PRTPED

C *****
C SUBROUTINE PRTPED
C PROGRAMMER: S. COOKE
C
C PURPOSE: TO PRINT OUT THE VARIOUS PEDIGREE RECORDS
C THAT HAVE BEEN ESTABLISHED.
C *****
C
C SUBROUTINE PRTPED(ITBL)
C COMMON/DATOUT/ NSAV,PED(20,30),SAVE(20,60)
C
C WRITE(ITBL,2010) NSAV
C FORMAT(' PRTPED 2010: NSAV = ',I8)
C IF (NSAV .GT. 90) NSAV = 90
C DO 100 J = 1,NSAV
C IF (PED(1,J).EQ.-504. .OR. PED(1,J).EQ.-505.) GO TO 80
C IF (PED(1,J).LE.-504.) GO TO 90
C WRITE (ITBL,2000) (PED(I,J),I=1,20),PED(5,J),PED(6,J)
C IF (J.EQ.1.) WRITE(ITBL,2001) (PED(K,1),K=10,12)
C FORMAT ('+',I20X,3A4)
C GO TO 100
C 80 WRITE (ITBL,2080) (PED(1,J),I=1,20),PED(5,J),PED(6,J)
C 2080 FORMAT (1X,F5.0,10E12.3,/,2X,9E12.3,2X,A4,1X,A4)
C GO TO 100
C 90 WRITE(ITBL,2090) (PED(1,J),I=1,20)
C 2090 FORMAT(1X,F5.0,16A9,3F9.2)
C 100 CONTINUE
C 2000 FORMAT (1X,F5.0,10F12.3/
C X 2X,9F12.3,2X,2A4)
C RETURN
C END

*** END OF MEMBER *** 33 RECORDS PROCESSED *****

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ORIGINAL PAGE 18
OF POOR QUALITY

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SUBROUTINE PRTSAV(NS,IMES)
C
C COOKE, REED
C
C AUG 1983
C
C PRTSAV PRINTS OUT THE VALUES FOR THE 'SAVE' ARRAY AFTER EACH
C FILTER. (ARRAY IS PRINTED OUT IN COLUMN, ROW ORDER)
C
C COMMON/DATOUT/ NSAV,PED(20,30),SAVE(20,60)
C
C GO TO 200
C
C 50 WRITE (IMES,2100)
C
C 2100 FORMAT(/,5X,'PRTSAV 2100: SAVE = (IN COLUMN,ROW ORDER)')
C
C 2105 FORMAT(/,1X,'NS',7X,12,10X,12,8X,12,10X,12,9X,12,8X,12,10X,12,
C 12X,12,10X,12,9X,12,10X,12,10X,12,9X,12,8X,12,10X,
C 12,12X,12,10X,12,9X,12,/)
C
C DO 100 J = 1,NS,2
C
C L = J + 1
C
C PRINT OUT THE ODD NUMBERED ARRAYS
C
C WRITE (IMES,2110) J,(SAVE(I,J),I=1,20)
C
C 2110 FORMATT(1X,12,7X,F4.0,8X,F3.0,5X,F6.1,6X,F6.3,5X,F6.1,2X,G10.4,2X,
C 10X,4,6X,F6.1,6X,F6.3,2X,G10.4,
C 10X,F4.0,2X,G9.3,5X,F6.3,3X,G9.3,2(2X,G9.3),7X,F5.2,2X,G10.3,
C 3X,F9.3,7X,F5.1)
C
C PRINT OUT THE EVEN NUMBERED ARRAYS
C
C WRITE (IMES,2210) L,(SAVE(I,L),I=1,20)
C
C 2210 FORMATT(1X,12,7X,F4.0,8X,F3.0,2X,G9.4,2X,G10.4,6X,F5.2,6X,F6.3,
C 3X,G9.4,3(2X,G10.4),
C 10X,F4.0,6X,F5.2,5X,F6.3,7X,F5.2,2X,G9.3,3(3X,G9.3),7X,F5.0,7X,
C F5.1)
C
C 100 CONTINUE
C
C 200 FILTER = SAVE(1,1) - 100.
C
C WRITE (IMES,2300) FILTER
C
C 2300 FORMATT('IPRTSAVE 2300: DATA FROM FILTER ',F3.0/)
C
C WRITE (IMES,2301)
C
C 2301 FORMATT('ALT HRX NMMSS.S SZA OZRX ATM-CM/KM OZ NUM/M3 OZATM-',
C 1X,'CM OZNUM/M2 AIRK TRX AIR MBAR PRX AIRNUM/M3 AIRCOLUM ',
C 1X,'OZ MBAR VOL MXR SEC')
C
C DO 300 I = 2,60,2
C
C WRITE (IMES,2302) (SAVE(J,I),J=2,19)
C
C 2302 FORMATT(1X,F3.0,F4.1,F9.1,F5.1,F5.1,1X,G9.4,1X,G9.4,1X,G8.3,1X,
C 1X,G8.3,F5.0,F4.1,1X,F9.5,F4.1,1X,G9.4,1X,G8.3,1X,G9.4,1X,G8.3,F6.0)
C
C IF (SAVE(20,I) .LE. 0.) GO TO 310
C
C 300 CONTINUE
C
C 10 WRITE (IMES,2311)
C
C 2311 FORMATT('OALT COMP SCNT CNT/RAT SLANTOZ SLNTAR ALFAEFF BETAF ',
C 1X,'DLNIDH DALFUD DAIR/DH TAUZ TAUAR FRASER NOISE DH',
C 1X,'BSMOOTH STDEV PHTMP')
C
C DO 320 I = 1,59,2
C
C WRITE (IMES,2312) (SAVE(J,I),J=2,20)
C
C 2312 FORMATT(1X,F3.0,F5.0,F5.2,F8.3,1X,G8.3,1X,G8.3,1X,G7.2,F8.3,F6.3,F9.5,1X,
C 1X,G6.2,1X,G7.2,F5.2,F6.3,1X,F8.3,1X,F8.3,F4.1,F8.5,F8.5,F5.0)
C
C IF (SAVE(20,I+1) .LE. 0.) GO TO 999
C
C 320 CONTINUE

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999 RETURN
END

*** END OF MEMBER ***

58 RECORDS PROCESSED

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ORIGINAL PAGE
OF POOR COPY X

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C *****
C SUBROUTINE PRYSMT(NLAYRS,IMES)
C REED/BATLUCK/COOKE      JUNE 1983
C ARGUMENTS
C N      NUMBER OF HEIGHT LEVELS
C IMES   OUTPUT TAPE UNIT NUMBER
C *****
C DIMENSION ARR(6), BRR(15)
C COMMON/DATAIN/NLAYRS,SECSZA(60),SMOOTH(20,60,7)
C PRINT COMMON PARAMETERS
C WRITE(IMES,2000)
C DO 20 J = 1,NLAYRS
C   ARR(1) = SMOOTH(2,J,1)
C   ARR(2) = SMOOTH(6,J,1)
C   ARR(3) = SMOOTH(5,J,1)
C   ARR(4) = SMOOTH(7,J,1)
C   ARR(5) = SMOOTH(8,J,1)
C   ARR(6) = SMOOTH(9,J,1)
C   WRITE(IMES,2010)ARR
C 20 CONTINUE
C PRINT DATA FOR EACH FILTER: S3,S2,S1 AND S0
C
C DO 50 KF = 1,7
C   K=KF
C   NEIL = SMOOTH(1,1,K)
C   WRITE(IMES,2050) NEIL
C   IF(NFIL.GT.5) WRITE(IMES,2051)
C   WRITE(IMES,2060)
C   DO 50 J = 1,NLAYRS
C     BRR(1) = SMOOTH(2,J,K)
C     BRR(2) = SMOOTH(3,J,K)
C     BRR(3) = SMOOTH(4,J,K)
C     BRR(12) = SMOOTH(11,J,K)
C     BRR(13) = SMOOTH(12,J,K)
C     BRR(7) = SMOOTH(14,J,K)
C     BRR(9) = EXP(SMOOTH(15,J,K))
C     IF(BRR(9).NE.0.) BRR(9)=(BRR(9)-1.)*100.
C     BRR(8) = (BRR(9)*BRR(7))*0.01
C     BRR(10) = SMOOTH(16,J,K)
C     BRR(11) = SMOOTH(17,J,K)
C     IF (BRR(3).NE.0.) GO TO 30
C     BRR(4) = SMOOTH(18,J,K)
C     BRR(5) = 100.0
C     IF(BRR(2).NE.0.) BRR(5)=100.*BRR(4)/ABS(BRR(2))
C     GO TO 40
C   30 BRR(5) = (SMOOTH(18,J,K)-1.)*100.
C   40 BRR(4) = BRR(5)*BRR(2)/100.
C   40 BRR(6) = SMOOTH(19,J,K)
C   BRR(14) = SMOOTH(13,J,K)
C   BRR(15) = SMOOTH(20,J,K)
C   50 WRITE(IMES,2070) BRR

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00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700
00000710
00000720
00000730

RETURN
2000 FORMAT(0,'ALT-KM SECONDS SZA TMP C CYCLE BATTV')
2010 FORMAT(1X,F6.0,F8.1,F7.2,F7.1,F7.3,F6.2)
2050 FORMAT(/,1X,'FILTER POSITION',13)
2051 FORMAT(+,20X,'(DIVIDED BY 50)')
2060 FORMAT(1X,'KM',3X,'CNT/RAT',4X,'SLOPE',3X,'SDCNT',3X,'SD X',
X3X,'COREL',3X,'END 10',2X,'DIOCNT',2X,'DIO X',3X,'ABSORP',
X4X,'DABSP',3X,'START',3X,'END',3X,'USD',3X,'PTS',/)
2070 FORMAT(1X,F3.0,3X,F8.3,2X,F8.3,2X,F7.4,2X,F5.2,3X,F8.3,2X,
X F6.4,3X,F5.2,3X,F7.3,3X,F6.3,3X,F5.2,3X,F5.0,1X,F5.0)
END

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*** END OF MEMBER *** 67 RECORDS PROCESSED *****

ORIGINAL PAGE 15
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26JUL84 08.53.47 - VOL=SACC10, DSN=13EIR.PROF.CNTL

MEMBER=PRTHRT

ORIGINAL PAGE 18
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SUBROUTINE PRTHRT(ITBL)
C REED, BATLUCK, AND COOKE
C PRTHRT DISPLAYS THE OZONE PROFILES AS TABLES,
C 1. FLIGHT PARAMETERS
C 2. OZONE VALUES FOR EACH FILTER AT EACH KM. ALTITUDE
C 3. COMPOSITE OZONE PROFILE -VS KM
C 4. OZONE CONTENT OF 12 STANDARD PRESSURE LEVELS
C 5. OZONE VALUES AT STANDARD PRESSURE LEVELS.
C NOTE THAT SMOOTH NOW CONTAINS THE 1XX. AND 2XX. RECORDS FROM OZDENS.
C
LOGICAL RTRN
DIMENSION I(11),TA(15),IB(17),TC(18),TD(8)
COMMON/DATAIN/NLAYRS,SECSZA(60),SMOOTH(20,60,7)
COMMON/DATOUT/NSAV,NDXTOP,NDXBAS,NLVLS,DM(10),DOSTM,DOBAM,DOBPM,
X PMDL(2),ECTIE,ECCOL,COMP(20,70),TYP4(40),TYP5(10,34)
EQUIVALENCE (T(1),TA(1),IB(1),TC(1),TD(1))
C
RTRN = .FALSE.
GO TO 10
C
ENTRY DATMRT(ITBL)
RTRN = .TRUE.
C (1) TABLE OF FLIGHT PARAMETERS:
C
10 WRITE (ITBL,2010) NDXBAS,(DM(1),I=1,4),(DM(J),J=7,10)
2010 FORMAT('1',ROCO,FLIGHT NO.,F6.1,' FLOWN',F8.0,'(MDDYY.)',F10.1,
X,'(HHMMSS.S)'/,' AT ',F7.3,' LAT',F9.3,' LONG. ',F4.4//)
WRITE (ITBL,2011)
2011 FORMAT('0',ALT-KM ERZ Z-HMMSS.S SZA-DEG SZA-SEC SLNT-ATM SCAT',
X' CMPX AIR T-K ERR-K AIR P-MBAR INSTR TMP-C'//)
T(1) = 100
DO 40 J = 1,4
DO 30 I = 1,60,2
IF (SMOOTH(1,I,J).LT.20.) GO TO 40
IF (SMOOTH(2,I,J).GE. T(1)) GO TO 30
T(1) = SMOOTH(2,I,J)
T(2) = SMOOTH(3,I+1,J)
T(3) = SMOOTH(4,I+1,J)
T(4) = SMOOTH(5,I+1,J)
T(5) = SMOOTH(4,I,J)
T(6) = SMOOTH(7,I,J)
T(7) = 100. * SMOOTH(15,I,J)
T(8) = SMOOTH(11,I+1,J)
T(9) = 0.01 * SMOOTH(12,I+1,J) * T(8)
T(10) = SMOOTH(13,I+1,J)
T(11) = SMOOTH(20,I,J)
WRITE (ITBL,2030) T
2030 FORMAT('1X,F5.0,F5.2,F10.1,F8.2,F8.4,F9.5,F9.3,F8.2,F6.2,F11.6,
X F12.1)
30 CONTINUE
40 CONTINUE
C

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C (2) OZONE PROFILE AS DERIVED FROM EACH FILTER.
C (A) INTERMEDIATE VALUES USED IN THE OZONE COMPUTATIONS.
C (B) OZONE VALUES WITH AIR TEMP AND PRESSURE.
DO 80 J = 1,7
  IF (SMOOTH(1,1,J).LT.20.) GO TO 80
  IFILTR = SMOOTH(1,1,J) - 100.
  IRATIO = 0
  IF (IFILTR .LT. 10) GO TO 45
  IRATIO = 1
  IFILTR = IFILTR / 10
  WRITE(ITB,2040)
  FORMAT('1')
  WRITE (ITBL,2045) IFILTR
2045 FORMAT ('0', 'DATA FOR FILTER POSITION S', I1)
  IF (IRATIO .EQ. 1) WRITE (ITBL,2046)
2046 FORMAT ('+', 27X, ' DIVIDED BY 50')
  WRITE (ITBL,2047)
2047 FORMAT('0', 'ALT INTENSITY DLI/DH NOISE SLNTO SLNTA ALPHA-F',
X, ' BET-F DA/DSLO DSLA/DH O3TAU AIRTAU COMP SCATZ B(SMTH) BSTDV',
X, ' BDH')
2048 FORMAT (1X,F3.0,F10.4,2X,F7.4,F7.4,2X,F6.5,1X,F6.5,F8.3,F6.3,1X,
00000500
00000510
00000520
00000530
00000540
00000550
00000560
00000570
00000580
00000590
00000592
00000594
00000600
00000610
00000620
00000630
00000640
00000650
00000660
00000662
00000670

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X F8.4,F7.4,F7.3,F6.3,F6.0,F6.3,F9.4,F7.4,F6.2)

N = 0

DO 50 I = 1,59.2

TB(1) = SMOOTH(2,I,J)

TB(2) = SMOOTH(5,I,J)

TB(3) = SMOOTH(10,I,J)

TB(4) = SMOOTH(16,I,J)

TB(5) = SMOOTH(6,I,J)

TB(6) = SMOOTH(7,I,J)

TB(7) = SMOOTH(8,I,J)

TB(8) = SMOOTH(9,I,J)

TB(9) = SMOOTH(11,I,J)

TB(10) = SMOOTH(12,I,J)

TB(11) = SMOOTH(13,I,J)

TB(12) = SMOOTH(14,I,J)

TB(13) = SMOOTH(3,I,J)

TB(14) = SMOOTH(15,I,J) * 100.

TB(15) = SMOOTH(18,I,J)

TB(16) = SMOOTH(19,I,J)

TB(17) = SMOOTH(17,I,J)

WRITE (ITBL,2048) TB

N = N+2

IF (SMOOTH(20,I+1,J).LE.0.) GO TO 52

CONTINUE

C PREPARE THE TABLES OF OZONE AND AIR PARAMETERS

50

DO 60 K = 2,N,2

TA(1) = SMOOTH(2,K,J)

TA(2) = SMOOTH(4,K,J)

TA(3) = SMOOTH(7,K,J)

TA(4) = SMOOTH(8,K,J)

TA(5) = SMOOTH(6,K,J)

TA(6) = SMOOTH(9,K,J)

TA(7) = SMOOTH(10,K,J)

TA(8) = SMOOTH(11,K,J)

TA(9) = SMOOTH(12,K,J)

TA(10) = SMOOTH(13,K,J)

TA(11) = SMOOTH(14,K,J)

TA(12) = SMOOTH(15,K,J)

TA(13) = SMOOTH(16,K,J)

TA(14) = SMOOTH(17,K,J)

TA(15) = SMOOTH(18,K,J)

IF (K.NE.2) GO TO 55

WRITE (ITBL,2045) IFILTR

IF (IRATIO.EQ. 1) WRITE (ITBL,2046)

WRITE (ITBL,2049)

2049 FORMAT ('0', 'ALT HMMSS.S 03ATM-CM/KM NUM/M3 ERRX COL-ATM-',

X 'CM NUM/M2 AIR-T-K ERX AIR-P-MBAR ERX AIR-N/M3 AIR-COL',

X 'ATM 03-NANOBAR PPMV'/)

2050 FORMAT (1X,F4.0,F9.1,1X,F10.6,1X,E10.4,F5.1,1X,F10.6,1X,E10.4,1X,

X F7.2,F4.1,1X,F10.5,F4.1,1X,E10.4,2X,F10.6,1X,F10.5,F6.2)

55 CONTINUE

60 CONTINUE

80 CONTINUE

IF (RTRH) GO TO 150

GO TO 90

ENTRY CNPMT(ITBL)

00000680
00000690
00000700
00000710
00000720
00000730
00000740
00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820
00000830
00000840
00000850
00000860
00000870
00000880
00000890
00000892
00000902
00000910
00000920
00000930
00000940
00000950
00000960
00000970
00000980
00000990
00010000
00010100
00010200
00010300
00010400
00010500
00010600
00010700
00010800
00010900
00011000
00011100
00011200
00011300
00011400
00011500
00011600
00011700
00012000
00012100
00012110
00012120
00012140
00012160
00012180

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C
C (3) COMPOSITE PROFILE - AT INTEGER ALT. LEVELS
  90 WRITE (ITBL,2010) DM(5),(DM(I),I=1,4),(DM(J),J=7,10)
  WRITE (ITBL,2090)
  2090 FORMAT ('0',: OZONE PROFILE BASED ON ALL AVAILABLE ROCOZ DATA',
X ' ALT ATM-CM/KM 03 NUM/H3 ERRX COL ATM-CM ERRX AIR T K ERRX ',
X ' AIR P MBAR ERRX 03 MANOBAR ERRX PPMV ERRX HHMMSS.S SECONDS',
X ' FL SZA',/)
      DO 100 I = NDXTOP,NDXBAS
      CALL CMOVE (COMP(2,1),TC(1),72)
      WRITE (ITBL,2100) TC
  2100 FORMAT (1X,F3.0,E11.4,E11.4,F5.1,F11.6,F5.1,F8.1,F5.1,F11.4,
X F5.1,F12.3,F5.1,F7.2,F5.1,F9.1,F7.0,F3.0,F6.2)
  100 CONTINUE
      IF (RTRN) GO TO 150
      GO TO 105
C
      ENTRY TP4MRT(ITBL)
      RTRN = .TRUE.
C

```

00001219
00001220
00001230
00001240
00001250
00001260
00001270
00001280
00001290
00001300
00001310
00001320
00001330
00001340
00001350
00001352
00001354
00001356
00001358
00001359
00001360

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=PRTHWT

```
C (4) OZONE VALUES OF 12 STANDARD PRESSURE LEVELS.
C
C 105 CONTINUE
C WRITE (ITBL,2010) DM(5),(DM(1),I=1,4),(DM(J),J=7,10)
C WRITE (ITBL,2110)
C 2110 FORMAT (// 'O LAYER BOUNDARIES OZONE CONTENT')
C WRITE (ITBL,2113)
C TYP4(21) = TYP4(23)
C DO 120 I = 3,27,2
C IF (I.EQ.21) GO TO 120
C WRITE (ITBL,2112) TYP4(I),TYP4(I+2),TYP4(I+1)
C 2112 FORMAT (IX,F7.3,'--',F8.3,6X,F8.3)
C 120 CONTINUE
C 2113 FORMAT (6X,'MILLIATM',8X,'MILLIATM-CM')
C IF (RTRN) GO TO 150
C GO TO 130
C
C ENTRY TP5WRT(ITBL)
C
C (5) OZONE VALUES AT STANDARD PRESSURE LEVELS
C
C 130 WRITE (ITBL,2010) DM(5),(DM(1),I=1,4),(DM(J),J=7,10)
C WRITE (ITBL,2130)
C 2130 FORMAT ('OZONE FROM THE COMPOSITE PROFILE AND ECC PROFILE AT',
C X ' STANDARD PRESSURE LEVELS','OPRESSURE ALTITUDE AIR TEMP',
C X 'ROCOZ O3 ROCOZ O3 ECC AIR ECC O3 ECC O3',
C X 'KM K NUM/M3 MRMASS TEMP K NUM/M3 MRMASS')
C DO 140 I = 1,33
C IF (TYP5(I,I)).LT. 499.) GO TO 150
C CALL CHOVE (TYP5(3,I),TD(I),32)
C WRITE (ITBL,2131) TD
C 2131 FORMAT (IX,F8.2,F9.3,F8.1,E12.3,F9.3,F8.1,E11.3,F7.3)
C 140 CONTINUE
C COMPLETED DISPLAYS
C 150 RETURN
C
C END
```

*** END OF MEMBER *** 191 RECORDS PROCESSED *****

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SUBROUTINE RELATD(IMES)
C CONVERT TO MILLI ATM-CM.
C REED, BATLUCK, AND COOKE
C
C RELATED COMPLETES THE PREPARATION OF COMPOSITE DATA RECORDS, LOCATED
C IN COMP (COMMON/DATOUT/) AND NEW RECORDS OF TYPES 400 AND 500 TO
C EXPRESS THE DATA IN UNITS MORE CONVENIENT FOR SOME USERS, NAMELY,
C OZONE CONTENT IN TWELVE STANDARD PRESSURE LAYERS, AND OZONE VALUES AT
C 33 STANDARD PRESSURE LEVELS, USING ROCOZ DATA, SUPPLEMENTED BY ECC
C DATA AT THE LOWER LEVELS.
C
C THE CONTENTS OF COMMON/DATOUT/ ARE RENAMED TO CORRESPOND TO THEIR
C USAGE IN THIS SUBROUTINE.
C
    DIMENSION PLS(33)
    COMMON/PROFLS/DSB(3),MXSHD,NECC(2),ECCLM(3,2),SONDE(5,70),
    X ECC(4,19,2),STD(3,60)
    COMMON/DATAIN/NLAYS,SECSZA(60),SMOOTH(20,60,7)
    COMMON/DATOUT/NSAV,NDXTOP,NDXBAS,NLVLS,DM(10),DOB(3),PMDL(2),
    X ECTIE,ECCOL,COMP(20,70),TYP4(40),TYP5(10,34)
    COMMON/CONSTI/AVOGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,RZRO
    DATA PLS/0.05,0.07,0.10,0.15,0.20,0.30,0.40,0.50,0.70,1.1,1.5,2.,
    X 3.4,5.7,10.,15.,20.,30.,40.,50.,70.,100.,150.,200.,250.,300.,
    X 400.,500.,700.,850.,1000./
C
C INITIALIZE TYP4 AND TYP5 TO 0.0
C PLACE LAYER BOUNDARIES (MILLIATMOSPHERES) IN TYP4
    TYP4(1) = 0.0
    CALL CHOVE (TYP4(1),TYP4(2),1516)
    TYP4(1) = 400.
    TYP4(2) = 1.
    TYP4(5) = 250./1024.
    DO 54 I = 7,25,2
    54 TYP4(I) = TYP4(I-2) * 2.
C FIND ROCOZ OVERBURDEN AT UPPER BOUNDARY OF EACH LAYER
C TO CONVERT HBAR TO MATM, DIVIDE HBAR BY 1.01325
    RPATM = COMP(10,NDXTOP) / 1.01325
    DO 58 I = 5,19,2
    L = I
    IF (TYP4(L) .GE. RPATM) GO TO 60
    58 CONTINUE
C
    60 TPMB = TYP4(L) * 1.01325
    DO 64 I = NDXTOP,NDXBAS
    N = I
    IF (TPMB - COMP(10,N+1)) 68,66,64
    64 CONTINUE
    GO TO 70
    66 TYP4(L+1) = COMP(10,N)
    GO TO 69
C
    68 IF (N .EQ. NDXBAS) GO TO 70
    TYP4(L+1) = COMP(6,N+1)+(TPMB-COMP(10,N+1))
    X / (COMP(10,N)-COMP(10,N+1))
    69 L = L + 2
    GO TO 60

```

```

C COMPUTE LAYER CONTENTS
70 DO 74 I = 4,24,2
  IF (TYP4(I).EQ.0.) OR. TYP4(I+2).EQ.0.) GO TO 74
  TYP4(I) = (TYP4(I+2) - TYP4(I)) * 1000.
  N = I
74 CONTINUE
  TYP4(N+2) = 0.0
  C ADD DATA FROM ECC SONDE, ESTIMATE OZONE CONTENT IN STD PRESS LAYERS
  TYP4(24) = (ECCLM(3,1) - ECCLM(2,1)) * 1013.25
  TYP4(26) = (ECCLM(2,1) - ECCLM(1,1)) * 1013.25
  TYP4(28) = (ECCLM(1,1)) * 1013.25
  C MOVE DATA AND CREATE 2ND RECORD
  TYP4(29) = 1000.
  TYP4(27) = 250.
  TYP4(25) = 125.
  TYP4(23) = 62.5
  IF (TYP4(22).NE.0.) TYP4(24) = TYP4(22)
  TYP4(22) = 2.
  TYP4(21) = 400.
  C *** TEST STATEMENT
  C CALL TP4WRT(IMES)
00000585
00000590
00000595
00000600
00000605
00000610
00000615
00000620
00000625
00000630
00000635
00000640
00000645
00000650
00000655
00000660
00000662
00000664
00000666
00000668
00000669

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26JUL84 08.53.47 - P22=SACC10, DSN=LEIR.PROF.CNTL

MEMBER=RELATD

```
C CREATE RECORDS GIVING DATA AT STANDARD PRESSURE LEVELS.
NC = 0
NC = MDXTOP
CON = 1.E-3 * AVOGAD/RSTAR
DO 100 IP = 1,33
N = N+1
TYP5(1,N) = 500.
TYP5(2,N) = N
TYP5(3,N) = PLS(IP)
IF (PLS(IP).LT.COMP(10,NC)) GO TO 100
86 IF ((NC+1).GT.NDXBAS) GO TO 91
IF (PLS(IP).LT.COMP(10,NC+1)) GO TO 90
NC = NC + 1
GO TO 86
90 FRAC = ALOG(PLS(IP)/COMP(10,NC))/ALOG(COMP(10,NC+1)/COMP(10,NC))
TYP5(4,N) = COMP(2,NC) + FRAC * (COMP(2,NC+1)-COMP(2,NC))
TYP5(5,N) = COMP(8,NC) + FRAC*(COMP(8,NC+1)-COMP(8,NC))
FRAC1 = (PLS(IP)-COMP(10,NC))/(COMP(10,NC+1)-COMP(10,NC))
TYP5(6,N) = COMP(4,NC) + FRAC1*(COMP(4,NC+1)-COMP(4,NC))
TYP5(7,N) = 1.65714 * (COMP(14,NC)+FRAC*(COMP(14,NC+1)-COMP(14,NC)
X))
C FIND ECC DATA FOR THIS RECORD
91 IF (IP.LT.17) GO TO 100
NE = 36 - IP
IF (NE.LE.16) NE = NE - 1
IF (NE.LE.12) NE = NE - 1
IF (ECC(4,NE,1).EQ.0.) GO TO 100
TYP5(8,N) = ECC(2,NE,1)
TYP5(9,N) = (CON * ECC(4,NE,1)) / ECC(2,NE,1)
TYP5(10,N) = 1.65714 * ECC(4,NE,1)/ECC(3,NE,1)
IF (TYP5(4,N).EQ.0.0) TYP5(4,N) = ECC(1,NE,1)
100 CONTINUE
C *** TEST STATEMENT
C *** CALL IPSHRT(INES)
C ALL TYP5 RECORDS COMPLETE
RETURN
END
```

*** END OF MEMBER *** 116 RECORDS PROCESSED

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SUBROUTINE SECANG(IMES)
C REED, BATLUCK, AND COOKE      MAR 83
C SECANG COMPUTES THE SECANT OR THE CHAPMAN FUNCTION FOR THE SOLAR
C ZENITH ANGLE.
C REF: CHAPMAN, S., PROC. PHYS. SOC. (LONDON), 43, 483-501, 1931
C CHAPMAN, S., PROC. PHYS. SOC. (LONDON), 66, 710-712, 1953
C MCCARTNEY, E.V., OPTICS OF THE ATMOSPHERE, J. WILEY, 1967, PP 109-13.
C FITZMAURICE, J.A., APPL. OPT. 3, 640, 1964.
C SERIES EXPANSION IS FROM K. KLENK, SYS. & APPL. SCI. CORP.
C SCALE HEIGHT IS FOR OZONE ABOVE 40 KM.

DIMENSION A(5)
COMMON/CONST/AVOGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,RZRO
COMMON/DATAIM/NLAYRS,SECSZA(60),SMOOTH(20,60,7)
DATA P/0.327591, A/1.061405, -1.453152, 1.421413, -0.284496, 0.254829,
X,SH /5.0,PI/3.141593/

DO 100 I = 1,NLAYRS
  ANG = SMOOTH(5,I,1)
  IF (ANG.GT. 86.) GO TO 80
  CZ = COS(ANG*DGTORD)
  IF (CZ.LT. 0.5) GO TO 20
  SECSZA(I) = 1./CZ
C *** TEST STATEMENTS
C WRITE (IMES,2000) I,ANG,SECSZA(I)
C2000 FORMAT (1X,12.3X,' ANGLE: ',F7.3,' SECSZA: ',F7.3)
  GO TO 100

C AT SOLAR ZENITH ANGLES GREATER THAN 60 DEG., USE CHAPMAN FUNCTION
C ARBITRARILY USE SCALE HEIGHT = 5; SUITABLE FOR OZONE ABOVE ABOUT 40
  20 R = (RZRO + SMOOTH(2,I,1))/SH
  X = CZ * SQRT(R*0.5)
  IF (CZ.GE. 0.2) GO TO 40
  C FOR SZA GREATER THAN 78.45 DEGREES
  T = 1./(1.+P*X)
  SUM = 0
  DO 22 J=1,5
    22 SUM = T * (A(J)+SUM)
  SECSZA(I) = SUM * SQRT(R*0.5*PI)
C *** TEST STATEMENTS
C WRITE (IMES,2000) I,ANG,SECSZA(I)
  GO TO 100

C FOR ANGLES BETWEEN 60 AND 78 DEGREES
  40 T = 0.5/(X*R*X)
  SECSZA(I) = (1.-T*(1.-3.*T*(1.-5.*T)))/CZ
C *** TEST STATEMENTS
C WRITE (IMES,2000) I,ANG,SECSZA(I)
  GO TO 100

C 80 WRITE (IMES,2000) SMOOTH(2,I,1), ANG
C2000 FORMAT ('OSECANG 2080: SOLAR ZENITH ANGLE AT',F4.0,' KM IS',F6.1,
X' SEC SZA IS ARBITRARILY SET TO 15.')
  SECSZA(I) = 15.

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C      100 CONTINUE
C
      DO 150 I=1,NLAYRS
      150 IF (SECSZA(I) .GT. 2.7) GO TO 160
      GO TO 900
C SCALE HEIGHT FOR AIR IS 6-10 KM AND SHOULD BE COMPUTED FROM
C DATASONDE PROFILE
      160 WRITE (TIMES,2160)
      2160 FORMAT ('SECANG 2160: WARNING: FOR SZA GT 69 DEGREES, THE SECANT',
      X,' FOR AIR MAY BE MORE THAN 1 x SMALLER THAN FOR OZONE,')
C
C      900 RETURN
      END

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END OF MEMBER XXXX 71 RECORDS PROCESSED

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=SHAPE

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C SUBROUTINE SHAPE(NF, FILTER, LMA, LMB, IMES, NCODE)
C REED, BATLUCK, COOKE                JUNE 1983
C SHAPE SELECTS THE DATA FILE FOR THE REQUESTED FILTER AND RETURNS THE
C   MEASURED TRANSMISSION.
C ARGUMENTS
C NF      THE FILTER NUMBER 1-4 CORRESPONDS TO S3, S2, S1, S0.
C FILTER  ARRAY CONTAINING PROVIDED FILTER TRANSMISSIONS.
C IMES    UNIT NUMBER FOR MESSAGES.
C LMA     INDEX OF SHORT WAVELENGTH
C LMB     START OF FILTER TRANSMISSION
C NCODE   INDEX OF LONG WAVELENGTH
C         END
C NCODE   IF NO DATA ARE AVAILABLE. FILTER CONTAINS 0.0.
C
C   DIMENSION FILTER(1000)
C   FILTER(1) = 0.
C   CALL CMOVE (FILTER(1), FILTER(2), 3996)
C NO MEASURED DATA AVAILABLE.
C 900 WRITE (IMES, 2900) NF
C 2900 FORMAT('0SHAPE 2900: NO TRANSMISSION DATA AVAILABLE FOR FILTER',
C           X 13)
C NCODE = -15
C RETURN
C END
```

*** END OF MEMBER *** 27 RECORDS PROCESSED *****

ORIGINAL FILED
OF POOR QUALITY

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SUBROUTINE SLANTA(LT,LC,LB,ALTT,ALTC,ALTB,ASLTT,ASLTC,ASLTB,DMDHC,
X ISNDC,NCODE,IMES)
C REED, BATLUCK, COOKE          APRIL 1983
C SLANTA OBTAINS THE SLANT AIR MASS IN ATMOSPHERES FOR THE THREE LAYERS
C UNDER CONSIDERATION. THE NUMBER OF ATMOSPHERES IN A COLUMN ABOVE A
C GIVEN LEVEL IS THE PRESSURE AT THAT LEVEL DIVIDED BY STANDARD
C ATMOSPHERIC PRESSURE, ADJUSTED FOR CHANGE IN GRAVITY. FROM
C U.S. STD. 1976, P0 = 1013.25 MBAR AND CORRESPONDING G = 9.80665
C M/S**2.
C
C ARGUMENTS
C LT,LC,LB = INDEX OF LEVELS UNDER CONSIDERATION - SECSZA ARRAY
C ALTT, ALTC, ALTB = ALTITUDES UNDER CONSIDERATION
C ASLTT, ASLTC, ASLTB = SLANT AIR MASS, IN ATMOSPHERES
C DMDHC = RATE OF CHANGE OF SLANT AIR MASS AT ALTITUDE C, IN ATM/KM
C ISNDC = INDEX IN SONDE FOR ALTC
C NCODE = -20 PRESSURE DATA ARE NOT AVAILABLE AT DESIRED LEVELS.
C
C LOGICAL NOT
C COMMON/PROFSL/DSB(3),MXSND,NECC(2),ECCLM(3,2),SONDE(5,70),
X ECC(4,19,2),STD(3,60)
C COMMON/DATAIN/NLAYRS,SECSZA(60),SMOOTH(20,60,7)
C
C COMMON/CONST/AVGAD,VOLSTP,RSTAR,DGTORD,GRV45,AIRM,GRV,RZRO
C
C COLUMN(P1,P2,Z) = CON * EXP(ALOG(P1)-(ALOG(P1)-ALOG(P2)) * (Z1-Z)/
* (Z1-Z2))
C NOT (SLT,Z) = (SLT,NE.0..OR. Z.GT.Z1 .OR. Z.LT.Z2)
C CON = 9.80665/(GRV*1013.25)
C TO CONVERT FROM KG/M3 PER M TO ATM PER KM
C CONM = 1000./10332.
C ISNDC = 0
C IF (SONDE(1,1) .LT. ALTT) GO TO 900
C ASLTT = 0.0
C ALTC = 0.0
C ASLTB = 0.0
C FIND DESIRED LEVELS IN SONDE; COMPUTE SLANT AIR MASS.
DO 100 I=1,MXSND
  ALT = SONDE(1,I)
  PRS = SONDE(3,I)
  IF (ALT .GT. ALTT) GO TO 100
  IF (ALT .EQ. ALTT) ASLTT = SECSZA(LT) * PRS * CON
  IF (ALT .NE. ALTC) GO TO 80
  IF (ALT .NE. ALTB) GO TO 80
  ASLTC = SECSZA(LC) * PRS * CON
  DMDHC = SECSZA(LC) * SONDE(4,I) * CONM
  ISNDC = I
  GO TO 100
80 IF (ALT .EQ. ALTB) ASLTB = SECSZA(LB) * PRS * CON
  IF (ALT .LT. ALTB) GO TO 110
100 CONTINUE
110 IF (ASLTB .NE. 0.0) GO TO 999
C
C
C

```

C INTERPOLATE AT DESIRED ALTITUDES AND COMPUTE SLANT AIR MASS.
C

```

N = NECC(1)
DO 200 J=1,N
  I = NECC(1) - J + 1
  Z1 = ECC(1,I,1)
  Z2 = ECC(1,I-1,1)

```

C

```

  IF (NOT(ASLTT,ALTT)) GO TO 120
  ASLTT = SECSZA(I) * COLUMN(ECC(3,I,1),ECC(3,I+1,1),ALTT)
120 IF (NOT(ASLTC,ALTC)) GO TO 140
  ASLTC = SECSZA(I) * COLUMN(ECC(3,I,1),ECC(3,I+1,1),ALTC)
  TEMP = ECC(2,I,1) - (ECC(2,I,1)-ECC(2,I+1,1)) *
    X (ECC(1,I,1)-ALTC) / (ECC(1,I,1)-ECC(1,I+1,1))
  DMDHC = AIRM * ASLTC * GRV * 103.41 / (RSTAR*TEMP)
140 IF (NOT(ASLTB,ALTB)) GO TO 200
  ASLTB = SECSZA(I) * COLUMN(ECC(3,I,1),ECC(3,I+1,1),ALTB)

```

C

```

GO TO 999

```

C

```

200 CONTINUE

```

```

00000490
00000500
00000502
00000510
00000514
00000520
00000530
00000540
00000550
00000560
00000580
00000590
00000600
00000610
00000620
00000630
00000640
00000650
00000660
00000670
00000680

```

26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=SLANTA

```
C
GO TO 910
C
C
C ODDS AND ENDS
C
C SONDE PROFILE DOES NOT EXTEND TO HIGH ENOUGH ALTITUDE.
900 WRITE (IMES,2900) ALTI, SONDE(1,1)
2900 FORMAT ('0SLANTA 2900: DESIRED TOP ALTITUDE =',F6.0,' TOP SONDE',
X' ALTITUDE IS',F6.0)
GO TO 990
C DESIRED ALTITUDES NOT FOUND IN ECC PROFILE
910 WRITE (IMES,2910)
2910 FORMAT ('0SLANT 2910: DESIRED ALTITUDES NOT FOUND IN ECC-1')
C
990 NCODE = -20
999 RETURN
END
```

*** END OF MEMBER *** 95 RECORDS PROCESSED

ORIGINAL FILE IN
OF POOR QUALITY

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SUBROUTINE TAPE(NCODE,IMES)
C REED, BATLUCK, AND COOKE, FEB 1983
C TAPE READS THE SMOOTHED OZONE DATA TAPE (COUNTS VS ALTITUDE) AND
C PLACES THE PEDIGREE RECORDS IN PED, THE DATA IN SMOOTH.
C
C NCODE = 1 NO PROBLEMS
C = -6 EOF DURING PEDIGREE RECORDS
C = -7 READ ERROR ON SMOOTH TAPE.
C = -8 WRONG FLIGHT NUMBER IN PEDIGREE RECORDS.
C NLAIRS= NUMBER OF ALTITUDE LEVELS IN ROCOZ SMOOTH ARRAY.
C
REAL*8 TAPEIN,TAPOUT
DIMENSION R(20)
COMMON/SETUP/TAPEIN,TAPOUT,NFIN,NFOT,INCLD(7),TOP(7),BASE(7)
COMMON/DATAIN/NLAIRS,SECSZA(60),SMOOTH(20,60,7)
COMMON/DATOUT/NSAV,PED(20,30),SAVE(20,60)
DATA IUNIT/10/

C MOUNT AND POSITION TAPE.
CALL MOUNT(1,IUNIT,TAPEIN,NFIN)
C READ PEDIGREE RECORDS; CHECK FLIGHT NUMBERS.
NREC = 0
FLTN = PED(2,5)
DO 20 I=1,4
CALL FREQO (PED(1,1),IUNIT,LEN,&910,&920)
C *** TEST STATEMENT
WRITE(IMES,2900) (PED(J,I),J=1,9)
2900 FORMAT (1X,F5.0,2X,F5.1,2X,F7.0,2X,F9.2,2X,F8.3,2X,
X F9.3,2X,F9.2,2X,F9.2)
NREC = NREC + 1
IF (PED(2,I) .NE. FLTN ) GO TO 930
20 CONTINUE
C READ SMOOTH DATA
PASTF = 99.
30 NREC = NREC + 1
CALL FREQO(R(1),IUNIT,LEN,&940,&920)
IF (R(1) .EQ. PASTF) GO TO 35
HRD1 = R(1)
J = 0
IF (HRD1 .EQ. 3.) J=1
IF (HRD1 .EQ. 2.) J=2
IF (HRD1 .EQ. 1.) J=3
IF (HRD1 .EQ. 0.) J=4
IF (HRD1 .EQ. 30.) J=5
IF (HRD1 .EQ. 20.) J=6
IF (HRD1 .EQ. 10.) J=7
PASTF = HRD1
IF (J .EQ. 0) GO TO 935
NLAIRS = 0
35 NLAIRS = NLAIRS + 1
CALL CHOVE (R(1),SMOOTH(1,NLAIRS,J),80)
C *** TEST STATEMENT
WRITE(IMES,2905) NREC,SMOOTH(1,NLAIRS,J),SMOOTH(2,NLAIRS,J),

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ORIGINAL PAGE 10
OF POOR QUALITY

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OF POOR QUALITY

```
C X NLAYS-J
2905 FORMAT(1X,I4,2F10.3,2X,I2,2X,I2)
GO TO 30
C
C ODDS AND ENDS
C
C END OF FILE DURING FIRST FOUR RECORDS
910 WRITE (IMES,2910) IUNIT, NREC
2910 FORMAT ('OTAPE 2910: UNEXPECTED EOF ON UNIT',I4,' AFTER RECORD',
X13)
NCODE = -6
GO TO 999
C ERROR IN READING SMOOTH TAPE.
920 WRITE (IMES,2920) IUNIT,NREC
2920 FORMAT ('OTAPE 2920: READ ERROR, UNIT',I4,' AFTER RECORD',I5)
NCODE = -7
GO TO 999
C FLIGHT NUMBERS DO NOT MATCH
930 WRITE (IMES,2930) FLTN,NREC,PED(1,NREC),PED(2,NREC)
2930 FORMAT ('OTAPE 2930: DESIRED FLIGHT NO.',F6.1,'.RECORD NO',I3,
X' HORDS 1 AND 2 ARE',F6.0,F7.1)
00000383
00000384
00000400
00000480
00000490
00000500
00000510
00000520
00000530
00000540
00000550
00000560
00000570
00000580
00000590
00000600
00000610
00000620
00000630
00000640
00000650
```


26JUL84 08.53.47 - VOL=SACC10, DSN=L3EIR.PROF.CNTL

MEMBER=TAPE

```
NCODE = -8
GO TO 999
C INVALID VALUE FOR WORD 1
935 WRITE (IMES,2935) NREC,MRD1,MRD1,MRD1
2935 FORMAT ('OTAPE 2935: RECORD NO',16,' ',WORD 1 IS: ',G13.4,
X2X,110,2X,A4)
NCODE = -1
GO TO 999
C NORMAL EOF
940 NREC=NREC-1
WRITE (IMES,2940) NREC
2940 FORMAT('OTAPE 2940:',15,' RECORDS FROM SMOOTH TAPE')
NCODE = 1
999 RETURN
END
```

00000660
00000670
00000672
00000674
00000676
00000678
00000680
00000682
00000740
00000750
00000760
00000770
00000780
00000790
00000800

*** END OF MEMBER *** 92 RECORDS PROCESSED *****

ORIGINAL PAGE 10
OF POOR QUALITY

ORIGINAL PAGE 11
OF POOR QUALITY

```

SUBROUTINE TAPMRT(MODE,IMES)
C REED, BATLUCK, COOKE
C TAPMRT PERFORMS ALL TAPE OUT OPERATIONS, USING FTIO
C
C MODE = 1 MOUNT TAPE AND WRITE PED RECORDS
C       = 2 WRITE OZONE PROFILES
C       = 3 WRITE DERIVED PROFILES AND CLOSE OUTPUT TAPE
C
REAL*8 TAPEIN,TAPOUT
DIMENSION COMP(20,70),TYP4(20,2),TYP5(20,17)
COMMON/SETUP/TAPEIN,TAPOUT,NFIN,NFOT,DUM(4,3)
COMMON/DATOUT/NSAV,PED(20,30),SAVE(20,60)
EQUIVALENCE (NDXTOP,PED(1,1)), (NDXBAS,PED(2,1)),
X(COMP(1,1),PED(1,2)),(TYP4(1,1),SAVE(1,42)),(TYP5(1,1),SAVE(1,44))
DATA NREC/0/,IOUT/15/,LEN/80/
IF (MODE - 2) 100,300,500
C WRITE PEDIGREE RECORDS
100 CALL MOUNT(2,IOUT,TAPOUT,NFOT)
DO 120 I = 1,NSAV
CALL FWRITE(PED(1,I),IOUT,LEN)
T = PED(1,I)
120 NREC = NREC + 1
130 GO TO 600
C WRITE THE OZONE DATA RECORDS
300 IF (NSAV.LE.60) GO TO 310
WRITE (IMES,2300) NSAV
2300 FORMAT ('OTAPMRT 2300: NSAV WAS',I8,'; RESET TO 60')
NSAV = 60
310 DO 320 I = 1,NSAV
CALL FWRITE(SAVE(1,I),IOUT,LEN)
320 NREC = NREC + 1
T = SAVE(1,NSAV)
GO TO 600
2320 FORMAT ('OTAPMRT 2320: ',A8,' FILE',I3,' ON UNIT',I3,' HAS',I4,
X' RECORDS. LAST RECORD IS TYPE',F6.0)
330 GO TO 990
C WRITE COMPOSITE PROFILE, PROFILE IN STD LAYERS, AND AT STD PRESSURES.
500 DO 510 I = NDXTOP,NDXBAS
CALL FWRITE(COMP(1,I),IOUT,LEN)
510 NREC = NREC + 1
CALL FWRITE(TYP4(1,1),IOUT,LEN)
CALL FWRITE(TYP4(1,2),IOUT,LEN)
NREC = NREC + 2
DO 520 I = 1,17

```

00000530
00000540
00000542
00000550
00000700
00000710
00000720

CALL FWRITE(TYP5(1,1),IOUT,LEN)
520 NREC = NREC + 1
T = TYP5(1,17)
600 WRITE (IMES.2320) TAPOUT,NFOT,IOUT,NREC,T
C END RETURN
990 END

*** END OF MEMBER *** 63 RECORDS PROCESSED *****

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OF POOR QUALITY

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graph TD
    MAIN[MAIN] --- SECANG[SECANG]
    MAIN --- OZDENS[OZDENS]
    MAIN --- COMPST[COMPST]
    MAIN --- CHECKS[CHECKS]
    MAIN --- RELATD[RELATD]
    MAIN --- CARDS[CARDS]
    MAIN --- TAPE[TAPE]
    MAIN --- MODEL[MODEL]
    MAIN --- DATSND[DATSND]
    MAIN --- PRTPRF[PRTPRF]
    MAIN --- TAPWRT[TAPWRT]
    OZDENS --- SLANTA[SLANTA]
    OZDENS --- ALFEFF[ALFEFF]
    OZDENS --- SHAPE[SHAPE]
    ALFEFF --- INARRY[INARRY]
    ALFEFF --- CFTWRT[CFTWRT]
    INARRY -.- CFTWRT
    SHAPE --- PRTPED[PRTPED]
    SHAPE --- TAPWRT
    COMPST -.- PRTSAV[PRTSAV]
    CHECKS --- OVERLP[OVERLP]
    OVERLP --- LINFIT[LINFIT]
    RELATD --- DAT[DAT]
    RELATD --- CMP[ CMP]
    RELATD --- TP4[ TP4]
    RELATD --- WRT[WRT]
    RELATD --- WRT[WRT]
    RELATD --- WRT[WRT]
    RELATD --- TP5[ TP5]
    RELATD --- WRT[WRT]
    RELATD --- WRT[WRT]
    RELATD --- PRTWRT[PRTWRT]
    
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NOV. 2 1983
E. REED

NOV. 2 1983
E. REED

		ALFEFF	CARDS	CFTWRT	CHECKS	COMST	DATSN	INARRY	LINEFIT	MODEL	OVERLP	OZDENS	PRTPED	PRTPRF	PRTSAV	PRTWRT	DATWRT	CMPWRT	TP4WRT	TP5WRT	RELATD	SECANG	SHAPE	SLANTA	TAPWRT	CMOVE	FT10	RPDAT0	COEFTS	SETUP	/PROFLS	/FSHAPE	/CONST	/DATAIN	/DATOUT	
MAIN		X			X		X	X	X	X				X			X	X	X					X	X	X	X	X	X	X	X	X	X	X	X	X
	ALFEFF							X					X											X	X	X										
	CARDS																																			X
	CFTWRT																																			
	CHECKS											X																								
COMPST																																				
	DATSN																																			
	INARRY																																			
	LINEFIT																																			
	MODEL																																			
OVERLP																																				
	OZDENS																																			
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PRTWRT																																				
	DATWRT																																			
	CMPWRT																																			
	TP4WRT																																			
	TP5WRT																																			
RELATD																																				
	SECANG																																			
	SHAPE																																			
	SLANTA																																			
	TAPE																																			
TAPWRT																																				

OUTPUT LISTINGS

PROGRAM TO SAMPLE RAW OZONE TAPE (REVISED OCT. 1982)

FLIGHT NUMBER	325	TAPE KA2130	FILE 2	PRINT VERSION 1
---------------	-----	-------------	--------	-----------------

PRINT 40 SAMPLES, RECORDS 1 TO 3 EVERY 50 RECORDS

RECORD 0 HAS 46 WORDS. TAPE 1 PCN6 S.L.O.O. T1-776

RECORD	WORDS	DT/FR	FR/BF	SCALE	NB/FR	HQ/FR	PRE	B	BFAPP	INPUT	OUTPUT		17	18	19	RUN	STREAM
-3	20	8	110	0	3	11	2	0	1210	122 ^c		0	0	0	0	PCMM	PCMM

1	1220	WORDS,	BLOCK	68	STREAM	PCMA	PR/AP	30	DATA	BF=	1210	STAT	00	COMP	START	326	D	15	HR	29	MM	39+	0.090	SEC.	MD1=0.F:	UNCOMP
	DAY	HOUR	MIN	SEC	SEC.	SEC.	ELAPSED	SEC	50		SI				54			S5		BATT		MARKER				
326	15	29	29	30	0.0900	1770.0898	1770.0899	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.1000	1770.0999	1770.0999	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.1100	1770.1099	1770.1099	1023	1023		1023				1023			1023		650				0		
326	15	29	29	30	0.1200	1770.1199	1770.1199	1023	1023		1023				1023			1023		650				0		
326	15	29	29	30	0.1300	1770.1299	1770.1299	1023	1023		1023				1023			1023		650				0		
326	15	29	29	30	0.1400	1770.1399	1770.1399	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.1500	1770.1499	1770.1499	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.1600	1770.1599	1770.1599	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.1700	1770.1699	1770.1699	1023	1023		1023				1023			1023		650				0		
326	15	29	29	30	0.1800	1770.1799	1770.1799	1023	1023		1023				1023			1023		650				0		
326	15	29	29	30	0.1900	1770.1899	1770.1899	1023	1023		1023				1023			1023		650				0		
326	15	29	29	30	0.2000	1770.2000	1770.2000	1023	1023		1023				1023			1023		650				0		
326	15	29	29	30	0.2100	1770.2100	1770.2100	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.2200	1770.2200	1770.2200	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.2300	1770.2300	1770.2300	1023	1023		1023				1023			1023		650				2		
326	15	29	29	30	0.2400	1770.2400	1770.2400	1023	1023		1023				1023			1023		650				2		
326	15	29	29	30	0.2500	1770.2500	1770.2500	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.2600	1770.2600	1770.2600	1023	1023		1023				1023			1023		650				0		
326	15	29	29	30	0.2700	1770.2700	1770.2700	1023	1023		1023				1023			1023		650				2		
326	15	29	29	30	0.2800	1770.2800	1770.2800	1023	1023		1023				1023			1023		650				1		
326	15	29	29	30	0.2900	1770.2900	1770.2900	1023	1023		1023		</													

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RADAR

FILE NO.: 1

INPUT TAPE NO.: KA2131

112283.

FLIGHT NO. 325

DATE

LAUNCHED

(MIDDY.):

SEC ELAPSED	HEIGHT	LATITUDE	LONGITUDE
0.00	6149.45	37.8347	-75.4773
1.00	6149.45	37.8347	-75.4773
2.00	6149.45	37.8347	-75.4773
3.00	6149.45	37.8347	-75.4773
4.00	6149.45	37.8347	-75.4773
5.00	6149.45	37.8347	-75.4773
6.00	7786.07	37.8278	-75.4686
7.00	11118.77	37.8137	-75.4509
8.00	14221.34	37.8025	-75.4371
9.00	16274.91	37.8158	-75.4508
10.00	16369.59	37.8200	-75.4569
11.00	16768.87	37.8234	-75.4613
12.00	16931.79	37.8267	-75.4648
13.00	14461.36	37.8328	-75.4729
14.00	16423.94	37.8308	-75.4700
15.00	17582.97	37.8303	-75.4692
16.00	18646.62	37.8298	-75.4683
17.00	19695.71	37.8293	-75.4674
18.00	20732.18	37.8288	-75.4665
19.00	21731.30	37.8283	-75.4656
20.00	22759.49	37.8278	-75.4648
21.00	23756.54	37.8273	-75.4639
22.00	24733.88	37.8268	-75.4630
23.00	25716.74	37.8263	-75.4621
24.00	26681.57	37.8258	-75.4613
25.00	27633.31	37.8252	-75.4604
26.00	28576.78	37.8247	-75.4595
27.00	29505.94	37.8243	-75.4587
28.00	30425.92	37.8237	-75.4578
29.00	31331.52	37.8233	-75.4570
30.00	32229.27	37.8227	-75.4561
31.00	33121.43	37.8223	-75.4553
32.00	33998.75	37.8217	-75.4544
33.00	34868.61	37.8212	-75.4536
34.00	35734.75	37.8207	-75.4527
35.00	36577.50	37.8202	-75.4519
36.00	37416.86	37.8197	-75.4510
37.00	38246.16	37.8192	-75.4502
38.00	39065.26	37.8187	-75.4493
39.00	39874.04	37.8182	-75.4485
40.00	40674.12	37.8177	-75.4477
41.00	41465.38	37.8172	-75.4468
42.00	42253.35	37.8167	-75.4460
43.00	43020.91	37.8162	-75.4451
44.00	43770.56	37.8157	-75.4444
45.00	44522.07	37.8152	-75.4435
46.00	45261.81	37.8147	-75.4427
47.00	45992.73	37.8142	-75.4419
48.00	46712.39	37.8137	-75.4411
49.00	47422.50	37.8132	-75.4402
50.00	48124.03	37.8127	-75.4394
51.00	48814.51	37.8122	-75.4385
52.00	49496.49	37.8117	-75.4377
53.00	50167.92	37.8112	-75.4369
54.00	50826.59	37.8107	-75.4361

PROGRAM: EDIT -- REVISED FEBRUARY 22, 1983

TAPE INFO: NAME I/O UNIT FILE# RECORD LEN.

KA2130 INPUT 10 2
KA2145 OUTPUT 15 1 80

INPUT DATA: DELTAT RECORD MPEAK LPEAK RANGE
0.677 24 462 132 30

HDR1: 46 WORDS. TAPE NUMBER 1 STREAM PCM4 S.L.O.O. T1-776

HDR2: 110 FRAMES PER RECORD 1220 WORDS PER RECORD

BATTERY VOLTAGE = -0.0 + 0.010 WORD-6 COUNTS

TEMPERATURE C VOLTS ADJUSTMENT TO SER NO 400 CURVE TYPICAL
-19.0 9.880 1.002
25.0 3.860 0.998
49.0 1.830 1.013

BATTERY CALIBRATION

TEMPERATURE CALIBRATION

FLT/LG	PAYLOAD	TAPE RCD	RUN DATE	VOLTS (UPPER)	TM CT	VOLTS (LOWER)	TM CT	DEG C. (LOWER)	TM VOLTS	DEG C. (UPPER)	TM VOLTS
-200.	325.0	489.	82984.	6.5	652.00	5.6	562.00	-19.0	9.88	25.0	3.86
		11684.								49.0	1.83

ORIGINAL PAGE IS
OF POOR QUALITY

T1(SEC)	T2(SEC)	T4(SEC)	T5(SEC)	AVG1	AVG2	AVG4	AVG5	MRKR	BASE	CMPI	CMF2	CMF4	CMF5	DELPK	DELAV	CHAV	BATV	TR	C	SM	EX
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 102.8201	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6550	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.7200	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6799	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6802	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6699	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6799	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6802	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6899	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6799	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.7000	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6902	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6799	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.7151	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6748	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.7148	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.	173.	130.	111.	0.495	0.495	0.495	0.495	0.495	0.495
CYCLE 2940: CYCLE REJECTED. LENGTH WAS 0.6951	1902.460	1902.530	1902.680	1902.815	173.2	59.6	46.3	62.8	462.	8	20	177.									

PROGRAM: MERGE UPDATED NOV, 1983

TAPE INFO: NAME UNIT FILE#

OZONE	KA2145	15	1
RADAR	KA2131	16	1
MERGE	KA2123	10	1

RADAR PED: -100. 325. 101. 112283. 163000.0 37.850 -75.480 11684. 82984. WALLOPS ISLAND LAUNCH TIME= 1800. SECONDS
LAUNCH SITE RH RM RS RACOR DD DM DS DECOR SH SM SS HOUR RESTR FLIGHT DATE AND TIME
WALLOPS 15.0J 47.00 32.41 252.09 -19.00 57.00 35.60 -779.00 4.00 1.00 39.32 16.00 0.00 325 NOV. 22, 1983 1630Z

BEG. RECORD 0 BAD RECORDS START END

1 0

PEDIGREE:

-300. 325.0 82984. 15.00 47.00 32.41 252.09 -19.00 57.00 35.60 -779.00 4.00 1.00 39.32 0. 0. 0. 0. 0. 0.

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ORIGINAL PAGE 19
OF POOR QUALITY

S0	SEC	CYCLE	SAM	TEMC	S0	S1	S2	S3	MARK	BATV	COM0	COM1	COM2	COM3	CMAVE	S0	S1	S2	S3	ALT	S2	S3	ALT	SZA
1902.460	0.495	44.	19.8	173.	60.	46.	63.	462.	6.42	177.	173.	130.	111.	136.	0.71354	0.71354	0.71354	0.71354	0.71354	0.71354	0.71354	0.71354	0.71354	58.02
1957.490	0.630	55.	20.9	808.	822.	815.	782.	445.	6.38	496.	504.	466.	481.	479.	6.68282	0.68282	0.68282	0.68282	0.68282	0.68282	0.68282	0.68282	0.68282	57.97
1958.120	0.580	51.	20.9	813.	828.	811.	775.	448.	6.38	504.	468.	394.	396.	429.	6.68128	0.68128	0.68128	0.68128	0.68128	0.68128	0.68128	0.68128	0.68128	57.97
1958.700	0.600	52.	20.9	791.	820.	821.	784.	449.	6.38	401.	381.	323.	353.	373.	6.67986	0.67986	0.67986	0.67986	0.67986	0.67986	0.67986	0.67986	0.67986	57.97
1959.300	0.595	53.	20.9	806.	824.	811.	783.	448.	6.38	458.	419.	415.	430.	437.	6.67837	0.67837	0.67837	0.67837	0.67837	0.67837	0.67837	0.67837	0.67837	57.97
1959.895	0.585	54.	20.9	804.	830.	823.	787.	448.	6.38	438.	450.	427.	454.	450.	6.67689	0.67689	0.67689	0.67689	0.67689	0.67689	0.67689	0.67689	0.67689	57.97
1960.480	0.600	54.	20.9	798.	820.	810.	769.	448.	6.38	438.	457.	427.	454.	424.	6.67545	0.67545	0.67545	0.67545	0.67545	0.67545	0.67545	0.67545	0.67545	57.97
1961.080	0.590	54.	20.9	803.	830.	823.	785.	448.	6.38	425.	457.	427.	454.	424.	6.67396	0.67396	0.67396	0.67396	0.67396	0.67396	0.67396	0.67396	0.67396	57.97
1961.670	0.600	54.	20.9	800.	823.	812.	775.	448.	6.38	442.	490.	443.	413.	440.	6.67247	0.67247	0.67247	0.67247	0.67247	0.67247	0.67247	0.67247	0.67247	57.97
1962.270	0.595	53.	20.9	800.	824.	822.	789.	448.	6.38	433.	456.	436.	406.	430.	6.67100	0.67100	0.67100	0.67100	0.67100	0.67100	0.67100	0.67100	0.67100	57.97
1962.865	0.585	54.	20.9	811.	827.	812.	781.	448.	6.38	420.	435.	396.	360.	399.	6.66957	0.66957	0.66957	0.66957	0.66957	0.66957	0.66957	0.66957	0.66957	57.97
1963.450	0.600	54.	20.9	798.	814.	805.	774.	448.	6.38	392.	395.	366.	370.	379.	6.66808	0.66808	0.66808	0.66808	0.66808	0.66808	0.66808	0.66808	0.66808	57.97
1964.050	0.600	55.	21.0	804.	829.	821.	781.	448.	6.38	377.	420.	411.	437.	387.	6.66652	0.66652	0.66652	0.66652	0.66652	0.66652	0.66652	0.66652	0.66652	57.97
1964.650	0.590	53.	21.0	803.	818.	806.	772.	448.	6.38	388.	417.	364.	359.	373.	6.66500	0.66500	0.66500	0.66500	0.66500	0.66500	0.66500	0.66500	0.66500	57.97
1965.845	0.585	54.	21.0	805.	815.	811.	777.	448.	6.38	362.	337.	354.	309.	331.	6.66351	0.66351	0.66351	0.66351	0.66351	0.66351	0.66351	0.66351	0.66351	57.97
1966.430	0.600	54.	21.0	805.	823.	817.	782.	447.	6.38	307.	387.	375.	322.	354.	6.66052	0.66052	0.66052	0.66052	0.66052	0.66052	0.66052	0.66052	0.66052	57.97
1967.030	0.590	54.	21.0	806.	824.	814.	774.	447.	6.38	391.	451.	386.	371.	399.	6.65903	0.65903	0.65903	0.65903	0.65903	0.65903	0.65903	0.65903	0.65903	57.97
1967.620	0.600	54.	21.0	799.	815.	799.	779.	447.	6.38	392.	356.	319.	401.	363.	6.65756	0.65756	0.65756	0.65756	0.65756	0.65756	0.65756	0.65756	0.65756	57.97
1968.220	0.595	53.	21.0	795.	809.	811.	779.	447.	6.38	354.	320.	425.	408.	377.	6.65607	0.65607	0.65607	0.65607	0.65607	0.65607	0.65607	0.65607	0.65607	57.97
1968.815	0.585	54.	21.1	803.	827.	824.	780.	446.	6.38	404.	451.	449.	382.	407.	6.65461	0.65461	0.65461	0.65461	0.65461	0.65461	0.65461	0.65461	0.65461	57.97
1969.400	0.575	53.	21.0	801.	808.	819.	781.	447.	6.38	346.	359.	343.	321.	331.	6.65317	0.65317	0.65317	0.65317	0.65317	0.65317	0.65317	0.65317	0.65317	57.97
1970.570	0.590	54.	21.0	801.	819.	819.	781.	447.	6.38	314.	367.	378.	385.	368.	6.65172	0.65172	0.65172	0.65172	0.65172	0.65172	0.65172	0.65172	0.65172	57.97
1971.160	0.590	53.	21.1	800.	824.	813.	768.	446.	6.38	372.	385.	406.	337.	365.	6.65030	0.65030	0.65030	0.65030	0.65030	0.65030	0.65030	0.65030	0.65030	57.96
1971.750	0.590	54.	21.0	792.	813.	815.	785.	447.	6.38	370.	334.	336.	357.	355.	6.64908	0.64908	0.64908	0.64908	0.64908	0.64908	0.64908	0.64908	0.64908	57.96
1972.340	0.615	54.	21.0	804.	806.	807.	773.	446.	6.38	340.	314.	282.	306.	284.	6.64740	0.64740	0.64740	0.64740	0.64740	0.64740	0.64740	0.64740	0.64740	57.96
1972.955	0.585	54.	21.0	808.	823.	808.	776.	446.	6.38	314.	265.	282.	306.	284.	6.64590	0.64590	0.64590	0.64590	0.64590	0.64590	0.64590	0.64590	0.64590	57.96
1973.540	0.590	54.	21.0	790.	813.	821.	776.	447.	6.38	274.	327.	390.	332.	336.	6.64431	0.64431	0.64431	0.64431	0.64431	0.64431	0.64431	0.64431	0.64431	57.96
1974.130	0.590	53.	21.1	799.	813.	811.	774.	446.	6.38	363.	395.	392.	366.	371.	6.64311	0.64311	0.64311	0.64311	0.64311	0.64311	0.64311	0.64311	0.64311	57.96
1974.720	0.590	54.	21.1	807.	820.	807.	769.	446.	6.38	338.	327.	310.	311.	319.	6.64171	0.64171	0.64171	0.64171	0.64171	0.64171	0.64171	0.64171	0.64171	57.96
1975.310	0.625	55.	21.1	797.	817.	818.	775.	446.	6.38	367.	361.	321.	391.	356.	6.64032	0.64032	0.64032	0.64032	0.64032	0.64032	0.64032	0.64032	0.64032	57.96
1975.935	0.585	54.	21.1	799.	810.	806.	768.	446.	6.38	363.	322.	364.	361.	341.	6.63893	0.63893	0.63893	0.63893	0.63893	0.63893	0.63893	0.63893	0.63893	57.96
1976.520	0.590	54.	21.1	802.	825.	816.	772.	446.	6.38	343.	326.	340.	361.	341.	6.63740	0.63740	0.63740	0.63740	0.63740	0.63740	0.63740	0.63740	0.63740	57.96
1977.110	0.600	54.	21.1	793.	810.	816.	771.	446.	6.38	334.	352.	413.	376.	367.	6.63609	0.63609	0.63609	0.63609	0.63609	0.63609	0.63609	0.63609	0.63609	57.96
1977.710	0.590	54.	21.1	799.	811.	823.	777.	446.	6.38	344.	381.	370.	368.	368.	6.63473	0.63473	0.63473	0.63473	0.63473	0.63473	0.63473	0.63473	0.63473	57.96
1978.300	0.615	54.	21.1	798.	819.	815.	776.	446.	6.38	349.	374.	370.	368.	368.	6.63334	0.63334	0.63334	0.63334	0.63334	0.63334	0.63334	0.63334	0.63334	57.96
1978.915	0.585	54.	21.1	798.	827.	822.	776.	445.	6.38	402.	394.	366.	363.	371.	6.63205	0.63205	0.63205	0.63205	0.63205	0.63205	0.63205	0.63205	0.63205	57.96
1979.500	0.600	54.	21.2	808.	819.	811.	772.	445.	6.38	397.	394.	400.	427.	400.	6.63060	0.63060	0.63060	0.63060	0.63060	0.63060	0.63060	0.63060	0.63060	57.96
1980.090	0.590	54.	21.2	808.	819.	809.	775.	445.	6.38	379.	372.	415.	416.	389.	6.62925	0.62925	0.62925	0.62925	0.62925	0.62925	0.62925	0.62925	0.62925	57.96
1980.690	0.590	54.	21.2	798.	816.	815.	775.	445.	6.38	379.	421.	431.	434.	419.	6.62790	0.62790	0.62790	0.62790	0.62790	0.62790	0.62790	0.62790	0.62790	57.96
1981.280	0.615	54.	21.2	807.	825.	822.	781.	445.	6.38	429.	468.	449.	385.	426.	6.62654	0.62654	0.62654	0.62654	0.62654	0.62654	0.62654	0.62654	0.62654	57.96
1981.895	0.585	54.	21.2	813.	828.	813.	771.	445.	6.38	394.	399.	371.	366.	383.	6.62522	0.62522	0.62522	0.62522	0.62522	0.62522	0.62522	0.62522	0.62522	57.96
1982.480	0.590	54.	21.2	803.	817.	803.	771.	445.	6.38	417.	415.	388.	361.	431.	6.62385	0.62385	0.62385	0.62385	0.62385	0.62385	0.62385	0.62385	0.62385	57.96
1983.070	0.600	54.	21.2	805.	817.	810.	772.	445.	6.38	437.	411.	378.	352.	382.	6.62254	0.62254	0.62254	0.62254	0.62254	0.62254	0.62254	0.62254	0.62254	57.96
1983.670	0.580	53.	21.2	801.	816.	816.	776.	445.	6.38	437.	411.	378.	352.	382.	6.62122	0.62122	0.62122	0.62122	0.62122	0.62122	0.62122	0.62122	0.62122	57.96
1984.250	0.615	54.	21.2	797.	820.	816.	776.	445.	6.38	350.	351.	383.	355.	372.	6.61992	0.61992	0.61992	0.61992	0.61992	0.61992	0.61992	0.61992	0.61992	57.96
1984.865	0.565	53.	21.2	812.	828.	816.	767.	445.	6.38	392.	430.	436.	401.	414.	6.61866	0.61866	0.61866	0.61866	0.61866	0.61866	0.61866	0.61866	0.61866	57.96
1985.430	0.600	54.	21.2	802.	821.	806.	763.	445.	6.38	403.	359.	361.	384.	431.	6.61730	0.61730	0.61730	0.61730	0.61730	0.61730	0.61730	0.61730	0.61730	57.96
1986.030	0.580	53.	21.2	799.	820.	815.	773.	444.	6.38	390.	403.	461.	404.	430.	6.61606	0.61606	0.61606	0.61606	0.61606	0.61606	0.61606	0.61606	0.61606	57.96
1986.610	0.600	54.	21.2	812.	833.	819.	769.	444.	6.38	464.</														

FLT. NO.

-400. 325. 82984.

TAPE INFORMATION:			
NAME	I/O	FILE	UNIT
KA2123	INPUT	1	10
KA2145	OUTPUT	2	15

UPPER HEIGHT LIMIT: 67.0 KM
LOWER HEIGHT LIMIT: 16.0 KM
MINIMUM ACCEPTABLE COMPENSATION WORD = 281.0
RATIOS= 1 MODE= 0

ZERO OFF-SETS: S0 S1 S2 S3 TA TB S2B S3B
 0 0 0 0 8.5 16.3 18.0 9.9
 LOGFIT 2800: NPTS = 260 NOLD = 127 N = 125 FP = 2. ALT = 23. A = -0.2179 B = 0.3631 TWO S.D. = 1.730

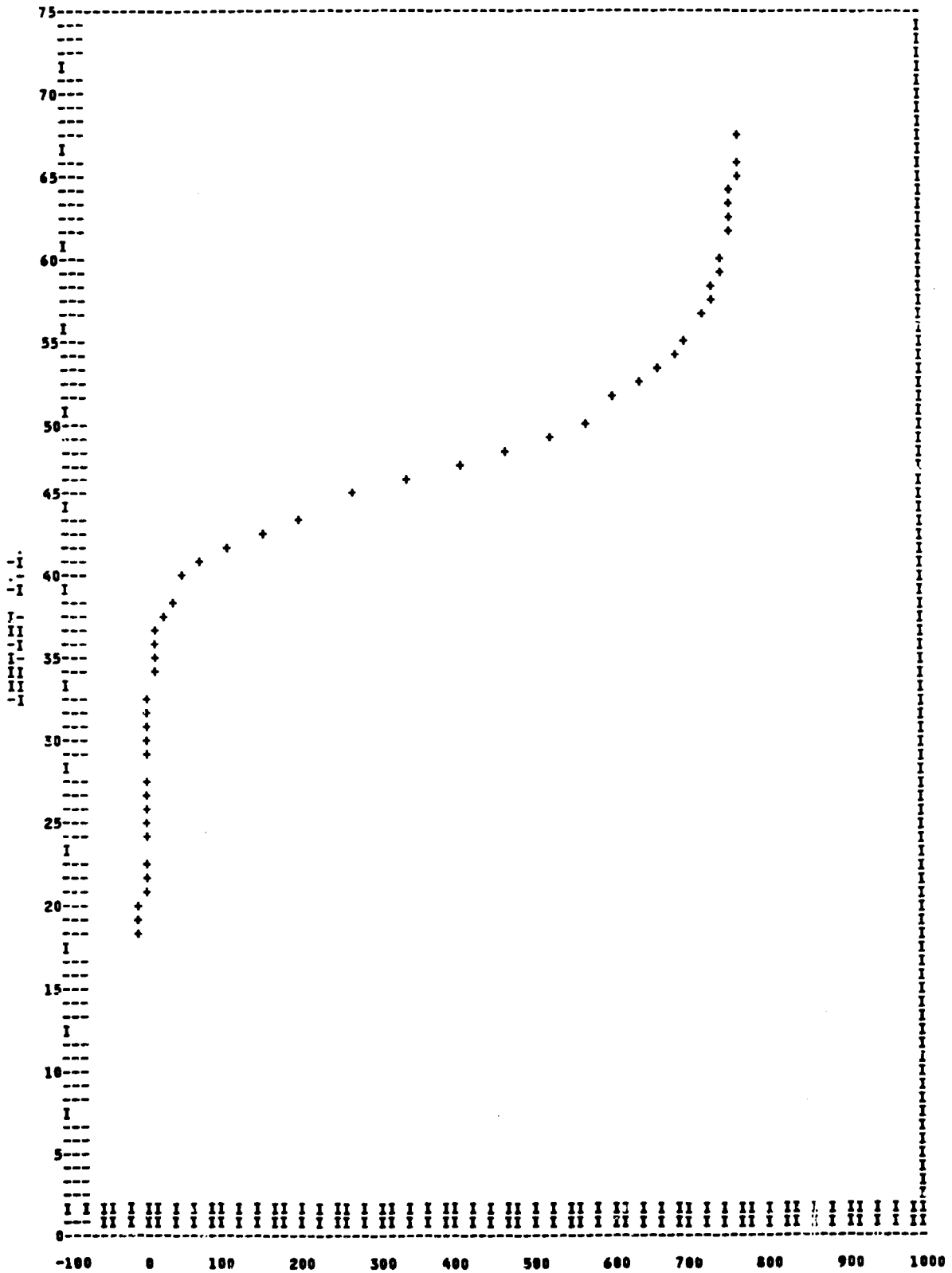
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0011111000000000	000000000000000000	0000000000000000	00000000000000	00000000000000
00477336000300	000100000000000000	0000000000000000	00000000000000	00000000000000
226208725332807	1200020011000011	1200020011000011	1200020011000011	1200020011000011

IV-197

FILTER POSITION	3	STDCTS	START	END	DIFF	BASEIO	STDCTS	STDY	ABSORP	DABSORP	SETSIX	COREL	USD	PTS
24. 2969.5	57.85	18.2	0.705	6.17	464.	734.606	1.0172	0.14	-0.0042	0.0002	0.79	0.87	86.	93.
23. 3057.1	57.85	17.2	0.743	6.14	496.	734.606	1.0172	0.14	-0.0042	0.0002	0.79	0.87	86.	93.
22. 3155.3	57.85	16.0	0.771	6.14	467.	734.606	1.0172	0.14	-0.0042	0.0002	0.79	0.87	86.	93.
21. 3265.0	57.86	14.4	0.792	6.12	474.	734.606	1.0172	0.14	-0.0042	0.0002	0.79	0.87	86.	93.
20. 3388.1	57.87	12.9	0.803	6.10	480.	734.606	1.0172	0.14	-0.0042	0.0002	0.79	0.87	86.	93.
19. 3531.5	57.89	10.9	0.802	6.08	472.	734.606	1.0172	0.14	-0.0042	0.0002	0.79	0.87	86.	93.
18. 3701.8	57.92	8.4	0.758	6.06	456.	732.889	1.1022	0.15	-0.0044	0.0002	0.90	0.87	90.	96.
						725.396	1.2224	0.17	-0.0054	0.0003	1.03	0.89	95.	100.
						717.344	1.1897	0.17	-0.0069	0.0003	0.99	0.92	94.	100.
						706.956	1.3073	0.18	-0.0088	0.0003	1.19	0.93	94.	100.
						693.306	1.5604	0.23	-0.0116	0.0004	1.28	0.93	97.	100.
						673.473	1.3713	0.20	-0.0160	0.0004	1.23	0.96	95.	100.
						655.995	1.3106	0.20	-0.0194	0.0005	1.32	0.97	94.	100.
						631.781	1.8081	0.29	-0.0250	0.0007	1.63	0.96	97.	100.
						597.105	1.9543	0.33	-0.0341	0.0009	1.76	0.97	100.	100.
						565.907	1.7276	0.31	-0.0428	0.0009	1.76	0.98	95.	100.
						520.858	1.8950	0.36	-0.0568	0.0012	2.00	0.98	98.	100.
						477.178	1.7343	0.36	-0.0721	0.0012	2.23	0.99	93.	100.
						419.427	2.0948	0.50	-0.0937	0.0018	2.74	0.98	96.	100.
						355.964	1.7734	0.50	-0.1258	0.0020	2.83	0.99	95.	100.
						290.115	1.4993	0.52	-0.1659	0.0023	2.94	0.99	97.	100.
						227.808	1.0602	0.47	-0.2054	0.0021	2.50	0.99	99.	100.
						175.368	0.6924	0.39	-0.2435	0.0019	2.19	1.00	96.	100.
						129.903	0.3728	0.49	-0.2922	0.0026	2.68	1.00	97.	100.
						89.503	0.2662	0.61	-0.3349	0.0023	2.36	1.00	97.	100.
						61.513	0.2496	0.61	-0.3756	0.0025	2.62	1.00	95.	100.
						41.252	0.2612	0.90	-0.4076	0.0038	3.85	1.00	95.	100.
						28.982	0.2979	1.33	-0.4406	0.0061	5.24	0.99	95.	100.
						22.402	0.2660	1.61	-0.3449	0.0098	7.36	0.96	97.	100.
						16.555	0.3001	2.17	-0.3250	0.0127	8.94	0.93	98.	100.
						13.821	0.4032	3.31	-0.2672	0.0183	12.49	0.83	97.	100.
						9.744	0.3750	3.85	-0.1768	0.0271	21.50	0.54	104.	110.
						6.816	0.2704	3.97	-0.1615	0.0315	25.98	0.43	116.	120.
						5.949	0.2755	4.16	-0.2597	0.0326	27.93	0.58	125.	130.
						5.949	0.2755	4.16	-0.0990	0.0337	31.14	0.25	135.	140.
						3.103	0.2168	5.07	-0.0862	0.0299	30.77	0.24	143.	150.
						3.103	0.1572	5.07	-0.4557	0.0409	49.55	0.67	152.	160.
						3.911	0.2212	5.66	-0.0287	0.0507	58.27	0.04	165.	170.
						2.869	0.2212	5.66	-0.1310	0.0471	58.22	0.21	172.	180.
						2.325	0.1880	8.09	-0.2441	0.0566	77.36	0.31	174.	190.
						1.558	0.1405	9.02	-0.1741	0.0667	88.66	0.19	186.	210.
						1.226	0.1250	9.69	-0.3523	0.0735	88.87	0.34	176.	220.
						1.426	0.1934	13.57	-0.2441	0.0792	83.62	0.24	155.	230.
						0.001	0.1270	12.69	-0.0169	0.1063	125.49	0.01	128.	240.
						0.001	0.0000	0.00	-0.2224	0.0920	145.04	0.22	114.	260.
						0.00	0.00	0.00	0.00	0.00	65.21	0.00	266.	280.
						0.00	0.00	0.00	0.00	0.00	77.55	0.00	283.	300.
						0.00	0.00	0.00	0.00	0.00	59.12	0.00	319.	330.
						0.00	0.00	0.00	0.00	0.00	47.06	0.00	370.	390.

ORIGINAL OF POOR QUALITY



UV SIGNAL SS

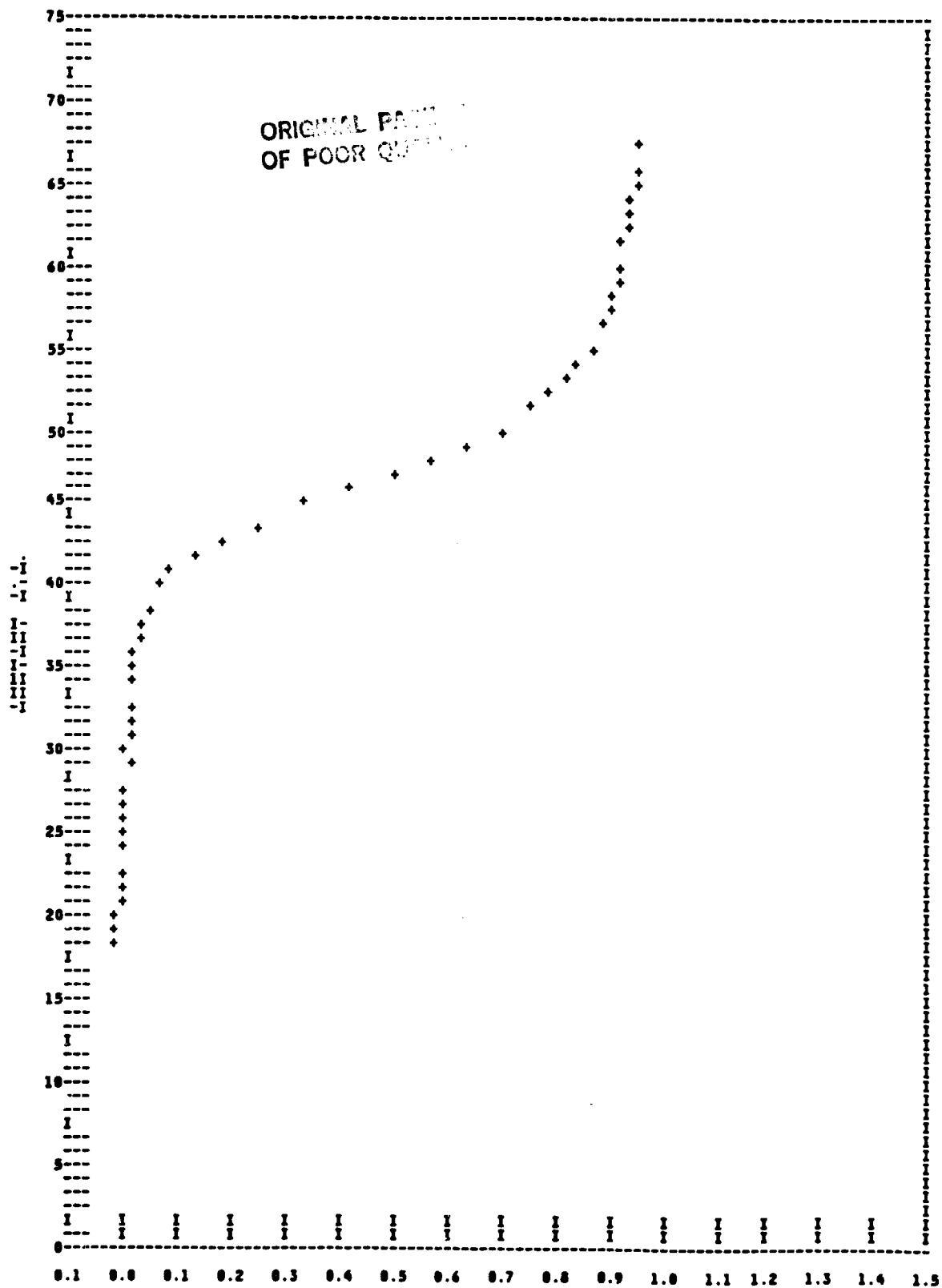
ORIGINAL FILED
OF POOR QUALITY

FILTER POSITION 30 (DIVIDED BY SC)

KM	CMT/RAT	STDCS	STDX	SLOPE	START	END	DIFF	BASEIO	STDCS	STDX	ABSORP	DABSORP	SETSDX	COREL	USD	PIS
67.	0.958	0.0036	0.38	-0.0045	67.28	56.21	11.07	0.911	0.0016	0.18	-0.0047	0.0013	0.99	0.85	89.	93.
66.	0.934	0.0033	0.35	-0.0044	67.28	56.21	11.07	0.911	0.0016	0.18	-0.0047	0.0003	0.99	0.85	89.	93.
65.	0.949	0.0031	0.32	-0.0044	67.28	56.21	11.07	0.911	0.0016	0.18	-0.0047	0.0003	0.99	0.85	89.	93.
64.	0.945	0.0028	0.30	-0.0044	67.28	56.21	11.07	0.911	0.0016	0.18	-0.0047	0.0003	0.99	0.85	89.	93.
63.	0.941	0.0026	0.28	-0.0044	67.28	56.21	11.07	0.911	0.0016	0.18	-0.0047	0.0003	0.99	0.85	89.	93.
62.	0.936	0.0024	0.25	-0.0044	67.28	56.21	11.07	0.911	0.0016	0.18	-0.0047	0.0003	0.99	0.85	89.	93.
61.	0.931	0.0023	0.24	-0.0047	67.28	55.96	11.32	0.908	0.0017	0.19	-0.0050	0.0003	1.03	0.86	93.	96.

11

60.	0.926	0.0022	0.24	-0.0057	66.54	55.23	11.31	0.899	0.0016	0.18	-0.0061	0.0003	1.04	0.90	96.	100.
59.	0.920	0.0023	0.26	-0.0072	65.21	54.52	10.69	0.888	0.0016	0.18	-0.0078	0.0003	1.11	0.92	95.	100.
58.	0.911	0.0023	0.26	-0.0083	63.78	53.79	9.99	0.876	0.0018	0.20	-0.0091	0.0004	1.24	0.93	95.	100.
57.	0.900	0.0029	0.29	-0.0109	62.42	53.09	9.33	0.858	0.0020	0.23	-0.0091	0.0005	1.37	0.94	94.	100.
56.	0.886	0.0029	0.33	-0.0141	60.88	52.30	8.59	0.835	0.0021	0.25	-0.0122	0.0006	1.44	0.95	97.	100.
55.	0.888	0.0031	0.35	-0.0179	59.49	51.55	7.94	0.808	0.0022	0.27	-0.0206	0.0007	1.54	0.96	98.	100.
54.	0.847	0.0031	0.37	-0.0224	58.13	50.78	7.34	0.778	0.0022	0.29	-0.0264	0.0008	1.58	0.97	98.	100.
53.	0.821	0.0032	0.39	-0.0284	56.72	49.95	6.77	0.739	0.0022	0.30	-0.0346	0.0009	1.64	0.97	98.	100.
52.	0.789	0.0034	0.43	-0.0341	55.47	49.17	6.29	0.698	0.0023	0.33	-0.0432	0.0011	1.80	0.98	97.	100.
51.	0.749	0.0034	0.45	-0.0424	54.15	48.34	5.80	0.644	0.0023	0.35	-0.0566	0.0012	1.95	0.98	98.	100.
50.	0.702	0.0032	0.45	-0.0499	52.96	47.56	5.40	0.591	0.0021	0.35	-0.0710	0.0015	1.99	0.99	97.	100.
49.	0.646	0.0036	0.55	-0.0599	51.68	46.69	4.99	0.521	0.0023	0.42	-0.0928	0.0020	2.38	0.99	95.	100.
48.	0.578	0.0040	0.68	-0.0697	50.45	45.85	4.59	0.446	0.0023	0.53	-0.1206	0.0023	2.82	0.99	97.	100.
47.	0.502	0.0036	0.71	-0.0801	49.28	45.02	4.25	0.366	0.0023	0.54	-0.1595	0.0023	2.97	0.99	97.	100.
46.	0.420	0.0026	0.61	-0.0850	48.06	44.12	3.94	0.287	0.0013	0.46	-0.2026	0.0021	2.54	0.99	96.	100.
45.	0.336	0.0019	0.57	-0.0813	46.90	43.25	3.65	0.220	0.0010	0.43	-0.2418	0.0021	2.51	1.00	97.	100.
44.	0.258	0.0014	0.54	-0.0740	45.78	42.37	3.41	0.162	0.0007	0.41	-0.2867	0.0022	2.23	1.00	97.	100.
43.	0.190	0.0010	0.53	-0.0620	44.65	41.47	3.18	0.116	0.0005	0.40	-0.3359	0.0022	2.49	1.00	95.	100.
42.	0.134	0.0009	0.66	-0.0492	43.55	40.58	2.97	0.080	0.0004	0.51	-0.3872	0.0030	3.09	1.00	95.	100.
41.	0.092	0.0008	0.89	-0.0366	42.43	39.67	2.76	0.054	0.0004	0.62	-0.3991	0.0042	5.62	0.99	94.	100.
40.	0.045	0.0008	1.27	-0.0242	41.33	38.77	2.55	0.038	0.0004	0.98	-0.3914	0.0066	5.62	0.99	94.	100.
39.	0.004	0.0007	1.85	-0.0146	40.21	37.84	2.37	0.030	0.0004	1.40	-0.3789	0.0103	7.75	0.96	97.	100.
38.	0.032	0.0007	2.17	-0.0097	39.10	36.91	2.19	0.023	0.0004	1.64	-0.3551	0.0129	9.07	0.92	98.	100.
37.	0.025	0.0007	2.87	-0.0061	38.04	36.00	2.04	0.019	0.0004	2.18	-0.2461	0.0134	12.61	0.81	97.	100.
36.	0.020	0.0009	4.33	-0.0032	37.08	35.00	2.08	0.017	0.0006	3.32	-0.1585	0.0271	12.45	0.50	103.	110.
35.	0.017	0.0008	5.06	-0.0022	36.08	33.97	2.11	0.014	0.0006	3.81	-0.1319	0.0313	25.79	0.37	115.	120.
34.	0.013	0.0007	5.25	-0.0031	35.10	32.98	2.12	0.010	0.0004	3.98	-0.2356	0.0326	27.96	0.54	125.	130.
33.	0.010	0.0006	5.82	-0.0006	34.09	31.98	2.11	0.010	0.0004	4.19	-0.0376	0.0339	31.39	0.15	135.	140.
32.	0.011	0.0005	6.84	-0.0004	33.07	30.97	2.10	0.010	0.0004	3.66	-0.0427	0.0300	30.85	0.12	143.	150.
31.	0.008	0.0005	6.67	-0.0034	32.08	29.99	2.09	0.005	0.0003	5.08	-0.4125	0.0410	49.58	0.64	152.	160.
30.	0.007	0.0006	8.11	-0.0001	31.05	28.99	2.06	0.003	0.0005	6.06	-0.0124	0.0508	58.44	0.02	165.	170.
29.	0.008	0.0006	7.51	-0.0006	30.04	28.00	2.04	0.008	0.0004	5.67	-0.0765	0.0472	58.33	0.12	172.	180.
28.	0.007	0.0006	8.98	-0.0013	29.02	27.02	2.00	0.006	0.0004	6.81	-0.1820	0.0566	77.46	0.24	174.	190.
27.	0.005	0.0006	10.72	-0.0006	28.06	26.01	2.05	0.005	0.0004	8.07	-0.1129	0.0665	88.56	0.12	186.	210.
26.	0.005	0.0006	11.94	-0.0013	27.02	25.01	2.01	0.004	0.0003	9.02	-0.2719	0.0735	88.90	0.27	186.	220.
25.	0.004	0.0005	12.84	-0.0007	26.02	24.02	2.00	0.003	0.0003	9.70	-0.2719	0.0735	88.90	0.17	186.	230.
24.	0.004	0.0007	18.02	-0.0003	25.01	23.00	2.01	0.003	0.0005	13.59	-0.0768	0.0793	83.73	0.06	186.	240.
23.	0.004	0.0006	16.34	-0.0005	24.07	21.99	2.08	0.003	0.0004	12.70	-0.1104	0.1064	145.19	0.13	114.	260.
22.	0.003	0.0003	0.00	0.0000	23.08	21.01	2.07	0.000	0.0000	0.00	0.0000	0.0920	145.19	0.00	265.	280.
21.	0.008	0.0000	0.00	0.0000	22.06	20.02	2.04	0.000	0.0000	0.00	0.0000	0.0000	-99.48	0.00	282.	300.
20.	0.013	0.0000	0.00	0.0000	21.07	19.06	2.01	0.000	0.0000	0.00	0.0000	0.0000	-99.38	0.00	320.	330.
19.	0.016	0.0000	0.00	0.0000	20.11	18.09	2.02	0.000	0.0000	0.00	0.0000	0.0000	-99.43	0.00	367.	390.
18.	0.019	0.0000	0.00	0.0000	19.09	17.09	2.00	0.000	0.0000	0.00	0.0000	0.0000	-99.27	0.00	445.	470.



UV SIGNAL 53 DIVIDED BY 50

PROFILE

ORIGINAL PAGE IS
OF POOR QUALITY

325.0	KAZ116	10	KAZ113	10	0	0.83	BARR	0	489
OPT	TOP BASE	CTR MM	MM	MM	A0	AL	BTMP	BMBAR	BETA
1	58.0	39.0	263.30	13.30	194.520	-3073.26978	-23416.39844	2.97930	
2	49.0	30.0	242.30	9.10	32.7789	-72.54568	138.06099	1.36420	
3	44.0	19.0	300.80	7.10	8.2503	-3.86985	2.06072	1.28600	
4	40.0	19.0	306.70	6.80	3.1370	-0.50358	0.07242	1.10980	
5	38.0	19.0	306.70	6.80	191.7250	-3072.76636	-23416.46875	0.96950	
6	49.0	30.0	0.0	0.0	29.6419	-72.04211	137.98857	0.23440	
7	44.0	19.0	0.0	0.0	5.1134	-3.36627	1.98830	0.09620	
DATE AM PM DOBSON UNITS									
11	22.83	260.0	253.0						
FLT ID	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	DATA
71-0771	11 22 83	1530	60	18.7	205.10	70.00			
FLT ID	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	DATA
440326	11 22 83	15 0	22000.	0.09096					
FLT ID	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	MM/DB/YY	DATA
440327	11 22 83	1720	22000.	0.08936					
DSB =	18.666	KM	205.100	K	70.000	MBAR			
MXSHD =	51								
NECC =	19	19							
ECCLIM AT	250	125	62.5	MBAR					
	0.824	0.833	0.833						
	0.0	0.0	0.0						
SONDE =									
ALT	TEMP	PRESS	DENS	ERR K					
1 70.000	234.450	0.049	0.7317E-04	11.476					
2 69.000	232.350	0.057	0.8512E-04	10.183					
3 68.000	232.450	0.066	0.9831E-04	9.175					
4 67.000	236.250	0.076	0.1116E-03	8.259					
5 66.000	240.050	0.087	0.1263E-03	7.495					
6 65.000	244.250	0.100	0.1426E-03	6.879					
7 64.000	247.050	0.115	0.1615E-03	6.249					
8 63.000	249.350	0.131	0.1831E-03	5.812					
9 62.000	251.250	0.150	0.2077E-03	5.177					
10 61.000	253.450	0.171	0.2351E-03	5.457					
11 60.000	255.150	0.195	0.2689E-03	4.964					
12 59.000	257.150	0.223	0.3042E-03	5.177					
13 58.000	258.750	0.254	0.3418E-03	4.752					
14 57.000	260.450	0.289	0.3842E-03	4.674					
15 56.000	262.350	0.329	0.4312E-03	4.504					
16 55.000	264.650	0.375	0.4790E-03	4.363					
17 54.000	266.350	0.427	0.5286E-03	4.253					
18 53.000	268.350	0.487	0.5799E-03	4.163					
19 52.000	269.450	0.555	0.6339E-03	4.088					
20 51.000	270.450	0.633	0.6908E-03	4.008					
21 50.000	271.750	0.721	0.7512E-03	3.908					
22 49.000	273.450	0.822	0.8166E-02	3.808					
23 48.000	274.050	0.930	0.8875E-02	3.584					
24 47.000	274.550	1.071	0.9648E-02	3.584					
25 46.000	274.950	1.223	0.1048E-01	3.561					
26 45.000	275.150	1.398	0.1175E-01	3.561					
27 44.000	275.350	1.597	0.1324E-01	3.539					
28 43.000	275.550	1.827	0.1498E-01	3.539					
29 42.000	275.750	2.091	0.1698E-01	3.539					
30 41.000	275.950	2.395	0.1924E-01	3.519					
31 40.000	276.150	2.749	0.2178E-01	3.519					
32 39.000	276.350	3.162	0.2460E-01	3.519					
33 38.000	276.550	3.642	0.2772E-01	3.519					
34 37.000	276.750	4.199	0.3118E-01	3.519					
35 36.000	276.950	4.845	0.3500E-01	3.481					
36 35.000	277.150	5.600	0.3918E-01	3.465					
37 34.000	277.350	6.477	0.4375E-01	3.465					
38 33.000	277.550	7.495	0.4875E-01	3.450					
39 32.000	277.750	8.685	0.5418E-01	3.450					
40 31.000	277.950	10.073	0.6000E-01	3.450					
41 30.000	278.150	11.692	0.6624E-01	3.436					
42 29.000	278.350	13.584	0.7286E-01	3.436					

ORIGINAL FILE
OF POOR QUALITY

	ALT	TEMP	PRESS	OS	03
43	28.000	220.450	13.015	0.299E-01	1.436
44	27.000	218.350	18.451	0.294E-01	1.436
45	26.000	216.850	21.556	0.346E-01	1.436
46	25.000	213.950	25.225	0.410E-01	1.436
47	24.000	211.350	29.559	0.487E-01	1.436
48	23.000	211.150	34.675	0.572E-01	1.436
49	22.000	210.950	40.716	0.672E-01	1.436
50	21.000	209.650	47.839	0.794E-01	1.436
51	20.000	208.950	56.254	0.937E-01	1.436
52	19.000	208.000	66.000	0.000	1.436
53	18.000	207.000	77.000	0.000	1.436
54	17.000	206.000	89.000	0.000	1.436
55	16.000	205.000	102.000	0.000	1.436
56	15.000	204.000	116.000	0.000	1.436
57	14.000	203.000	131.000	0.000	1.436
58	13.000	202.000	147.000	0.000	1.436
59	12.000	201.000	164.000	0.000	1.436
60	11.000	200.000	182.000	0.000	1.436
61	10.000	199.000	201.000	0.000	1.436
62	9.000	198.000	221.000	0.000	1.436
63	8.000	197.000	242.000	0.000	1.436
64	7.000	196.000	264.000	0.000	1.436
65	6.000	195.000	287.000	0.000	1.436
66	5.000	194.000	312.000	0.000	1.436
67	4.000	193.000	338.000	0.000	1.436
68	3.000	192.000	365.000	0.000	1.436
69	2.000	191.000	394.000	0.000	1.436
70	1.000	190.000	424.000	0.000	1.436

ECC =

	ALT	TEMP	PRESS	OS	03
1	0.167	200.000	100.000	27.500	13.700
2	1.352	201.500	105.000	38.000	15.000
3	3.121	203.100	110.000	50.000	16.000
4	5.758	204.800	115.000	63.000	17.000
5	7.413	206.500	120.000	77.000	18.000
6	9.439	208.200	125.000	92.000	19.000
7	10.661	209.900	130.000	108.000	20.000
8	12.128	211.600	135.000	125.000	21.000
9	13.963	213.300	140.000	143.000	22.000
10	16.454	215.000	145.000	162.000	23.000
11	19.687	216.700	150.000	182.000	24.000
12	23.669	218.400	155.000	203.000	25.000
13	28.556	220.100	160.000	225.000	26.000
14	34.513	221.800	165.000	248.000	27.000
15	41.708	223.500	170.000	272.000	28.000
16	50.300	225.200	175.000	297.000	29.000
17	60.540	226.900	180.000	323.000	30.000
18	72.670	228.600	185.000	350.000	31.000
19	86.840	230.300	190.000	378.000	32.000

STD =

	ALT	OS/MS	ATM-CN
1	70.0	0.540E 15	0.535E-05
2	69.0	0.645E 15	0.756E-05
3	68.0	0.750E 15	0.102E-04
4	67.0	0.123E 16	0.138E-04
5	66.0	0.172E 16	0.195E-04
6	65.0	0.244E 16	0.271E-04
7	64.0	0.317E 16	0.375E-04
8	63.0	0.399E 16	0.509E-04
9	62.0	0.481E 16	0.672E-04
10	61.0	0.563E 16	0.875E-04
11	60.0	0.645E 16	0.112E-03
12	59.0	0.727E 16	0.145E-03
13	58.0	0.809E 16	0.181E-03
14	57.0	0.891E 16	0.220E-03
15	56.0	0.973E 16	0.262E-03
16	55.0	0.208E 17	0.308E-03
17	54.0	0.255E 17	0.358E-03
18	53.0	0.319E 17	0.415E-03
19	52.0	0.384E 17	0.476E-03

ROCOZ FLIGHT NO. 325.0 FLOWN 112283 (MIDDY.) 163000.0 (HMMSS.S)
AT 37.850 LAT, -75.480 LONG., MALLOPS ISLAND

ORIGINAL PAGE IS
OF POOR QUALITY

ALT-KM	ERX	Z-HMMSS.S	SZA-DEG	SZA-SEC	SINT-ATM	SCAT	CMF%	AIR T-K	ERR-K	AIR P-MBAR	INSTR	TWP-C
57.00	0.04	15330.3	57.95	1.8843	0.0054	0.018	231.75	4.47	0.28743	21.5		
56.00	0.04	15327.1	57.95	1.8842	0.0061	0.021	231.75	4.46	0.28642	21.5		
55.00	0.04	15324.0	57.94	1.8841	0.0070	0.024	231.75	4.45	0.28542	21.5		
54.00	0.04	15320.9	57.94	1.8840	0.0079	0.027	231.75	4.44	0.28442	21.5		
53.00	0.04	15317.8	57.94	1.8839	0.0088	0.030	231.75	4.43	0.28342	21.5		
52.00	0.04	15314.7	57.94	1.8838	0.0097	0.033	231.75	4.42	0.28242	21.5		
51.00	0.04	15311.6	57.93	1.8837	0.0106	0.036	231.75	4.41	0.28142	21.5		
50.00	0.04	15308.5	57.93	1.8836	0.0115	0.039	231.75	4.40	0.28042	21.5		
49.00	0.04	15305.4	57.93	1.8835	0.0124	0.042	231.75	4.39	0.27942	21.5		
48.00	0.04	15302.3	57.92	1.8834	0.0133	0.045	231.75	4.38	0.27842	21.5		
47.00	0.04	15299.2	57.92	1.8833	0.0142	0.048	231.75	4.37	0.27742	21.5		
46.00	0.04	15296.1	57.92	1.8832	0.0151	0.051	231.75	4.36	0.27642	21.5		
45.00	0.04	15293.0	57.92	1.8831	0.0160	0.054	231.75	4.35	0.27542	21.5		
44.00	0.04	15289.9	57.92	1.8830	0.0169	0.057	231.75	4.34	0.27442	21.5		
43.00	0.04	15286.8	57.92	1.8829	0.0178	0.060	231.75	4.33	0.27342	21.5		
42.00	0.04	15283.7	57.92	1.8828	0.0187	0.063	231.75	4.32	0.27242	21.5		
41.00	0.04	15280.6	57.92	1.8827	0.0196	0.066	231.75	4.31	0.27142	21.5		
40.00	0.04	15277.5	57.92	1.8826	0.0205	0.069	231.75	4.30	0.27042	21.5		
39.00	0.04	15274.4	57.92	1.8825	0.0214	0.072	231.75	4.29	0.26942	21.5		
38.00	0.04	15271.3	57.92	1.8824	0.0223	0.075	231.75	4.28	0.26842	21.5		
37.00	0.04	15268.2	57.92	1.8823	0.0232	0.078	231.75	4.27	0.26742	21.5		
36.00	0.04	15265.1	57.92	1.8822	0.0241	0.081	231.75	4.26	0.26642	21.5		
35.00	0.04	15262.0	57.92	1.8821	0.0250	0.084	231.75	4.25	0.26542	21.5		
34.00	0.04	15258.9	57.92	1.8820	0.0259	0.087	231.75	4.24	0.26442	21.5		
33.00	0.04	15255.8	57.92	1.8819	0.0268	0.090	231.75	4.23	0.26342	21.5		
32.00	0.04	15252.7	57.92	1.8818	0.0277	0.093	231.75	4.22	0.26242	21.5		
31.00	0.04	15249.6	57.92	1.8817	0.0286	0.096	231.75	4.21	0.26142	21.5		
30.00	0.04	15246.5	57.92	1.8816	0.0295	0.099	231.75	4.20	0.26042	21.5		
29.00	0.04	15243.4	57.92	1.8815	0.0304	0.102	231.75	4.19	0.25942	21.5		
28.00	0.04	15240.3	57.92	1.8814	0.0313	0.105	231.75	4.18	0.25842	21.5		
27.00	0.04	15237.2	57.92	1.8813	0.0322	0.108	231.75	4.17	0.25742	21.5		
26.00	0.04	15234.1	57.92	1.8812	0.0331	0.111	231.75	4.16	0.25642	21.5		
25.00	0.04	15231.0	57.92	1.8811	0.0340	0.114	231.75	4.15	0.25542	21.5		
24.00	0.04	15227.9	57.92	1.8810	0.0349	0.117	231.75	4.14	0.25442	21.5		
23.00	0.04	15224.8	57.92	1.8809	0.0358	0.120	231.75	4.13	0.25342	21.5		
22.00	0.04	15221.7	57.92	1.8808	0.0367	0.123	231.75	4.12	0.25242	21.5		
21.00	0.04	15218.6	57.92	1.8807	0.0376	0.126	231.75	4.11	0.25142	21.5		
20.00	0.04	15215.5	57.92	1.8806	0.0385	0.129	231.75	4.10	0.25042	21.5		
19.00	0.04	15212.4	57.92	1.8805	0.0394	0.132	231.75	4.09	0.24942	21.5		
18.00	0.04	15209.3	57.92	1.8804	0.0403	0.135	231.75	4.08	0.24842	21.5		
17.00	0.04	15206.2	57.92	1.8803	0.0412	0.138	231.75	4.07	0.24742	21.5		
16.00	0.04	15203.1	57.92	1.8802	0.0421	0.141	231.75	4.06	0.24642	21.5		
15.00	0.04	15200.0	57.92	1.8801	0.0430	0.144	231.75	4.05	0.24542	21.5		
14.00	0.04	15196.9	57.92	1.8800	0.0439	0.147	231.75	4.04	0.24442	21.5		
13.00	0.04	15193.8	57.92	1.8799	0.0448	0.150	231.75	4.03	0.24342	21.5		
12.00	0.04	15190.7	57.92	1.8798	0.0457	0.153	231.75	4.02	0.24242	21.5		
11.00	0.04	15187.6	57.92	1.8797	0.0466	0.156	231.75	4.01	0.24142	21.5		
10.00	0.04	15184.5	57.92	1.8796	0.0475	0.159	231.75	4.00	0.24042	21.5		
9.00	0.04	15181.4	57.92	1.8795	0.0484	0.162	231.75	3.99	0.23942	21.5		
8.00	0.04	15178.3	57.92	1.8794	0.0493	0.165	231.75	3.98	0.23842	21.5		
7.00	0.04	15175.2	57.92	1.8793	0.0502	0.168	231.75	3.97	0.23742	21.5		
6.00	0.04	15172.1	57.92	1.8792	0.0511	0.171	231.75	3.96	0.23642	21.5		
5.00	0.04	15169.0	57.92	1.8791	0.0520	0.174	231.75	3.95	0.23542	21.5		
4.00	0.04	15165.9	57.92	1.8790	0.0529	0.177	231.75	3.94	0.23442	21.5		
3.00	0.04	15162.8	57.92	1.8789	0.0538	0.180	231.75	3.93	0.23342	21.5		
2.00	0.04	15159.7	57.92	1.8788	0.0547	0.183	231.75	3.92	0.23242	21.5		
1.00	0.04	15156.6	57.92	1.8787	0.0556	0.186	231.75	3.91	0.23142	21.5		
0.00	0.04	15153.5	57.92	1.8786	0.0565	0.189	231.75	3.90	0.23042	21.5		

DATA FOR FILTER POSITION 53

ALT	INTENSITY	DLI/DM	NOISE	SLNTO	SLNTA	ALPHA-F	BET-F	DA/DSLQ	DSLQ/DM	OSTAU	AIRTAU	COMP	SCATX	B(SMTH)	BSTDV	BDI
57.	725.3667	-0.0132	0.0035	.00041	.00054	193.600	1.607	510.5198	0.0001	0.079	0.001	456.	0.018	-0.0116	0.0004	11.48
56.	714.4973	-0.0148	0.0038	.00050	.00061	193.332	1.607	539.3660	0.0001	0.096	0.001	462.	0.021	-0.0160	0.0004	10.87
55.	701.3755	-0.0213	0.0045	.00061	.00070	192.993	1.607	560.8982	0.0001	0.117	0.001	466.	0.024	-0.0194	0.0005	10.10
54.	684.6254	-0.0285	0.0049	.00075	.00079	192.536	1.607	606.8872	0.0001	0.145	0.001	462.	0.028	-0.0250	0.0007	9.54
53.	662.5422	-0.0349	0.0054	.00093	.00091	191.274	1.607	625.0447	0.0001	0.179	0.001	483.	0.032	-0.0341	0.0009	8.96
52.	638.4157	-0.0449	0.0064	.00117	.00103	191.245	1.607	625.0447	0.0001	0.223	0.002	493.	0.037	-0.0428	0.0009	8.38
51.	605.4542	-0.0578	0.0062	.00147	.00118	189.595	1.607	646.3625	0.0002	0.279	0.002	489.	0.042	-0.0568	0.0012	7.91
50.	568.9336	-0.0712	0.0081	.00177	.00134	189.558	1.607	646.3625	0.0002	0.353	0.002	485.	0.049	-0.0721	0.0012	7.46
49.	528.7173	-0.0893	0.0084	.00200	.00148	185.134	1.607	710.5862	0.0002	0.449	0.002	474.	0.057	-0.0937	0.0018	7.10
48.	482.6011	-0.1200	0.0090	.00230	.00169	182.187	1.607	737.9478	0.0003	0.572	0.003	456.	0.065	-0.1258	0.0020	6.65
47.	442.4334	-0.1656	0.0096	.00251	.00192	178.744	1.607	737.9478	0.0003	0.728	0.004	464.	0.087	-0.1659	0.0021	6.32
46.	394.9889	-0.2028	0.0086	.00277	.00220	175.921	1.607	726.3825	0.0004	0.915	0.004	484.	0.101	-0.2054	0.0019	5.69
45.	348.3982	-0.2460	0.0089	.00313	.00260	173.972	1.607	726.3825	0.0004	1.139	0.005	495.	0.116	-0.2435	0.0026	5.43
44.	294.7740	-0.2912	0.0075	.00367	.00340	160.370	1.607	710.5864	0.0005	1.361	0.005	480.	0.134	-0.2922	0.0028	5.19
43.	199.9281	-0.3353	0.0085	.01036	.00389	151.410	1.607	699.0559	0.0005	1.661	0.006	479.	0.155	-0.3349	0.0025	4.99
42.	104.7249	-0.3738	0.0095	.01282	.00445	140.959	1.607	675.3992	0.0006	2.200	0.007	473.	0.179	-0.3756	0.0038	4.78
41.	70.9960	-0.3963	0.0130	.01562	.00445	140.959	1.607	675.3992	0.0006	2.200	0.007	473.	0.179	-0.4076	0.0038	4.78
40.	47.4087	-0.3773	0.0191	.01832	.00511	129.584	1.607	608.8564	0.0007	2.400	0.008	501.	0.207	-0.4006	0.0061	4.58

DATA FOR FILTER POSITION 53

ALT	HMMSS.S	O3ATH-CH/KM	NUM/M3	ERRX	COL-ATH-CH	NUM/M2	AIR-T-K	ERRX	AIR-P-MBAR	EXR	AIR-N/M3	AIR-COL-ATH	O3-NANOBAR	PPMV
57.	133339.3	0.00026	0.934E 16	26.7	0.00027	0.587E 20	261.75	1.8	0.28874	2.3	0.7990E 22	0.00023	0.34813	1.21
56.	133337.1	0.00034	0.132E 17	22.7	0.00023	0.707E 20	264.45	1.8	0.28864	2.3	0.9282E 22	0.00035	0.43460	1.33
55.	133340.2	0.00038	0.136E 17	22.1	0.00038	0.863E 20	265.35	1.8	0.27048	2.3	0.1063E 23	0.00030	0.55005	1.47
54.	133351.9	0.00096	0.297E 17	17.4	0.00039	0.107E 21	256.65	1.8	0.47716	2.3	0.1206E 23	0.00042	0.71035	1.67
53.	133400.2	0.00096	0.332E 17	15.5	0.00049	0.133E 21	256.45	1.4	0.48688	2.3	0.1376E 23	0.00048	0.91025	1.83
52.	133409.1	0.000124	0.421E 17	14.2	0.000780	0.166E 21	256.45	1.4	0.53501	2.0	0.1568E 23	0.00054	1.17957	2.13
51.	133418.8	0.000211	0.421E 17	10.7	0.000991	0.268E 21	256.45	1.4	0.62251	2.0	0.1780E 23	0.00063	1.53352	2.42
50.	133422.2	0.000221	0.567E 17	8.1	0.001272	0.341E 21	255.45	1.4	0.72082	2.0	0.2033E 23	0.00071	2.01294	2.79
49.	133440.5	0.000368	0.753E 17	7.4	0.001640	0.449E 21	254.95	1.4	0.82190	2.0	0.2374E 23	0.00082	2.65845	3.23
48.	133452.7	0.000481	0.987E 17	5.5	0.002121	0.569E 21	252.95	1.4	0.93785	2.0	0.2674E 23	0.00092	3.46482	3.69
47.	133505.7	0.000602	0.129E 18	4.3	0.002723	0.731E 21	252.95	1.4	1.07090	2.0	0.3066E 23	0.00108	4.51722	4.22
46.	133520.1	0.000750	0.161E 18	3.7	0.003474	0.933E 21	252.95	1.4	1.22336	2.0	0.3509E 23	0.001208	5.64094	5.04
45.	133531.4	0.000920	0.214E 18	3.7	0.004394	0.118E 22	251.55	1.4	1.39758	2.0	0.4002E 23	0.001380	7.04142	5.61
44.	133551.0	0.001108	0.271E 18	2.7	0.005502	0.147E 22	249.65	1.4	1.59713	2.0	0.4603E 23	0.001577	10.24666	6.1
43.	133609.6	0.001308	0.340E 18	2.6	0.006801	0.183E 22	249.65	1.4	2.05111	2.0	0.5307E 23	0.001805	12.11938	6.5
42.	133628.6	0.001489	0.430E 18	3.5	0.008301	0.223E 22	242.25	1.4	2.35509	2.0	0.6063E 23	0.002035	15.62733	6.8
41.	133649.1	0.011340	0.402E 18	5.1	0.009842	0.264E 22	242.25	1.5	2.74916	2.0	0.7033E 23	0.002315	19.64277	7.0
40.	133711.0	0.001340	0.413E 18	5.1	0.009842	0.264E 22	242.25	1.5	2.74916	2.0	0.7033E 23	0.002315	19.64277	7.0

DATA FOR FILTER POSITION 33 DIVIDED BY 50

ALT	INTENSITY	DL1/DM	NOISE	SIMTO	SIMTA	ALPHA-F	BET-F	DA/DSLO	DSLA/DM	OSTAU	AIRTAU	COMP	SCATX	B(SMTH)	BSTDV	BDH
57.	0.8997	-0.0138	0.0042	.00041	.00054	190.448	0.969	539.8430	0.0001	0.079	0.001	456	0.018	-0.0122	0.0005	11.48
56.	0.8858	-0.0183	0.0046	.00051	.00061	190.157	0.969	572.3806	0.0001	0.097	0.001	463	0.021	-0.0159	0.0006	10.77
55.	0.8679	-0.0226	0.0049	.00063	.00070	189.790	0.969	586.3986	0.0001	0.113	0.001	469	0.024	-0.0176	0.0007	10.54
54.	0.8467	-0.0268	0.0052	.00077	.00091	188.752	0.969	601.2246	0.0001	0.146	0.001	483	0.028	-0.0244	0.0007	9.36
53.	0.8209	-0.0335	0.0056	.00120	.00103	187.969	0.969	633.3889	0.0001	0.226	0.001	483	0.032	-0.0346	0.0009	8.36
52.	0.7887	-0.0460	0.0060	.00151	.00118	187.016	0.969	642.2517	0.0002	0.283	0.001	483	0.037	-0.0432	0.0009	7.91
51.	0.7487	-0.0538	0.0062	.00191	.00134	185.763	0.969	655.5845	0.0002	0.355	0.001	483	0.049	-0.0566	0.0011	7.11
50.	0.7023	-0.0732	0.0072	.00244	.00153	184.387	0.969	687.8948	0.0002	0.449	0.001	474	0.065	-0.0710	0.0012	7.46
49.	0.6459	-0.1060	0.0082	.00313	.00174	181.865	0.969	709.8948	0.0002	0.569	0.002	474	0.075	-0.0928	0.0015	7.10
48.	0.5782	-0.1260	0.0090	.00402	.00227	178.957	0.969	729.9292	0.0003	0.720	0.002	466	0.087	-0.1295	0.0023	6.35
47.	0.5021	-0.1683	0.0091	.00516	.00297	175.188	0.969	729.9292	0.0003	0.905	0.002	466	0.101	-0.1595	0.0021	5.43
46.	0.4196	-0.2002	0.0091	.00659	.00426	170.393	0.969	729.9292	0.0004	1.123	0.003	484	0.116	-0.2018	0.0021	5.43
45.	0.3364	-0.2431	0.0081	.00832	.00597	164.439	0.969	715.6538	0.0004	1.368	0.003	493	0.134	-0.2667	0.0022	5.43
44.	0.2580	-0.2849	0.0077	.01040	.00840	157.084	0.969	707.2397	0.0005	1.605	0.004	481	0.155	-0.3259	0.0022	5.43
43.	0.1903	-0.3276	0.0085	.01294	.00889	148.140	0.969	695.6909	0.0005	1.905	0.004	479	0.179	-0.3672	0.0030	4.99
42.	0.1340	-0.3646	0.0103	.01566	.00945	137.579	0.969	674.3257	0.0006	2.155	0.004	471	0.207	-0.3991	0.0042	4.78
41.	0.0918	-0.3849	0.0142	.01566	.00945	137.579	0.969	674.3257	0.0006	2.155	0.004	471	0.207	-0.3991	0.0042	4.78
40.	0.0618	-0.3845	0.0203	.01853	.00951	126.398	0.969	603.2217	0.0007	2.343	0.005	501	0.207	-0.3914	0.0066	4.58

DATA FOR FILTER POSITION 33 DIVIDED BY 50

ALT	HWSS.S	OSATH-CM/KM	NUM/M3	ERRX	COL-ATN-CH	NUM/M2	AIR-T-K	EXX	AIR-P-MBAR	EXX	AIR-M/M3	AIR-COL-ATM	OS-MANOBAR	PPHV
57.	163350.3	0.00038	0.1031E	17.30.1	0.000320	0.905E	20	261.75	1.8	0.28874	2.3	0.7900E	2.22	0.00285
56.	163357.1	0.00050	0.1342E	17.25.5	0.00070	0.747E	20	256.45	1.8	0.27884	2.3	0.7900E	2.22	0.00285
55.	163354.2	0.00063	0.1691E	17.20.8	0.00133	0.638E	20	256.35	1.8	0.27458	2.3	0.7900E	2.22	0.00285
54.	163351.9	0.00078	0.2081E	17.18.8	0.00210	0.538E	21	256.35	1.8	0.27116	2.3	0.7900E	2.22	0.00285
53.	163340.2	0.00130	0.3482E	17.15.0	0.00310	0.417E	21	256.35	1.8	0.26680	2.3	0.7900E	2.22	0.00285
52.	163340.1	0.00130	0.3482E	17.15.0	0.00310	0.417E	21	256.35	1.8	0.26680	2.3	0.7900E	2.22	0.00285
51.	163341.8	0.00211	0.5657E	17.10.7	0.00504	0.276E	21	256.75	1.4	0.25251	2.0	0.7900E	2.22	0.00285
50.	163340.2	0.00280	0.7518E	17.9.8	0.00804	0.216E	21	256.75	1.4	0.25251	2.0	0.7900E	2.22	0.00285
49.	163352.7	0.00367	0.9865E	17.7.2	0.01294	0.378E	21	255.45	1.4	0.23785	2.0	0.7900E	2.22	0.00285
48.	163350.3	0.00475	0.1272E	18.4.6	0.02137	0.465E	21	255.95	1.4	0.23785	2.0	0.7900E	2.22	0.00285
47.	163350.1	0.00606	0.1628E	18.5.7	0.02743	0.574E	21	255.95	1.4	0.23785	2.0	0.7900E	2.22	0.00285
46.	163350.1	0.00757	0.2035E	18.4.6	0.03300	0.690E	21	255.95	1.4	0.23785	2.0	0.7900E	2.22	0.00285
45.	163351.4	0.00919	0.2469E	18.2.8	0.04419	0.840E	21	255.95	1.4	0.23785	2.0	0.7900E	2.22	0.00285
44.	163351.4	0.01106	0.2971E	18.2.7	0.05525	0.1185E	22	249.35	1.4	0.23785	2.0	0.7900E	2.22	0.00285
43.	163349.4	0.01305	0.3506E	18.2.9	0.06831	0.1485E	22	249.35	1.4	0.23785	2.0	0.7900E	2.22	0.00285
42.	163349.4	0.01490	0.4006E	18.3.7	0.08322	0.236E	22	246.45	1.4	0.23785	2.0	0.7900E	2.22	0.00285
41.	163349.1	0.01527	0.4106E	18.5.6	0.09950	0.2647E	22	242.25	1.5	0.23785	2.0	0.7900E	2.22	0.00285
40.	163311.8													

ORIGINAL OF POOR QUALITY

OVERLAP ANALYSIS , WITH WEIGHTING MODE = 1 FILT Y = A + B * FILT X

FILT X		FILT Y		MX ALT		MY ALT		PAIRS		A		STD DEV A		B		STD DEV B		CORREL	
S3	S2	48.	48.	9.	9.	-0.2235E-03	0.37E-04	1.3932	0.03875	0.9844									
S3	S1	43.	43.	3.	3.	-0.3337E-03	0.39E-03	1.4462	0.70337	0.9992									
S3	S3/0	48.	48.	9.	9.	0.9177E-06	0.27E-04	0.9986	0.03172	0.9999									
S3	S2/0	48.	48.	8.	8.	-0.1574E-03	0.37E-04	1.2806	0.04078	0.9948									
S3	S1/0	43.	43.	3.	3.	-0.4990E-03	0.59E-03	1.6253	0.46732	0.9981									
S2	S0	39.	39.	13.	13.	-0.1528E-03	0.11E-03	1.1053	0.02268	0.9982									
S2	S1	31.	31.	9.	9.	-0.3809E-03	0.39E-03	1.1616	0.07649	0.9774									
S2	S2/0	48.	48.	8.	8.	0.1033E-03	0.24E-04	0.8147	0.0211	0.9938									
S2	S1/0	43.	43.	3.	3.	0.1041E-04	0.20E-04	0.9917	0.00977	0.9998									
S1	S0	39.	39.	13.	13.	-0.1747E-04	0.37E-04	1.0717	0.01782	0.9999									
S1	S1/0	43.	43.	3.	3.	-0.5462E-03	0.15E-03	1.1054	0.01697	0.9921									
S1	S2/0	43.	43.	3.	3.	0.2162E-03	0.48E-04	0.7037	0.10741	0.9994									
S0	S0	39.	39.	24.	24.	0.1284E-03	0.50E-04	0.9047	0.01383	0.9979									
S0	S1/0	43.	43.	9.	9.	0.2341E-03	0.50E-04	0.8752	0.05715	0.9991									
S0	S2/0	48.	48.	20.	20.	0.6523E-03	0.62E-04	0.8683	0.00789	0.9935									
S3/0	S2/0	48.	48.	8.	8.	-0.1571E-03	0.37E-04	1.2805	0.04078	0.9946									
S3/0	S1/0	43.	43.	3.	3.	-0.4825E-03	0.59E-03	1.6140	0.44405	0.9985									
S2/0	S1/0	43.	43.	13.	13.	-0.6517E-04	0.78E-04	1.0926	0.01817	0.9998									

MODE 1 IS INSTRUMENTAL WEIGHTING, THAT IS, 1/SIGMA**2

ORIGINAL FILE
OF POOR QUALITY

ORIGINAL
OF POC

COMPARISON OF COMPOSITE PROFILE WITH KUUMINZ MODEL

ALT-KM	COMP 03	%3 COMP	ERR X	MODL 03	%3 COMP-MODL	COMP COL	ATM-CN	COMP	ERR X	MODEL COL	COMP-MODL	ATM-CN	X
57.	0.9634E 16	26.7	-41.69	0.1365E 17	0.0001607	30.63	0.0002276	-0.000670	-41.69	0.0002276	-0.000670	-41.69	
56.	0.1232E 17	22.7	-30.63	0.1610E 17	0.0002013	24.67	0.0002830	-0.000815	-30.63	0.0002830	-0.000815	-30.63	
55.	0.1542E 17	21.1	-33.14	0.2080E 17	0.0002535	19.87	0.0003516	-0.000981	-33.14	0.0003516	-0.000981	-33.14	
54.	0.2097E 17	17.4	-21.61	0.2550E 17	0.0003216	15.22	0.0004378	-0.001162	-21.61	0.0004378	-0.001162	-21.61	
53.	0.2572E 17	15.5	-24.23	0.3195E 17	0.0004085	12.77	0.0005497	-0.001362	-24.23	0.0005497	-0.001362	-24.23	
52.	0.3332E 17	14.2	-15.23	0.3840E 17	0.0005104	10.31	0.0006757	-0.001573	-15.23	0.0006757	-0.001573	-15.23	
51.	0.4314E 17	10.7	-16.93	0.5240E 17	0.0006607	8.30	0.0008466	-0.001840	-16.93	0.0008466	-0.001840	-16.93	
50.	0.5679E 17	10.7	-12.37	0.6640E 17	0.0008466	6.59	0.0010657	-0.002191	-12.37	0.0010657	-0.002191	-12.37	
49.	0.7538E 17	8.1	-4.65	0.8470E 17	0.0010926	5.39	0.0013869	-0.002543	-4.65	0.0013869	-0.002543	-4.65	
48.	0.9843E 17	4.6	-3.78	0.1030E 16	0.0014160	4.28	0.0015962	-0.002802	-3.78	0.0015962	-0.002802	-3.78	
47.	0.1310E 18	3.2	-4.69	0.1360E 18	0.0018430	3.34	0.0021409	-0.002979	-4.69	0.0021409	-0.002979	-4.69	
46.	0.1614E 18	2.5	-10.37	0.1690E 18	0.0023873	2.62	0.0027085	-0.003212	-10.37	0.0027085	-0.003212	-10.37	
45.	0.2070E 18	1.7	-8.93	0.2215E 18	0.0030612	2.08	0.0034352	-0.003440	-8.93	0.0034352	-0.003440	-8.93	
44.	0.2515E 18	1.7	-7.75	0.2746E 18	0.0039028	1.66	0.0045573	-0.003745	-7.75	0.0045573	-0.003745	-7.75	
43.	0.3118E 18	1.5	-5.06	0.3366E 18	0.0049512	1.33	0.0058925	-0.004113	-5.06	0.0058925	-0.004113	-5.06	
42.	0.3735E 18	1.4	-10.62	0.3980E 18	0.0062305	1.08	0.0068584	-0.004541	-10.62	0.0068584	-0.004541	-10.62	
41.	0.4346E 18	1.3	-11.46	0.4502E 18	0.0077748	0.99	0.0083541	-0.004979	-11.46	0.0083541	-0.004979	-11.46	
40.	0.5077E 18	1.4	-7.42	0.5078E 18	0.0096356	0.74	0.0103988	-0.005391	-7.42	0.0103988	-0.005391	-7.42	
39.	0.7037E 18	1.3	-7.42	0.7408E 18	0.0119677	0.62	0.0131378	-0.005888	-7.42	0.0131378	-0.005888	-7.42	
38.	0.8127E 18	1.1	-11.69	0.8730E 18	0.0148080	0.53	0.0161071	-0.006224	-11.69	0.0161071	-0.006224	-11.69	
37.	0.9370E 18	1.2	-15.91	0.1046E 19	0.0180580	0.46	0.0196792	-0.006624	-15.91	0.0196792	-0.006624	-15.91	
36.	0.1053E 19	1.0	-18.18	0.1220E 19	0.0217591	0.40	0.0235970	-0.007071	-18.18	0.0235970	-0.007071	-18.18	
35.	0.1185E 19	1.1	-14.82	0.1400E 19	0.0259224	0.36	0.0287726	-0.007501	-14.82	0.0287726	-0.007501	-14.82	
34.	0.1376E 19	0.8	-14.08	0.1580E 19	0.0306877	0.32	0.0343181	-0.007950	-14.08	0.0343181	-0.007950	-14.08	
33.	0.1582E 19	0.7	-19.36	0.1805E 19	0.0361928	0.28	0.0406133	-0.008425	-19.36	0.0406133	-0.008425	-19.36	
32.	0.1731E 19	0.7	-28.34	0.2030E 19	0.0423020	0.25	0.0475359	-0.008996	-28.34	0.0475359	-0.008996	-28.34	
31.	0.1978E 19	1.2	-27.39	0.2275E 19	0.0487656	0.23	0.0537652	-0.009427	-27.39	0.0537652	-0.009427	-27.39	
30.	0.2253E 19	0.8	-26.14	0.2520E 19	0.0557455	0.21	0.0612650	-0.010617	-26.14	0.0612650	-0.010617	-26.14	
29.	0.2537E 19	0.7	-29.30	0.2880E 19	0.0636755	0.19	0.0743732	-0.011587	-29.30	0.0743732	-0.011587	-29.30	
28.	0.2811E 19	0.7	-29.30	0.3240E 19	0.0726355	0.19	0.0861260	-0.012493	-29.30	0.0861260	-0.012493	-29.30	
27.	0.3081E 19	0.8	-20.34	0.3635E 19	0.0825842	0.19	0.0989197	-0.013355	-20.34	0.0989197	-0.013355	-20.34	
26.	0.3346E 19	0.6	-17.08	0.4031E 19	0.0937444	0.18	0.1131837	-0.014333	-17.08	0.1131837	-0.014333	-17.08	
25.	0.3575E 19	0.6	-18.22	0.4282E 19	0.1062633	0.17	0.1285572	-0.015390	-18.22	0.1285572	-0.015390	-18.22	
24.	0.3807E 19	0.6	-29.35	0.4502E 19	0.1200756	0.16	0.1450796	-0.016508	-29.35	0.1450796	-0.016508	-29.35	
23.	0.3976E 19	0.6	-47.27	0.4708E 19	0.1368897	0.14	0.1627447	-0.017747	-47.27	0.1627447	-0.017747	-47.27	
22.	0.3270E 19	0.8	-72.46	0.4860E 19	0.1490800	0.13	0.1806650	-0.019059	-72.46	0.1806650	-0.019059	-72.46	
21.	0.4815E 19	1.0		0.4815E 19	0.1621564		0.1980694	-0.020510		0.1980694	-0.020510		
20.	0.2766E 19	1.0		0.4770E 19	0.1733879		0.2159063	-0.021514		0.2159063	-0.021514		

COMPARE ROCOZ + ECC COLUMN CONTENT WITH DOBSON TOTAL

	ROC02 22. + KM	ATM-CN	ERROR
	ECC 0-22. KM	0.1498	0.0021
	TOTAL	0.0996	0.0016
	DOBSON	0.2400	0.0010
	ROC02+ECC-DOBSON	0.2600	0.0182
		-0.0196	0.0203
			-7.58 PERCENT

CHECKS 2170: COMPENSATION CHANNEL FOR SZA=0, BASED ON DATA 50 - 35 KM, IS 897.0+-, 6.0 COUNTS.

ALTITUDE OBS.COMP COS SZA COMP(SZA=0)

59.	484.66	0.531	912.88
49.	474.12	0.531	892.99
48.	473.57	0.531	891.77
47.	455.65	0.531	857.64
46.	464.49	0.531	874.52
45.	483.74	0.531	910.70
44.	495.29	0.531	932.56
43.	480.27	0.531	904.00
42.	479.56	0.531	902.21
41.	472.97	0.531	890.07
40.	500.73	0.531	942.21
39.	473.77	0.532	891.35
38.	488.44	0.532	918.82
37.	478.56	0.532	900.09
36.	458.58	0.532	862.39
35.	461.82	0.532	868.56

CHECKS 2190:

ALTITUDE COS SZA I-SCATRD CORR FACTR PRED COMP OBS COMP PR-OB/PR X

57.	0.531	0.00009	0.5306	476.	456.	4.26
56.	0.531	0.00011	0.5307	476.	462.	2.89
55.	0.531	0.00013	0.5307	476.	466.	2.05
54.	0.531	0.00015	0.5307	476.	462.	3.05
53.	0.531	0.00017	0.5307	476.	483.	-1.41
52.	0.531	0.00019	0.5308	476.	493.	-3.49
51.	0.531	0.00022	0.5308	476.	489.	-2.63
50.	0.531	0.00026	0.5308	476.	485.	-1.78
49.	0.531	0.00030	0.5308	476.	474.	0.43
48.	0.531	0.00035	0.5309	476.	474.	0.55
47.	0.531	0.00040	0.5309	476.	454.	4.32
46.	0.531	0.00046	0.5309	476.	464.	2.46
45.	0.531	0.00053	0.5309	476.	462.	-1.58
44.	0.531	0.00062	0.5309	476.	493.	-4.00
43.	0.531	0.00071	0.5309	476.	480.	-0.66
42.	0.531	0.00082	0.5309	476.	479.	-0.66
41.	0.531	0.00095	0.5309	476.	473.	-5.15
40.	0.531	0.00110	0.5309	476.	501.	0.51
39.	0.532	0.00127	0.5308	476.	474.	0.51
38.	0.532	0.00146	0.5308	476.	488.	-2.58
37.	0.532	0.00169	0.5307	476.	479.	-0.51
36.	0.532	0.00195	0.5307	476.	459.	3.67
35.	0.532	0.00225	0.5306	476.	462.	2.98
34.	0.532	0.00260	0.5305	476.	483.	-1.42
33.	0.532	0.00301	0.5304	476.	477.	-4.53
32.	0.532	0.00347	0.5302	476.	476.	-0.05
31.	0.532	0.00401	0.5299	473.	476.	-1.23
30.	0.532	0.00453	0.5296	473.	481.	-1.49
29.	0.532	0.00535	0.5293	473.	488.	-2.78
28.	0.532	0.00618	0.5289	474.	483.	-2.17
27.	0.532	0.00714	0.5284	474.	479.	-1.08
26.	0.532	0.00824	0.5278	473.	483.	-2.09
25.	0.532	0.00952	0.5271	473.	495.	-4.74
24.	0.532	0.01099	0.5263	472.	464.	1.80
23.	0.532	0.01269	0.5254	471.	496.	-5.22
22.	0.532	0.01465	0.5243	470.	467.	0.70
21.	0.532	0.01691	0.5230	469.	474.	-1.02
20.	0.532	0.01952	0.5214	468.	480.	-2.53

ORIGINAL FILED IN
OF POOR QUALITY

CHECKS 2210:

CHECK OF DRAG COEFFICIENT VS ALTITUDE

ALTITUDE	VELOCITY	ACCELER	AIR DENS	DRAG C	REYNOLDS NO.
55.	134.98	-1.2638	0.511E-03	0.513	9050.
54.	125.21	-1.1941	0.580E-03	0.529	9486.
53.	115.91	-1.1048	0.642E-03	0.551	10025.
52.	107.20	-0.8708	0.754E-03	0.574	10565.
51.	99.46	-0.7337	0.856E-03	0.596	11116.
50.	92.44	-0.6782	0.970E-03	0.611	11807.
49.	84.99	-0.5538	0.112E-02	0.639	12492.
48.	79.36	-0.4746	0.129E-02	0.644	13442.
47.	73.03	-0.4455	0.147E-02	0.665	14236.
46.	67.16	-0.3411	0.169E-02	0.695	14998.
45.	62.87	-0.2719	0.192E-02	0.700	15992.
44.	58.51	-0.2444	0.221E-02	0.705	17206.
43.	54.52	-0.2141	0.255E-02	0.707	18608.
42.	50.66	-0.1869	0.292E-02	0.719	19715.
41.	47.14	-0.1635	0.338E-02	0.717	21510.
40.	43.72	-0.1543	0.395E-02	0.714	23657.
39.	40.08	-0.1293	0.459E-02	0.734	25360.
38.	37.27	-0.0998	0.535E-02	0.731	27743.
37.	34.73	-0.0919	0.618E-02	0.729	29944.
36.	31.97	-0.0794	0.719E-02	0.730	32311.
35.	29.76	-0.0656	0.842E-02	0.739	35583.
34.	27.57	-0.0507	0.971E-02	0.738	37918.
33.	25.36	-0.0326	0.111E-01	0.749	40935.
32.	23.43	-0.0443	0.132E-01	0.767	44677.
31.	21.58	-0.0383	0.156E-01	0.767	47907.
30.	19.88	-0.0314	0.180E-01	0.768	51817.
29.	18.42	-0.0267	0.211E-01	0.765	56547.
28.	16.99	-0.0252	0.250E-01	0.758	62794.
27.	15.45	-0.0223	0.294E-01	0.779	67710.
26.	14.10	-0.0175	0.346E-01	0.795	73239.
25.	12.97	-0.0142	0.411E-01	0.793	80782.
24.	11.91	-0.0131	0.483E-01	0.800	87378.
23.	10.76	-0.0123	0.572E-01	0.826	94440.
22.	9.62	-0.0104	0.672E-01	0.880	99269.

PROCOZ FLIGHT NO. 325.0 FLOWN 112283.(MIDDY.) 163000.0(HMMWISS.S)
AT 37.850 LAT, -75.480 LONG. ,MALLOPS ISLAND

OZONE PROFILE BASED ON ALL AVAILABLE ROCOZ DATA

ATM-CHN	OS	RUMPHS	ERRX	COL	ATM-CHN	RUMPHS	ERRX	COL	ATM-CHN	RUMPHS	ERRX	AIR	T	K	ERRX	AIR	PBAR	ERRX	PPMV	ERRX	MMWSS	S	SECHDS	FL	SZ
3566E-04	3	964E-16	26.7	0.00161	30.6	1.8	0.287	3.2224	0.348	26.8	1.3	0.387	261.7	1.8	1.8	0.387	0.387	0.387	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	122E-17	22.1	0.00254	24.9	1.8	0.286	3.2224	0.356	26.8	1.3	0.286	255.4	1.8	1.8	0.286	0.356	0.356	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	1207E-17	17.5	0.00322	15.8	1.8	0.274	3.2224	0.353	26.8	1.3	0.274	255.3	1.8	1.8	0.274	0.353	0.353	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	957E-17	15.4	0.00409	12.8	1.8	0.269	3.2224	0.343	26.8	1.3	0.269	256.3	1.8	1.8	0.269	0.343	0.343	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	3334E-17	14.2	0.00661	8.3	1.4	0.262	3.2224	0.343	26.8	1.3	0.262	256.4	1.4	1.4	0.262	0.343	0.343	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	5694E-17	10.7	0.00847	1.8	1.4	0.255	3.2224	0.333	26.8	1.3	0.255	257.7	1.4	1.4	0.255	0.333	0.333	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	758E-17	8.1	0.01093	5.4	1.4	0.249	3.2224	0.325	26.8	1.3	0.249	256.7	1.4	1.4	0.249	0.325	0.325	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	9835E-17	4.6	0.01416	3.3	1.4	0.239	3.2224	0.318	26.8	1.3	0.239	255.4	1.4	1.4	0.239	0.318	0.318	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	130E-18	3.2	0.01843	3.3	1.4	0.228	3.2224	0.312	26.8	1.3	0.228	252.9	1.4	1.4	0.228	0.312	0.312	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	1644E-18	2.5	0.02387	2.2	1.4	0.219	3.2224	0.306	26.8	1.3	0.219	252.9	1.4	1.4	0.219	0.306	0.306	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	207E-18	2.2	0.03061	1.1	1.4	0.212	3.2224	0.301	26.8	1.3	0.212	252.9	1.4	1.4	0.212	0.301	0.301	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	2551E-18	1.7	0.03951	1.1	1.4	0.209	3.2224	0.295	26.8	1.3	0.209	249.3	1.4	1.4	0.209	0.295	0.295	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	3746E-18	1.4	0.05233	1.0	1.4	0.201	3.2224	0.288	26.8	1.3	0.201	246.6	1.4	1.4	0.201	0.288	0.288	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	507E-18	1.1	0.07775	0.7	1.4	0.195	3.2224	0.277	26.8	1.3	0.195	240.0	1.4	1.4	0.195	0.277	0.277	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	7407E-18	1.1	0.11968	0.6	1.4	0.188	3.2224	0.266	26.8	1.3	0.188	237.2	1.4	1.4	0.188	0.266	0.266	1.3	23.8	1333.9	3.1	2018	1.1	57.95
3566E-04	3	9913E-18	1.1	0.1801	0.5	1.4	0.181	3.2224	0.254	26.8	1.3	0.181	233.6	1.4	1.4	0.181	0.254								

LAYER	BOUNDARIES	WILLIAMS	CH	OZONE CONTENT
0.0	---	0.244	0.0	0.0
0.244	---	0.488	0.0	0.0
0.488	---	0.977	1.161	4.115
0.977	---	1.953	1.953	10.923
1.953	---	3.906	7.113	31.764
3.906	---	7.813	15.225	54.359
7.813	---	15.625	31.250	55.356
15.625	---	31.250	62.500	20.082
31.250	---	62.500	125.000	7.022
62.500	---	125.000	250.000	26.659
125.000	---	250.000	500.000	
250.000	---	500.000	1000.000	

ROCOZ FLIGHT NO. 325.0 FLOWN 112283.(HHMMYY.) 163000.0(HHMMSS.S)
AT 37.850 LAT, -75.480 LONG. ,MALLOPS ISLAND

OZONE FROM THE COMPOSITE PROFILE AND ECC PROFILE AT STANDARD PRESSURE LEVELS

PRESSURE MBAR	ALTITUDE KM	AIR TEMP K	ROCOZ O3 NUM/M3	ROCOZ O3 MR/M3	ECC AIR TEMP K	ECC O3 NUM/M3	ECC O3 MR/M3
0.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.15	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.30	56.705	260.2	0.0	0.0	0.0	0.0	0.0
0.40	54.501	256.6	0.104E 17	2.659	0.0	0.0	0.0
0.50	52.797	254.4	0.182E 17	3.184	0.0	0.0	0.0
0.60	50.224	254.0	0.272E 17	4.491	0.0	0.0	0.0
0.70	47.516	253.3	0.374E 17	6.575	0.0	0.0	0.0
1.00	44.470	252.1	0.527E 18	8.706	0.0	0.0	0.0
1.50	42.330	249.7	0.734E 18	10.092	0.0	0.0	0.0
2.00	39.375	240.9	0.993E 18	11.821	0.0	0.0	0.0
3.00	37.341	234.0	0.108E 19	12.093	0.0	0.0	0.0
4.00	35.783	231.4	0.148E 19	11.564	0.0	0.0	0.0
5.00	33.468	227.7	0.177E 19	11.209	0.0	0.0	0.0
7.00	31.049	221.9	0.240E 19	9.217	0.0	0.0	0.0
10.00	28.348	213.1	0.308E 19	7.470	230.6	0.192E 20	10.109
15.00	26.482	213.1	0.389E 19	6.323	222.5	0.274E 20	9.291
20.00	25.907	213.1	0.478E 19	5.574	220.0	0.363E 20	9.131
30.00	22.110	209.5	0.514E 19	3.025	216.4	0.486E 20	8.015
40.00	20.727	209.5	0.0	0.0	212.9	0.458E 20	5.576
50.00	18.607	209.5	0.0	0.0	212.1	0.391E 20	3.795
70.00	16.458	209.5	0.0	0.0	205.1	0.254E 20	1.520
100.00	13.943	209.5	0.0	0.0	208.0	0.738E 19	0.351
150.00	12.128	209.5	0.0	0.0	213.8	0.343E 19	0.114
200.00	10.641	209.5	0.0	0.0	221.7	0.343E 19	0.082
250.00	9.415	209.5	0.0	0.0	225.2	0.611E 19	0.126
300.00	8.415	209.5	0.0	0.0	233.2	0.544E 19	0.097
400.00	5.732	209.5	0.0	0.0	247.0	0.501E 19	0.071
500.00	3.131	209.5	0.0	0.0	259.4	0.389E 19	0.062
700.00	1.532	209.5	0.0	0.0	273.1	0.689E 19	0.075
950.00	0.167	209.5	0.0	0.0	289.0	0.689E 19	0.046

ORIGINAL PAGE IS
OF POOR QUALITY

CARDS 2150: NUMBER OF DATAS RECORDS READ IS 103
 TAPE 2940: 404 RECORDS FROM SMOOTH TAPE
 PRIMARY 2000: ARRAYS ARE NOT FILLED

IV-214

ORIGINAL DATA OF POOR QUALITY

31. -0.1015 0.0012 -0.0993 0.0005 -0.0022 0.0013 2.19
30. -0.1109 0.0018 -0.1066 0.0006 -0.0043 0.0019 3.50
29. -0.1257 0.0021 -0.1213 0.0011 -0.0016 0.0017 -1.26
28. -0.1322 0.0022 -0.1412 0.0006 -0.0030 0.0022 -2.16
27. -0.1326 0.0013 -0.1459 0.0009 -0.0007 0.0016 -4.52
26. -0.1726 0.0017 -0.1811 0.0006 -0.0007 0.0018 -4.92
25. -0.1995 0.0013 -0.1835 0.0006 -0.0062 0.0015 3.30
24. -0.2079 0.0015 -0.2123 0.0007 -0.0003 0.0016 -4.00
23. -0.2046 0.0019 -0.2052 0.0007 -0.0007 0.0021 -0.33
22. -0.1914 0.0021 -0.1946 0.0011 -0.0030 0.0024 -1.54
21. -0.1702 0.0026 -0.1694 0.0012 -0.0008 0.0028 -0.49
20. -0.1479 0.0028 -0.1491 0.0014 -0.0011 0.0031 -0.76

COMPARISON OF B(LM I)/DM WITH B FROM SMOOTH FOR FILTER S0
ALT-EN B(LM I)/DM NOISE B(SMOOTH) STDEV DIFFERENCE+ - ERROR DIFFX

39. -0.0167 0.0023 -0.0156 0.0008 -0.0011 0.0025 -6.72
38. -0.0150 0.0021 -0.0235 0.0009 -0.0014 0.0023 -7.17
37. -0.0224 0.0023 -0.0205 0.0012 -0.0019 0.0023 -8.95
36. -0.0226 0.0020 -0.0244 0.0012 -0.0013 0.0023 -1.10
35. -0.0226 0.0020 -0.0226 0.0008 -0.0018 0.0022 -3.84
34. -0.0311 0.0019 -0.0271 0.0006 -0.0039 0.0017 13.93
33. -0.0342 0.0013 -0.0414 0.0006 -0.0032 0.0014 -6.09
32. -0.0497 0.0013 -0.0435 0.0005 -0.0028 0.0014 -6.64
31. -0.0495 0.0012 -0.0345 0.0006 -0.0052 0.0013 5.50
30. -0.0457 0.0016 -0.0410 0.0005 -0.0037 0.0016 8.54
29. -0.0527 0.0013 -0.0544 0.0009 -0.0017 0.0015 -3.18
28. -0.0586 0.0017 -0.0616 0.0007 -0.0030 0.0018 -5.00
27. -0.0649 0.0011 -0.0611 0.0007 -0.0039 0.0013 -6.14
26. -0.0729 0.0014 -0.0804 0.0004 -0.0075 0.0014 -9.78
25. -0.0809 0.0009 -0.0746 0.0006 -0.0064 0.0011 8.31
24. -0.0901 0.0010 -0.0949 0.0005 -0.0048 0.0011 -5.16
23. -0.0944 0.0012 -0.0927 0.0003 -0.0017 0.0012 1.85
22. -0.0962 0.0009 -0.0942 0.0006 -0.0040 0.0010 -4.54
21. -0.0800 0.0011 -0.0786 0.0005 -0.0014 0.0012 1.81
20. -0.0710 0.0012 -0.0710 0.0005 -0.0010 0.0013 -1.35

COMPARISON OF B(LM I)/DM WITH B FROM SMOOTH FOR FILTER S1/0
ALT-EN B(LM I)/DM NOISE B(SMOOTH) STDEV DIFFERENCE+ - ERROR DIFFX

57. -0.0130 0.0002 -0.0122 0.0005 -0.0017 0.0002 12.01
56. -0.0130 0.0006 -0.0139 0.0006 -0.0021 0.0006 12.12
55. -0.0228 0.0009 -0.0204 0.0007 -0.0029 0.0009 9.07
54. -0.0228 0.0002 -0.0264 0.0007 -0.0014 0.0003 5.21
53. -0.0335 0.0006 -0.0346 0.0008 -0.0009 0.0007 2.56
52. -0.0400 0.0006 -0.0432 0.0009 -0.0028 0.0001 6.58
51. -0.0500 0.0002 -0.0566 0.0011 -0.0015 0.0003 2.55
50. -0.0738 0.0002 -0.0710 0.0012 -0.0028 0.0003 3.88
49. -0.0972 0.0002 -0.0928 0.0015 -0.0044 0.0003 4.67
48. -0.1200 0.0000 -0.1206 0.0015 -0.0054 0.0002 4.40
47. -0.1693 0.0001 -0.1595 0.0023 -0.0098 0.0004 0.52
46. -0.2002 0.0001 -0.2026 0.0021 -0.0024 0.0003 -1.17
45. -0.2411 0.0001 -0.2418 0.0021 -0.0014 0.0003 0.57
44. -0.2849 0.0007 -0.2847 0.0021 -0.0018 0.0000 -0.02
43. -0.3276 0.0005 -0.3259 0.0022 -0.0017 0.0000 0.53
42. -0.3646 0.0013 -0.3672 0.0030 -0.0026 0.0007 -0.72
41. -0.3869 0.0012 -0.3991 0.0042 -0.0122 0.0009 -3.09
40. -0.3653 0.0023 -0.3914 0.0066 -0.0269 0.0014 -7.12

COMPARISON OF B(LM I)/DM WITH B FROM SMOOTH FOR FILTER S2/0
ALT-EN B(LM I)/DM NOISE B(SMOOTH) STDEV DIFFERENCE+ - ERROR DIFFX

48. -0.0201 0.0021 -0.0199 0.0005 -0.0022 0.0021 1.16
47. -0.0201 0.0022 -0.0249 0.0005 -0.0013 0.0021 4.93
46. -0.0338 0.0021 -0.0334 0.0006 -0.0004 0.0022 1.05
45. -0.0323 0.0024 -0.0417 0.0005 -0.0006 0.0023 -1.58
44. -0.0458 0.0026 -0.0531 0.0007 -0.0012 0.0027 1.83
43. -0.0415 0.0023 -0.0446 0.0009 -0.0004 0.0025 0.52
42. -0.0415 0.0023 -0.0411 0.0009 -0.0004 0.0025 -0.42
41. -0.0994 0.0025 -0.0998 0.0008 -0.0004 0.0026 -0.93
40. -0.1174 0.0021 -0.1105 0.0008 -0.0011 0.0023 0.62
39. -0.1346 0.0023 -0.1358 0.0010 -0.0008 0.0025 -0.93
38. -0.1327 0.0024 -0.1544 0.0010 -0.0017 0.0026 -1.11
37. -0.1717 0.0031 -0.1714 0.0012 -0.0003 0.0024 0.15
36. -0.1931 0.0034 -0.1900 0.0016 -0.0031 0.0033 1.64
35. -0.2185 0.0043 -0.2112 0.0018 -0.0031 0.0038 1.64
34. -0.2423 0.0009 -0.2466 0.0022 -0.0043 0.0034 -3.40
33. -0.2551 0.0009 -0.2554 0.0025 -0.0004 0.0034 -1.75
32. -0.2652 0.0007 -0.2574 0.0030 -0.0018 0.0034 -0.15
31. -0.2858 0.0001 -0.2988 0.0034 -0.0131 0.0007 -4.47

ORIGINAL PAGE IS
OF POOR QUALITY

COMPARISON OF D(LN I)/DM WITH B FROM SMOOTH FOR FILTER S1/0
ALT-KN D(LN I)/DM NOISE B(SMOOTH) STDEV DIFFERENCE+- ERROR DIFFX

43.	-0.0126	0.0012	-0.0139	0.0004	0.0005	0.0013	-3.63
42.	-0.0153	0.0013	-0.0137	0.0004	0.0004	0.0014	-2.50
41.	-0.0134	0.0011	-0.0162	0.0004	-0.0002	0.0012	1.34
40.	-0.0222	0.0012	-0.0217	0.0004	-0.0005	0.0012	2.10
39.	-0.0208	0.0011	-0.0262	0.0004	0.0002	0.0011	-0.80
38.	-0.0295	0.0010	-0.0297	0.0005	0.0002	0.0011	-0.75
37.	-0.0340	0.0011	-0.0354	0.0004	-0.0003	0.0011	0.91
36.	-0.0346	0.0011	-0.0382	0.0005	-0.0004	0.0010	1.09
35.	-0.0438	0.0009	-0.0437	0.0004	-0.0003	0.0010	0.03
34.	-0.0404	0.0008	-0.0505	0.0003	0.0008	0.0008	-1.69
33.	-0.0537	0.0007	-0.0501	0.0003	0.0011	0.0007	-0.58
32.	-0.0597	0.0007	-0.0558	0.0003	-0.0011	0.0007	2.00
31.	-0.0611	0.0007	-0.0689	0.0004	-0.0002	0.0008	0.29
30.	-0.0653	0.0008	-0.0656	0.0004	-0.0002	0.0008	1.10
29.	-0.0729	0.0008	-0.0733	0.0004	0.0004	0.0009	-0.59
28.	-0.0795	0.0009	-0.0795	0.0004	-0.0008	0.0009	0.85
27.	-0.0880	0.0009	-0.0841	0.0004	-0.0038	0.0010	4.45
26.	-0.1096	0.0011	-0.1005	0.0005	0.0010	0.0010	-1.01
25.	-0.1139	0.0012	-0.1086	0.0004	-0.0038	0.0013	0.92
24.	-0.1190	0.0014	-0.1177	0.0005	0.0038	0.0013	-3.27
23.	-0.1011	0.0010	-0.1127	0.0007	0.0027	0.0016	-2.41
22.	-0.0944	0.0008	-0.1001	0.0008	-0.0010	0.0019	0.99
21.	-0.0797	0.0004	-0.0901	0.0009	-0.0004	0.0022	0.40
20.	-0.0777	0.0024	-0.0791	0.0011	0.0014	0.0027	-1.77

BT:PMT 2320: K42113 FILE 10 ON UNIT 15 HAS 361 RECORDS. LAST RECORD IS TYPE 500.
MAIN 2990: PROGRAM END